Lecture Navigation Mathematics: Other Descriptions of Orientation

EE 570: Location and Navigation

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Lecture Topics

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1 Review

Review

Rotation Matrices R, C

- Notation to be adopted:
 - C represents an orientation
 - R represents a rotation
- Sequence of rotations can be composed via multiplication of rotation matrices
 - rotations about relative axis \Rightarrow post-/right-multiply

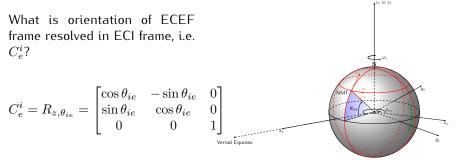
$$C_{final} = C_{initial}R$$

- rotations about fixed axis \Rightarrow pre-/left-multiply

$$C_{final} = RC_{initial}$$

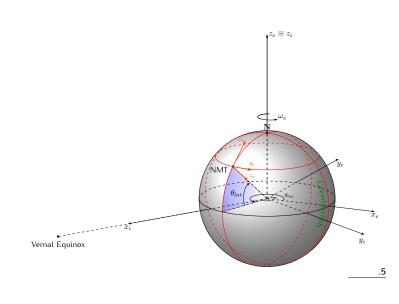
• $3 \times 3 = 9$ elements with 6 constraints $\Rightarrow 3$ parameters are sufficient to describe orientation

Review - Example



What is θ_{ie} ? angle from frame $\{i\}$ to frame $\{e\}$; here $\theta_{ie} = \omega_{ie}(t - t_0)$

Review - Example



What is the nav frame resolved in the ECEF frame, i.e. C_n^e ?

2 Roll-Pitch-Yaw Angles

Roll-Pitch-Yaw Angles

Roll-Pitch-Yaw angles

- often used to represent orientation of aircraft
- three angles (ϕ, θ, ψ) that represent the sequence of rotations about the x-, y- and z-axes of a fixed frame
- given angles (ϕ, θ, ψ) , equivalent rotation matrix can be found via

$$\begin{split} C_{RPY} &= R_{z,\psi} R_{y,\theta} R_{x,\phi} \\ &= \begin{bmatrix} c_{\psi} & -s_{\psi} & 0 \\ s_{\psi} & c_{\psi} & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} c_{\theta} & 0 & s_{\theta} \\ 0 & 1 & 0 \\ -s_{\theta} & 0 & c_{\theta} \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 \\ 0 & c_{\phi} & -s_{\phi} \\ 0 & s_{\phi} & c_{\phi} \end{bmatrix} \\ &= \begin{bmatrix} c_{\theta} c_{\psi} & c_{\psi} s_{\theta} s_{\phi} - c_{\phi} s_{\psi} & c_{\phi} c_{\psi} s_{\theta} + s_{\phi} s_{\psi} \\ c_{\theta} s_{\psi} & c_{\phi} c_{\psi} + s_{\theta} s_{\phi} s_{\psi} & c_{\phi} s_{\theta} s_{\psi} - c_{\psi} s_{\phi} \\ -s_{\theta} & c_{\theta} s_{\phi} & c_{\theta} c_{\phi} \end{bmatrix} \end{split}$$

Roll-Pitch-Yaw Angles

Given a rotation matrix that describes a desired orientation

$$C_{desired} = \begin{bmatrix} C_{11} & C_{12} & C_{13} \\ C_{21} & C_{22} & C_{23} \\ C_{31} & C_{32} & C_{33} \end{bmatrix}$$

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Roll-Pitch-Yaw angles $(\phi,\ \theta,\ \psi)$ can be found (the inverse solution) by equating combinations of terms

$$\begin{bmatrix} \hline c_{\theta}c_{\psi} & c_{\psi}s_{\theta}s_{\phi} - c_{\phi}s_{\psi} & c_{\phi}c_{\psi}s_{\theta} + s_{\phi}s_{\psi} \\ \hline c_{\theta}s_{\psi} & c_{\phi}c_{\psi} + s_{\theta}s_{\phi}s_{\psi} & c_{\phi}s_{\theta}s_{\psi} - c_{\psi}s_{\phi} \\ \hline -s_{\theta} & c_{\theta}s_{\phi} & c_{\theta}c_{\phi} \end{bmatrix} = \begin{bmatrix} \hline C_{11} & C_{12} & C_{13} \\ \hline C_{21} & C_{22} & C_{23} \\ \hline C_{31} & C_{32} & C_{33} \end{bmatrix}$$
$$\frac{C_{21}}{C_{11}} = \frac{c_{\theta}s_{\psi}}{c_{\theta}c_{\psi}} = \tan(\psi)$$

