EE 565: Position, Navigation and Timing

Navigation Equations: ECI Mechanization

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ECI Mechanization



- Determine the position, velocity and attitude of the body frame wrt the inertial frame
 - **Position** Vector from the origin of the inertial frame to the origin of the body frame resolved in the inertial frame: \vec{r}_{ib}^i
 - **Velocity** Velocity of the body frame *wrt* the inertial frame resolved in the inertial frame: \vec{v}_{ib}^i
 - Attitude Orientation of the body frame wrt the inertial frame: C_b^i or \bar{q}_b^i

ECI Mechanization

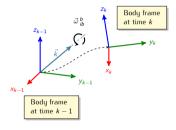


- Determine the position, velocity and attitude of the body frame wrt the inertial frame
 - **Position** Vector from the origin of the inertial frame to the origin of the body frame resolved in the inertial frame: \vec{r}_{ib}^i
 - **Velocity** Velocity of the body frame wrt the inertial frame resolved in the inertial frame: \vec{v}_{ib}^{i}
 - Attitude Orientation of the body frame wrt the inertial frame: C_b^i or \bar{q}_b^i
- The inputs are $\vec{\omega}_{ib}^{\ b}$ and $\vec{f}_{ib}^{\ b}$



• Body orientation frame at time "k" wrt time "k-1"

$$\dot{C}_b^i = C_b^i \Omega_{ib}^b$$

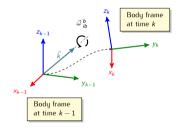




- Body orientation frame at time "k" wrt time "k-1"

$$\dot{C}_b^i = C_b^i \Omega_{ib}^b$$

$$= \lim_{\Delta t \to 0} \left(\frac{C_b^i(k) - C_b^i(k-1)}{\Delta t} \right) = C_b^i(k-1)\Omega_{ib}^b$$



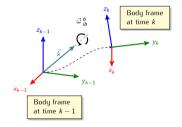


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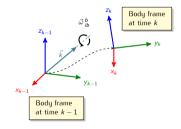
$$C_b^i(+) - C_b^i(-) \approx C_b^i(-)\Omega_{ib}^b \Delta t$$





• Body orientation frame at time "k" wrt time "k-1"

$$\begin{split} \dot{C}_b^i &= C_b^i \Omega_{ib}^b \\ &= \lim_{\Delta t \to 0} \left(\frac{C_b^i(k) - C_b^i(k-1)}{\Delta t} \right) = C_b^i(k-1) \Omega_{ib}^b \\ &C_b^i(+) - C_b^i(-) \approx C_b^i(-) \Omega_{ib}^b \Delta t \\ &C_b^i(+) \approx C_b^i(-) \left(\mathcal{I} + \Omega_{ib}^b \Delta t \right) \end{split}$$

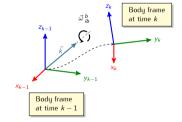




- Body orientation frame at time "k" wrt time "k-1"

$$C_{b(k)}^{i} = C_{b(k-1)}^{i} C_{b(k)}^{b(k-1)}$$

$$\vec{\omega}_{ib}^{\ b} \Delta t = \vec{k} \Delta \theta$$



•

$$\mathfrak{K} = [\vec{k} \times]$$

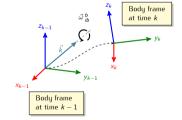


- Body orientation frame at time "k" wrt time "k-1"

$$C_{b(k)}^{i} = C_{b(k-1)}^{i} C_{b(k)}^{b(k-1)}$$

$$C_{b(k)}^{b(k-1)} = e^{\Omega_{ib}^b \Delta t} = e^{\Re \Delta \theta}$$

$$\vec{\omega}_{ib}^{\ b} \Delta t = \vec{k} \Delta \theta$$



$$\mathfrak{K} = [\vec{k} \times]$$

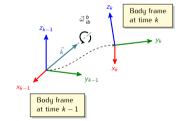


- Body orientation frame at time "k" wrt time "k-1"

$$C_{b(k)}^{i} = C_{b(k-1)}^{i} C_{b(k)}^{b(k-1)}$$

$$\vec{\omega}_{ib}^{\ b} \Delta t = \vec{k} \Delta \theta$$

$$egin{align} \mathcal{C}_{b(k)}^{b(k-1)} &= e^{\Omega_{ib}^b \Delta t} = e^{\mathfrak{K} \Delta heta} \ &= \mathcal{I} + \mathfrak{K} \Delta heta + rac{\mathfrak{K}^2 \Delta heta^2}{2!} + rac{\mathfrak{K}^3 \Delta heta^3}{3!} + \dots \end{split}$$



$$\mathfrak{K} = [\vec{k} \times]$$

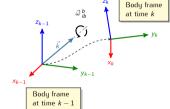


- Body orientation frame at time "k" wrt time "k-1"

