

# EE 322 Advanced Analog Electronics, Spring 2012

## Homework #9 solution

SS 13.34. Figure P13.34 shows a monostable multivibrator circuit. In the stable state,  $v_o = L_+$ ,  $v_A = 0$ , and  $v_B = -V_{\text{ref}}$ . the circuit can be triggered by applying a positive input pulse of height greater than  $V_{\text{ref}}$ . For normal operation,  $C_1 R_1 \ll CR$ . Show the resulting waveforms of  $v_o$  and  $v_A$ . Also, show that the pulse generated at the output will have a width  $T$  given by

$$T = CR \ln \left( \frac{L_+ - L_-}{V_{\text{ref}}} \right)$$

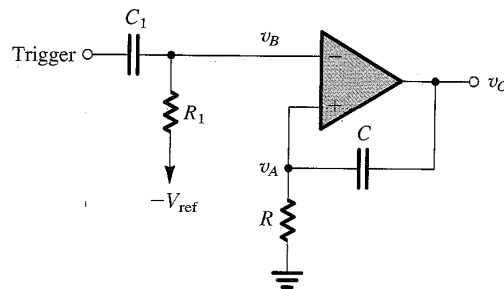
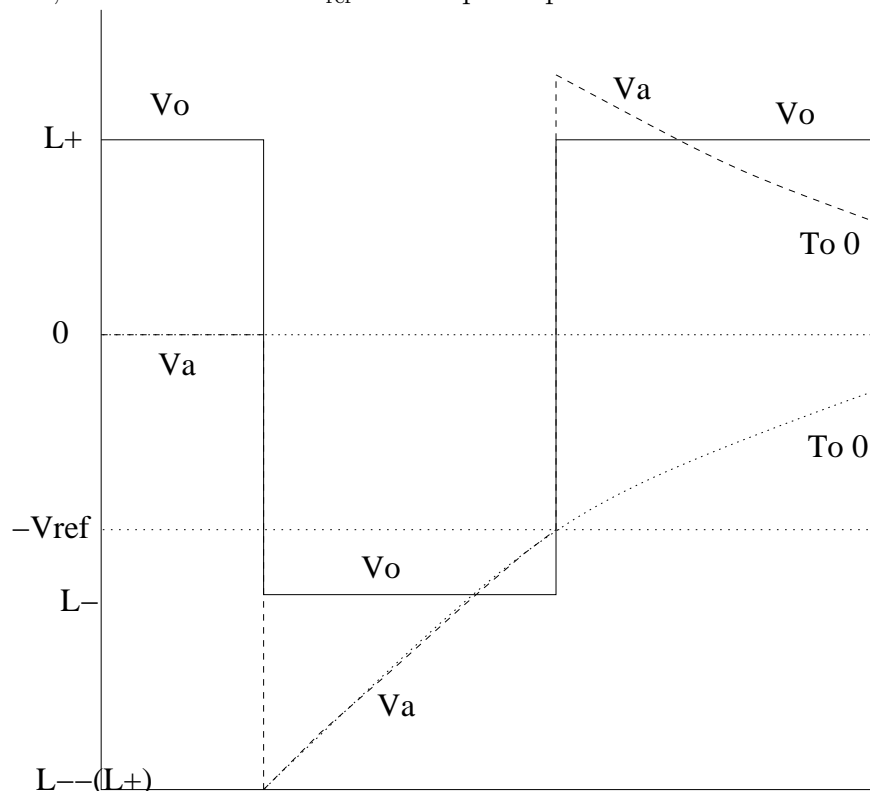


FIGURE P13.34

$v_A$  begins at ground because there is no current through  $R$ . As the positive pulse is applied to trigger,  $v_B$  is pulled low which causes  $v_o$  to go low. The voltage across the capacitor is still  $L_+$ , so the voltage  $v_A = L_- - L_+$ . The capacitor begins to charge from that voltage to ground. However, once it reaches  $-V_{\text{ref}}$  the output flips. The waveforms are here