Roll-Pitch-Yaw Angles

$$\begin{bmatrix} c_{\theta}c_{\psi} & c_{\psi}s_{\theta}s_{\phi} - c_{\phi}s_{\psi} & c_{\phi}c_{\psi}s_{\theta} + s_{\phi}s_{\psi} \\ c_{\theta}s_{\psi} & c_{\phi}c_{\psi} + s_{\theta}s_{\phi}s_{\psi} & c_{\phi}s_{\theta}s_{\psi} - c_{\psi}s_{\phi} \\ -s_{\theta} & \boxed{c_{\theta}s_{\phi}} & \boxed{c_{\theta}c_{\phi}} \end{bmatrix} = \begin{bmatrix} C_{11} & C_{12} & C_{13} \\ C_{21} & C_{22} & C_{23} \\ C_{31} & \boxed{C_{32}} & \boxed{C_{33}} \end{bmatrix}$$
$$\frac{C_{32}}{C_{33}} = \frac{c_{\theta}s_{\phi}}{c_{\theta}c_{\phi}} = \tan(\phi)$$

$$\begin{array}{cccc} c_{\theta}c_{\psi} & c_{\psi}s_{\theta}s_{\phi} - c_{\phi}s_{\psi} & c_{\phi}c_{\psi}s_{\theta} + s_{\phi}s_{\psi} \\ c_{\theta}s_{\psi} & c_{\phi}c_{\psi} + s_{\theta}s_{\phi}s_{\psi} & c_{\phi}s_{\theta}s_{\psi} - c_{\psi}s_{\phi} \\ \hline \hline -s_{\theta} & \hline \\ \hline \hline c_{\theta}s_{\phi} & \hline \\ \hline c_{\theta}s_{\phi} & \hline \\ \hline c_{\theta}c_{\phi} \end{bmatrix} = \begin{bmatrix} C_{11} & C_{12} & C_{13} \\ C_{21} & C_{22} & C_{23} \\ \hline C_{31} & \hline \\ \hline \\ C_{31} & \hline \\ \hline \\ c_{32} & \hline \\ \hline \\ c_{33} \end{bmatrix}$$
$$\frac{-C_{31}}{\sqrt{C_{32}^2 + C_{33}^2}} = \frac{-(-s_{\theta})}{\sqrt{c_{\theta}^2(s_{\phi}^2 + c_{\phi}^2)}} = \frac{s_{\theta}}{c_{\theta}} = \tan(\theta)$$

3 Angle-Axis

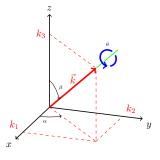
Angle-Axis

Angle-Axis

- one rotation about general axis will be used to describe orientation, so **does not** have the "rotation in sequence" issue
- rotation matrix C can be realized via rotation away from initial frame by angle θ about appropriately chosen axis $\vec{k} = [k_1, k_2, k_3]^T$ of rotation
- assume \vec{k} is a unit vector

Angle-Axis

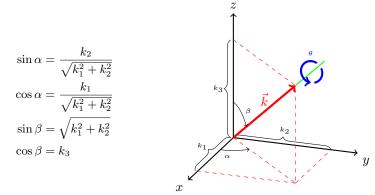
Rotation matrix can be derived by rotating one of the principal axis (x, y, or z) onto the vector \vec{k} , then performing a rotation of θ , and finally undoing the original changes



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• it can be shown (by composing rotations) that

$$R_{\vec{k},\theta} = \begin{bmatrix} k_1^2 V_{\theta} + c_{\theta} & k_1 k_2 V_{\theta} - k_3 s_{\theta} & k_1 k_3 V_{\theta} + k_2 s_{\theta} \\ k_1 k_2 V_{\theta} + k_3 s_{\theta} & k_2^2 V_{\theta} + c_{\theta} & k_2 k_3 V_{\theta} - k_1 s_{\theta} \\ k_1 k_3 V_{\theta} - k_2 s_{\theta} & k_2 k_3 V_{\theta} + k_1 s_{\theta} & k_3^2 V_{\theta} + c_{\theta} \end{bmatrix}$$
(1)

where $V_{\theta} \equiv 1 - c_{\theta}$.

Angle-Axis - Alternate Approach

Alternate approach to development of angle-axis is to relate rotation matrix to its equivalent angle-axis pair by

$$R_{\vec{k},\theta(t)} = e^{\kappa\theta(t)}$$

where

skew-symmetric

$$\kappa = [\vec{k} \times] = \begin{bmatrix} 0 & -k_3 & k_2 \\ k_3 & 0 & -k_1 \\ -k_2 & k_1 & 0 \end{bmatrix}$$

is the skew-symmetric matrix version of the axis vector $\vec{k} = \begin{bmatrix} k_1 & k_2 & k_3 \end{bmatrix}^T$. Note: $\kappa^T = -\kappa$.