$$C_{b(k)}^i=C_{b(k-1)}^iC_{b(k)}^{b(k-1)}$$
 $C_{b(k)}^{b(k-1)}=e^{\Omega_{ib}^b\Delta t}=e^{\Re\Delta heta}$

$$\vec{\omega}_{ib}^{\ b} \Delta t = \vec{k} \Delta \theta$$

$$= \mathcal{I} + \mathfrak{K}\Delta\theta + \frac{\mathfrak{K}^2\Delta\theta^2}{2!} + \frac{\mathfrak{K}^3\Delta\theta^3}{3!} + \dots$$
$$= \mathcal{I} + \sin(\Delta\theta)\mathfrak{K} + [1 - \cos(\Delta\theta)]\mathfrak{K}^2$$



$$\mathfrak{K} = [\vec{k} \times]$$



Body frame at time k

- Body orientation frame at time "k" wrt time "k-1"

$$C_{b(k)}^{i} = C_{b(k-1)}^{i} C_{b(k)}^{b(k-1)}$$

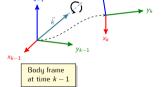
$$C_{b(k)}^{b(k-1)} = e^{\Omega_{ib}^{b} \Delta t} = e^{\Re \Delta \theta}$$

$$= \mathcal{I} + \Re \Delta \theta + \frac{\Re^{2} \Delta \theta^{2}}{2!} + \frac{\Re^{3} \Delta \theta^{3}}{3!} + \dots$$

$$= \mathcal{I} + \sin(\Delta \theta) \Re + [1 - \cos(\Delta \theta)] \Re^{2}$$

$$C_{b}^{i}(+) = C_{b}^{i}(-) C_{b(k)}^{b(k-1)}$$

$$\vec{\omega}_{ib}^{\ b} \Delta t = \vec{k} \Delta \theta$$



$$\mathfrak{K} = [\vec{k} \times]$$



- Body orientation frame at time "k" wrt time "k-1"

$$C_{b(k)}^{i} = C_{b(k-1)}^{i} C_{b(k)}^{b(k-1)}$$

$$C_{b(k)}^{b(k-1)} = e^{\Omega_{ib}^{b} \Delta t} = e^{\Re \Delta \theta}$$

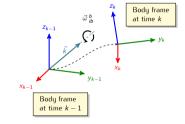
$$= \mathcal{I} + \Re \Delta \theta + \frac{\Re^{2} \Delta \theta^{2}}{2!} + \frac{\Re^{3} \Delta \theta^{3}}{3!} + \dots$$

$$= \mathcal{I} + \sin(\Delta \theta) \Re + [1 - \cos(\Delta \theta)] \Re^{2}$$

$$C_{b}^{i}(+) = C_{b}^{i}(-) C_{b(k)}^{b(k-1)}$$

$$\approx C_{b}^{i}(-) \left(\mathcal{I} + \Omega_{ib}^{b} \Delta t\right)$$

$$\vec{\omega}_{ib}^{\ b} \Delta t = \vec{k} \Delta \theta$$



$$\mathfrak{K} = [\vec{k} \times]$$



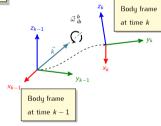
- Body orientation frame at time "k" wrt time "k-1"
 - $egin{aligned} oldsymbol{\Delta} t &= t_k t_{k-1} \ ar{q}^{~i}_{~b(k)} &= ar{q}^{~i}_{~b(k-1)} \otimes ar{q}^{~b(k-1)}_{~b(k)} \end{aligned}$

$$ar{q}_{b(k)}^{b(k-1)} = egin{bmatrix} \cos(rac{\Delta heta}{2}) \ ec{k}\sin(rac{\Delta heta}{2}) \end{bmatrix}$$

$$ar{q}_{b}^{i}(+)=ar{q}_{b}^{i}(-)\otimesar{q}_{b(k)}^{b(k-1)}$$

Need to periodically renormalize \bar{q}

$$\vec{\omega}_{ib}^{\ b} \Delta t = \vec{k} \Delta \theta$$



Attitude Update— Summary



$$\vec{\omega}_{ib}^{\ b} \Delta t = \vec{k} \Delta \theta$$

$$\mathfrak{K} = [\vec{k} \times]$$

High fidelity

$$C_b^i(+) = C_b^i(-) \left[\mathcal{I} + \sin(\Delta \theta) \mathfrak{K} + \left[1 - \cos(\Delta \theta) \right] \mathfrak{K}^2 \right] \tag{1}$$

or

$$\bar{q}_{b}^{i}(+) = \bar{q}_{b}^{i}(-) \otimes \begin{bmatrix} \cos(\frac{\Delta\theta}{2}) \\ \vec{k}\sin(\frac{\Delta\theta}{2}) \end{bmatrix}$$
 (2)