and here is the expression for determining  $T$

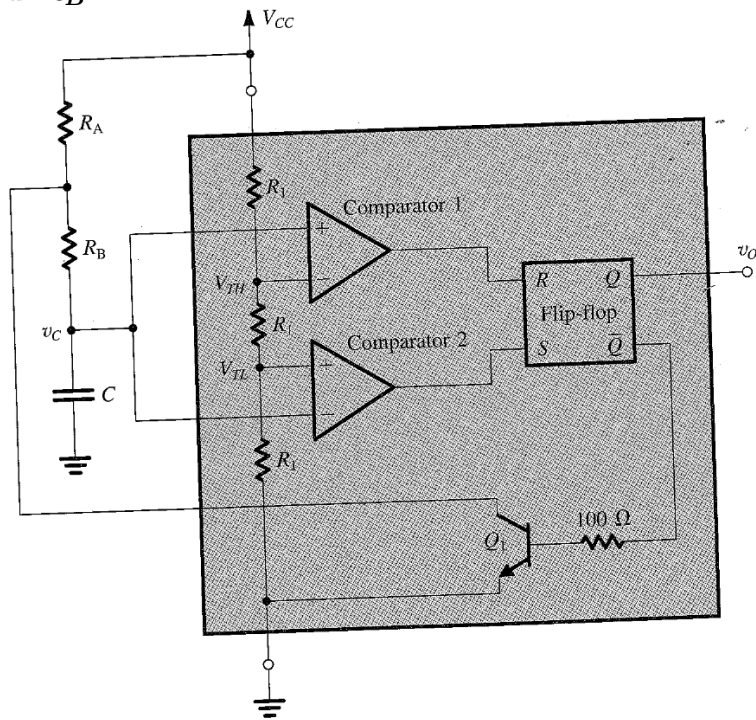
$$(L_- - L_+) e^{-\frac{T}{RC}} = -V_{\text{ref}}$$

which can be re-written as

$$\ln \left( \frac{-V_{\text{ref}}}{L_- - L_+} \right) = -\frac{T}{RC}$$

$$T = RC \ln \left( \frac{L_+ - L_-}{V_{\text{ref}}} \right)$$

**SS 13.39.** Using a 680 pF capacitor, design the astable circuit of Fig. 13.29(a) to obtain a square wave with a 50 kHz frequency and a 75% duty cycle. Specify the values of  $R_A$  and  $R_B$ .



This is a straightforward application of formulas given in the text book,

$$T = \frac{1}{f} = 0.69C(R_A + 2R_B) \quad \text{duty} = \frac{R_A + R_B}{R_A + 2R_B}$$

Begin by finding  $R_A + 2R_B$ ,

$$R_A + 2R_B = \frac{1}{0.69fC} = \frac{1}{0.69 \times 50 \times 10^3 \times 680 \times 10^{-12}} = 42.63 \text{ k}\Omega$$

Next, find  $R_A + R_B$  from the duty cycle formula,

$$R_A + R_B = \text{duty} \times (R_A + 2R_B) = 0.75 \times 42.63 = 31.97 \text{ k}\Omega$$

Next,

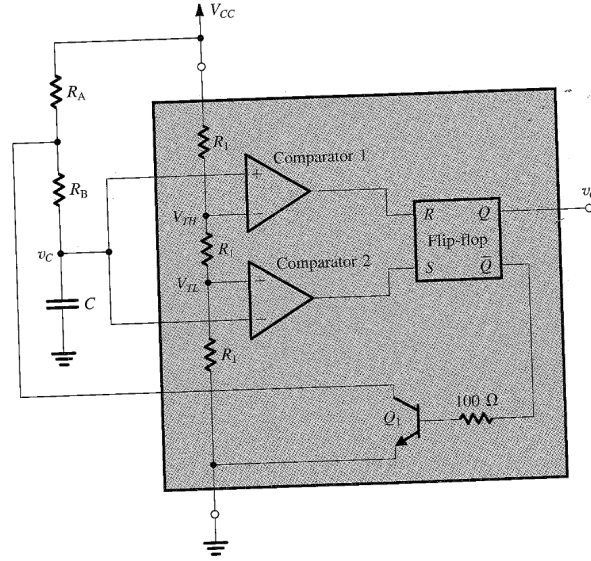
$$R_B = (R_A + 2R_B) - (R_A + R_B) = 42.63 - 31.97 = 10.66 \text{ k}\Omega$$

and

$$R_A = (R_A + R_B) - R_B = 31.97 - 10.66 = 21.31 \text{ k}\Omega$$

**SS 13.40** The node in the 555 timer at which the voltage is  $V_{TH}$  (i.e. the inverting input terminal for the comparator 1) is usually connected to an external terminal. This allows the user to change  $V_{TH}$  externally (i.e.,  $V_{TH}$  no longer remains at  $\frac{2}{3}V_{CC}$ ). Note, however, that whatever the value of  $V_{TH}$  becomes,  $V_{TL}$  always remains  $\frac{1}{2}V_{TH}$ .

- (a) For the astable circuit of Fig. 13.29, rederive the expression for  $T_H$  and  $T_L$ , expressing them in terms of  $V_{TH}$  and  $V_{TL}$ .