Angle-Axis - Rodrigues Formula

• Using Taylor expansion of matrix-exponential

$$R_{\vec{k},\theta(t)} = e^{\kappa\theta(t)} = \mathcal{I} + \kappa\theta(t) + \frac{\kappa^2\theta^2(t)}{2!} + \frac{\kappa^3\theta^3(t)}{3!} + \cdots$$

which, after a bit of manipulation (recalling Taylor series of sine and cosine and noting $\kappa^3 = -\kappa$), can be shown to be

Rodrigues Formula

$$R_{\vec{k},\theta(t)} = \mathcal{I} + \sin(\theta(t))\kappa + [1 - \cos(\theta(t))]\kappa^2$$

• Multiplying out the *rhs* of the above equation gives us the same rotation matrix as that in Eq. 1.

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Angle-Axis to Rotation Matrix

Desired rotation matrix to (\vec{k}, θ) – the inverse problem

$$R_{\vec{k},\theta} = \begin{bmatrix} k_1^2 V_{\theta} + c_{\theta} & k_1 k_2 V_{\theta} - k_3 s_{\theta} & k_1 k_3 V_{\theta} + k_2 s_{\theta} \\ k_1 k_2 V_{\theta} + k_3 s_{\theta} & k_2^2 V_{\theta} + c_{\theta} & k_2 k_3 V_{\theta} - k_1 s_{\theta} \\ k_1 k_3 V_{\theta} - k_2 s_{\theta} & k_2 k_3 V_{\theta} + k_1 s_{\theta} & k_3^2 V_{\theta} + c_{\theta} \end{bmatrix} = \begin{bmatrix} r_{11} & r_{12} & r_{13} \\ r_{21} & r_{22} & r_{23} \\ r_{31} & r_{32} & r_{33} \end{bmatrix} = R_{desired}$$

- find angle-axis pair (\vec{k}, θ) needed to realize desired rotation matrix
- look at trace of rotation matrix and recall $V_{\theta} \equiv 1 \cos \theta$

$$Tr\left(R_{\vec{k},\theta}\right) = \left[k_{1}^{2} + k_{2}^{2} + k_{3}^{2}\right]\left(1 - \cos\theta\right) + 3\cos\theta = 1 + 2\cos\theta$$
$$\Rightarrow \theta = \cos^{-1}\left(\frac{Tr\left(R_{\vec{k},\theta}\right) - 1}{2}\right) = \cos^{-1}\left(\frac{r_{11} + r_{22} + r_{33} - 1}{2}\right)$$

Angle-Axis to Rotation Matrix

Now for the axis of rotation; a review of the structure suggests

$$r_{32} - r_{23} = 2k_1s_{\theta}$$

$$r_{13} - r_{31} = 2k_2s_{\theta}$$

$$r_{21} - r_{12} = 2k_3s_{\theta}$$

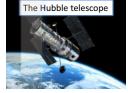
$$\Rightarrow \vec{k} = \begin{bmatrix} k_1 \\ k_2 \\ k_3 \end{bmatrix} = \frac{1}{2s_{\theta}} \begin{bmatrix} r_{32} - r_{23} \\ r_{13} - r_{31} \\ r_{21} - r_{12} \end{bmatrix}$$

Angle-Axis - Example

A satellite orbiting the earth can be made to point it's telescope at a desired star by performing the following motions

- 1. Rotate about it's *x*-axis by -30° , then
- 2. Rotate about it's new *z*-axis by 50° , then finally
- 3. Rotate about it's initial *y*-axis by 40° .

is its final orientation wrt the starting orientation?



What

 $C_{final}^{start} = R_{(\vec{y},40^{\circ})}R_{(\vec{x},-30^{\circ})}R_{(\vec{z},50^{\circ})}$

	0.766044	0	0.642788	1	1	0	0	1	0.642788	-0.766044	0
=	0	1	0		0	0.866025	0.5		0.766044	0.642788	0
	-0.642788	0	0.766044		0	-0.5	0.866025	5	0	0	1
=	$\begin{bmatrix} 0.246202 \\ 0.663414 \\ -0.706588 \end{bmatrix}$	0.	.793412 663414 246202		- 556 0.5 2462						