- (b) For the case  $C = 1 \text{ nF}$ ,  $R_A = 7.2 \text{ k}\Omega$ ,  $R_B = 3.6 \text{ k}\Omega$ , and  $V_{CC} = 5 \text{ V}$ , find the frequency of oscillation and the duty cycle of the resulting square wave when no external voltage is applied to the terminal  $V_{TH}$ .
- (c) For the design in (b), let a sine-wave signal of a much lower frequency than that found in (b) and of 1-V peak amplitude be capacitively coupled to the circuit node  $V_{TH}$ . This signal will cause  $V_{TH}$  to change around its quiescent value of  $\frac{2}{3}V_{CC}$ , and thus  $T_H$  will change correspondingly - a modulation process. Find  $T_H$ , and find the frequency of oscillation and the duty cycle at the two extreme values of  $V_{TH}$ .
- (a)  $T_H$  is the time when the output is high and the capacitor is charging up. It is charging from  $V_{TL}$  towards  $V_{CC}$  with time-constant  $(R_A + R_B)C$  and gets interrupted at  $V_{TH}$ . Thus we have

$$\left(1 - e^{-\frac{T_H}{(R_A + R_B)C}}\right)(V_{CC} - V_{TL}) - V_{TL} = V_{TH}$$

$$1 - e^{-\frac{T_H}{(R_A + R_B)C}} = \frac{V_{TH} - V_{TL}}{V_{CC} - V_{TL}}$$

$$e^{-\frac{T_H}{(R_A + R_B)C}} = 1 - \frac{V_{TH} - V_{TL}}{V_{CC} - V_{TL}} = \frac{V_{CC} - V_{TL} - V_{TH} + V_{TL}}{V_{CC} - V_{TL}} = \frac{V_{CC} - V_{TH}}{V_{CC} - V_{TL}}$$

$$T_H = (R_A + R_B)C \ln \frac{V_{CC} - V_{TL}}{V_{CC} - V_{TH}}$$

$T_L$  is the time when the output is low and the capacitor is discharging. It discharges from  $V_{TH}$  towards ground with time constant  $R_B C$  and gets interrupted at  $V_{TL}$ . Thus we have

$$e^{-\frac{T_L}{R_B C}} V_{TH} = V_{TL}$$

$$T_L = R_B C \ln \frac{V_{TH}}{V_{TL}} = R_B C \ln 2$$

(not it is independent of  $V_{TH}$ )

(b) In this case we have  $V_{TH} = \frac{2}{3}V_{CC}$  and  $V_{TL} = \frac{1}{3}V_{CC}$ . Then  $T_H$  is

$$T_H = (7.2 + 3.6) \times 10^3 \times 1 \times 10^{-9} \ln \left( \frac{1 - \frac{1}{3}}{1 - \frac{2}{3}} \right) = 7.5 \times 10^{-6} \text{ s} = 7.5 \mu\text{s}$$

and  $T_L$  is

$$T_L = 3.6 \times 10^3 \times 1 \times 10^{-9} \times \ln 2 = 2.5 \times 10^{-6} = 2.5 \mu\text{s}$$

The period of the signal is then  $T = T_H + T_L = 10 \mu\text{s}$  and the frequency is  $f = 100 \text{ kHz}$ . The duty cycle for high output is 75%.

(c) We always have  $V_{TL} = \frac{V_{TH}}{2}$ . At the two extremes we have  $V_{TH} = \frac{2}{3}V_{TH} \pm A$ , where  $A$  is the amplitude of the sine wave. When the the voltage is increased we have

$$V_{TH} = \frac{2}{3}V_{CC} + A = \frac{2}{3} \times 5 + 1 = 4.33 \text{ V}$$

and

$$V_{TL} = \frac{V_{TH}}{2} = 2.17 \text{ V}$$

so that

$$T_H = (7.2 + 3.6) \times 10^3 \times 1 \times 10^{-9} \ln \frac{5 - 2.17}{5 - 4.33} = 1.55 \times 10^{-5} \text{ s} = 15.5 \mu\text{s}$$

and the frequency is

$$f = \frac{1}{T_H + T_L} = \frac{10^6}{15.5 + 2.5} = 55.5 \text{ kHz}$$

and the duty

$$\frac{T_H}{T_H + T_L} = \frac{15.5}{15.5 + 2.5} = 86.1\%$$

when the voltage is one volt lower we get

$$V_{TH} = 2.33 \text{ V} \quad V_{TL} = \frac{2.33}{2} = 1.17 \text{ V}$$

and

$$T_H = (7.2 + 3.6) \times 10^3 \times 1 \times 10^{-9} \ln \frac{5 - 1.17}{5 - 2.33} = 3.90 \mu\text{s}$$

Then the frequency is

$$f = \frac{1}{T_H + T_L} = \frac{10^6}{3.90 + 2.5} = 156 \text{ kHz}$$

and the duty cycle is

$$\frac{T_H}{T_H + T_L} = 60.9\%$$