Angle-Axis - Example

- In order to save energy it is desirable to perform this change in orientation with only one rotation — How?
- Perform a single, equivalent angle-axis rotation with

$$\theta = \cos^{-1} \left(\frac{Tr\left(C_{final}^{start}\right) - 1}{2} \right) = 76.5^{\circ}$$
$$\vec{k} = \frac{1}{2s_{\theta}} \begin{bmatrix} r_{32} - r_{23} \\ r_{13} - r_{31} \\ r_{21} - r_{12} \end{bmatrix} = \begin{bmatrix} -0.130495 \\ 0.649529 \\ 0.749055 \end{bmatrix}$$

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Angle-Axis - Three Parameters

Angle-Axis representation can be made three parameters via

$$\vec{K} = \theta \vec{k}$$

such that

and

$$\vec{k} = \frac{\vec{K}}{\|\vec{K}\|}$$

 $\theta = \|\vec{K}\|$

4 Quaternions

Quaternions - Singularity Problems

Euler angles, RPY angles and angle-axis consist three elements, but they are not unique, e.g., there are orientations that are represented by different Euler angles, RYP angles and angle-axis.

Quaternion

- Quaternions are 4-element representation of the rotation vectors where the additional element makes quaternions unique.
- With 4 elements quaternions have the lowest dimensionality possible for a globally nonsingular attitude representation.

Quaternions

Given an angle-axis pair (θ, \vec{k}) or the corresponding rotation vector $\vec{K} = \theta \vec{k}$, a quaternion is defined as

$$\bar{q} = \begin{bmatrix} q_s \\ \vec{q} \end{bmatrix} = \begin{bmatrix} q_s \\ q_x \\ q_y \\ q_z \end{bmatrix} = \begin{bmatrix} \cos(\frac{\theta}{2}) \\ \vec{k}\sin(\frac{\theta}{2}) \end{bmatrix}$$

where

- $q_s = \cos(\frac{\theta}{2})$ is the scalar component
- $\vec{q} = [q_x, q_y, q_z]^T = \vec{k} \sin(\frac{\theta}{2})$ is the vector component

•
$$|\bar{q}| = \sqrt{q_s^2 + q_x^2 + q_y^2 + q_z^2} = \sqrt{(\cos(\frac{\theta}{2}))^2 + (k_1\sin(\frac{\theta}{2}))^2 + (k_2\sin(\frac{\theta}{2}))^2 + (k_3\sin(\frac{\theta}{2}))^2} = 1 \Rightarrow a \text{ unit quaternion}$$

Quaternions

Quaternions can be used to describe orientation and compose rotations like rotation matrices

•
$$C^a_b \Leftrightarrow \bar{q}^a_b$$

• $C_f^{i} = \hat{R}_2 R_1 R_3 \Leftrightarrow \bar{q}_f^{i} = \bar{q}_2 \otimes \bar{q}_1 \otimes \bar{q}_3$

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Quaternions - Properties

• Quaternion inverse or conjugate

$$\bar{q}^{-1} = \bar{q}^* = \begin{bmatrix} q_s \\ -q_x \\ -q_y \\ -q_z \end{bmatrix}$$

• Vector transformation (change of coordinates) Define a "pure" vector

 $\breve{v} = \begin{bmatrix} 0\\ \vec{v} \end{bmatrix}$

then a vector \vec{v}^{p} written in the *p*-frame may be transformed to the *i*-frame using

$$\check{v}^i = \bar{q} \otimes \check{v}^p \otimes \bar{q}^{-1}$$

Quaternions - Multiplication

Quaternion multiplication - first type \otimes

$$\bar{r} = \bar{q} \otimes \bar{p} = [\bar{q} \otimes] \bar{p} = \begin{bmatrix} q_s p_s - \vec{q} \cdot \vec{p} \\ q_s \vec{p} + p_s \vec{q} + \vec{q} \times \vec{p} \end{bmatrix}$$

where implementation via matrix multiplication achieved by defining

$$[\bar{q}\otimes] = \begin{bmatrix} q_s & -q_x & -q_y & -q_z \\ q_x & q_s & -q_z & q_y \\ q_y & q_z & q_s & -q_x \\ q_z & -q_y & q_x & q_s \end{bmatrix}$$

Note multiplication does not commute.

Quaternions - Multiplication

Quaternion multiplication – second type \circledast (useful to re-order multiplication when certain factorizations and coordinatizations needed)

$$\bar{r} = \bar{q} \circledast \bar{p} = [\bar{q} \circledast] \bar{p} = \begin{bmatrix} q_s p_s - \vec{q} \cdot \vec{p} \\ q_s \vec{p} + p_s \vec{q} \\ - \end{bmatrix} \vec{q} \times \vec{p}$$

where

 $\bar{q}\otimes\bar{p}=\bar{p}\circledast\bar{q}$

and

$$[\bar{q}\circledast] = \begin{bmatrix} q_s & -q_x & -q_y & -q_z \\ q_x & q_s & q_z & -q_y \\ q_y & -q_z & q_s & q_x \\ q_z & q_y & -q_x & q_s \end{bmatrix}$$

Quaternion to Rotation Matrix

Rotation matrix from given quaternion

$$\begin{aligned} R_{\bar{q}} &= (q_s^2 - |\vec{q}|^2)\mathcal{I} + 2q_s[\vec{q}\times] + 2\vec{q}\vec{q}\vec{T} = \\ &= \begin{bmatrix} q_s^2 + q_x^2 - q_y^2 - q_z^2 & 2(q_xq_y - q_sq_z) & 2(q_xq_z + q_sq_y) \\ 2(q_xq_y + q_sq_z) & q_s^2 - q_x^2 + q_y^2 - q_z^2 & 2(q_yq_z - q_sq_x) \\ 2(q_xq_z - q_sq_y) & 2(q_yq_z + q_sq_x) & q_s^2 - q_x^2 - q_y^2 + q_z^2 \end{bmatrix} \end{aligned}$$

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Quaternion from Rotation Matrix

Quaternion from given rotation matrix

$$R_{\bar{q}} = \begin{bmatrix} q_s^2 + q_x^2 - q_y^2 - q_z^2 & 2(q_x q_y - q_s q_z) & 2(q_x q_z + q_s q_y) \\ 2(q_x q_y + q_s q_z) & q_s^2 - q_x^2 + q_y^2 - q_z^2 & 2(q_y q_z - q_s q_x) \\ 2(q_x q_z - q_s q_y) & 2(q_y q_z + q_s q_x) & q_s^2 - q_x^2 - q_y^2 + q_z^2 \end{bmatrix}$$
$$= \begin{bmatrix} r_{11} & r_{12} & r_{13} \\ r_{21} & r_{22} & r_{23} \\ r_{31} & r_{32} & r_{33} \end{bmatrix} = R_{desired}$$
$$q_s = \frac{1}{2}\sqrt{1 + r_{11} + r_{22} + r_{33}} \text{ and } \vec{q} = \frac{1}{4q_s} \begin{bmatrix} r_{32} - r_{23} \\ r_{13} - r_{31} \\ r_{21} - r_{12} \end{bmatrix}$$

Quaternions - Identities

 \Rightarrow

Identities for quaternions

$$[\bar{q}^{-1}\otimes] = [\bar{q}\otimes]^{-1} = [\bar{q}\otimes]^{T}$$
$$[\bar{q}^{-1}\otimes] = [\bar{q}\otimes]^{-1} = [\bar{q}\otimes]^{T}$$
$$[\bar{q}\otimes] = e^{\frac{1}{2}[\check{k}\otimes]} = \cos(\theta/2)\mathcal{I} + \frac{1}{2}[\check{k}\otimes]\frac{\sin(\theta/2)}{\theta/2}$$
$$[\bar{q}\otimes] = e^{\frac{1}{2}[\check{k}\otimes]} = \cos(\theta/2)\mathcal{I} + \frac{1}{2}[\check{k}\otimes]\frac{\sin(\theta/2)}{\theta/2}$$
$$[\bar{q}\otimes] = e^{\frac{1}{2}[\check{k}\otimes]} = \cos(\theta/2)\mathcal{I} + \frac{1}{2}[\check{k}\otimes]\frac{\sin(\theta/2)}{\theta/2}$$
$$[\bar{q}\otimes][\bar{q}\otimes]^{-1} = [\bar{q}\otimes]^{-1}[\bar{q}\otimes] = \begin{bmatrix} 1 & 0\\ 0 & \mathcal{T}(\bar{q}) \end{bmatrix}$$

Quaternions - Identities

$$\begin{split} \bar{q} \otimes \bar{p} \otimes \bar{r} &= (\bar{q} \otimes \bar{p}) \otimes \bar{r} = \bar{q} \otimes (\bar{p} \otimes \bar{r}) \\ \bar{q} \circledast \bar{p} \circledast \bar{r} &= (\bar{q} \circledast \bar{p}) \circledast \bar{r} = \bar{q} \circledast (\bar{p} \circledast \bar{r}) \\ (\bar{q} \circledast \bar{p}) \otimes \bar{r} \neq \bar{q} \circledast (\bar{p} \otimes \bar{r}) \\ (\bar{q} \otimes \bar{p}) \circledast \bar{r} \neq \bar{q} \otimes (\bar{p} \circledast \bar{r}) \end{split}$$

The End

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