Low fidelity

$$C_b^i(+) \approx C_b^i(-) \left(\mathcal{I} + \Omega_{ib}^b \Delta t \right)$$
 (3)

Steps 2-4



- Specific force transformation
 - Simply coordinatize the specific force

$$\vec{f}_{ib}^{i} = C_{b}^{i}(+)\vec{f}_{ib}^{b}$$
 (4)

Steps 2-4



- Specific force transformation
 - Simply coordinatize the specific force

$$\vec{f}_{ib}^{i} = C_{b}^{i}(+)\vec{f}_{ib}^{b}$$
 (4)

- Velocity update
 - Assuming that we are in space (i.e., no centrifugal component)

$$\vec{f}_{ib}^{i} = \vec{a}_{ib}^{i} - \vec{\gamma}_{ib}^{i}$$

$$\vec{a}_{ib}^{i} = \vec{f}_{ib}^{i} + \vec{\gamma}_{ib}^{i}$$

• Thus, by simple numerical integration

$$\vec{v}_{ib}^{i}(+) = \vec{v}_{ib}^{i}(-) + \vec{a}_{ib}^{i} \Delta t$$
 (6)

(5)

Steps 2-4



- Specific force transformation
 - Simply coordinatize the specific force

$$\vec{f}_{ib}^{i} = C_{b}^{i}(+)\vec{f}_{ib}^{b} \tag{4}$$

- Velocity update
 - Assuming that we are in space (i.e., no centrifugal component)

$$\vec{f}_{ib}^{i} = \vec{a}_{ib}^{i} - \vec{\gamma}_{ib}^{i}$$

$$\vec{a}_{ib}^{i} = \vec{f}_{ib}^{i} + \vec{\gamma}_{ib}^{i}$$

• Thus, by simple numerical integration

$$\vec{v}_{ib}^{i}(+) = \vec{v}_{ib}^{i}(-) + \vec{a}_{ib}^{i}\Delta t$$
 (6)

- Position update
 - by simple numerical integration

$$\vec{r}_{ib}^{i}(+) = \vec{r}_{ib}^{i}(-) + \vec{v}_{ib}^{i}(-)\Delta t + \vec{a}_{ib}^{i} \frac{\Delta t^{2}}{2}$$
 (7)

(5)

ECI Mechanization Summary



$$C_b^i(+) = C_b^i(-) \left[\mathcal{I} + \sin(\Delta \theta) \mathfrak{K} + \left[1 - \cos(\Delta \theta) \right] \mathfrak{K}^2 \right]$$

or

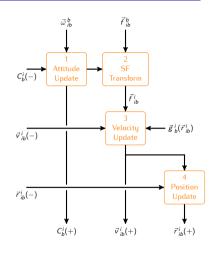
$$C_b^i(+) pprox C_b^i(-) \left(\mathcal{I} + \Omega_{ib}^b \Delta t\right)$$

or

$$ar{q}_{b}^{i}(+) = ar{q}_{b}^{i}(-) \otimes egin{bmatrix} \cos(rac{\Delta heta}{2}) \ ec{k}\sin(rac{\Delta heta}{2}) \end{bmatrix}$$

and

$$\begin{split} \vec{f}_{ib}^{i} &= C_{b}^{i}(+)\vec{f}_{ib}^{b} \\ \vec{a}_{ib}^{i} &= \vec{f}_{ib}^{i} + \vec{\gamma}_{ib}^{i} \\ \vec{v}_{ib}^{i}(+) &= \vec{v}_{ib}^{i}(-) + \vec{a}_{ib}^{i} \Delta t \\ \vec{r}_{ib}^{i}(+) &= \vec{r}_{ib}^{i}(-) + \vec{v}_{ib}^{i}(-) \Delta t + \vec{a}_{ib}^{i} \frac{\Delta t^{2}}{2} \end{split}$$



ECI Mechanization Summary



$$C_b^i(+) = C_b^i(-) \left[\mathcal{I} + \sin(\Delta \theta) \mathfrak{K} + \left[1 - \cos(\Delta \theta) \right] \mathfrak{K}^2 \right]$$

or

$$C_b^i(+) pprox C_b^i(-) \left(\mathcal{I} + \Omega_{ib}^b \Delta t\right)$$

or

$$ar{q}_{b}^{i}(+) = ar{q}_{b}^{i}(-) \otimes egin{bmatrix} \cos(rac{\Delta heta}{2}) \ \vec{k}\sin(rac{\Delta heta}{2}) \end{bmatrix}$$

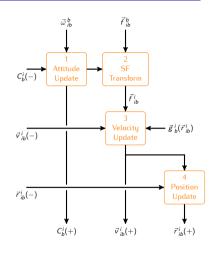
and

$$\vec{f}_{ib}^{i} = C_{b}^{i}(+)\vec{f}_{ib}^{b}$$

$$\vec{a}_{ib}^{i} = \vec{f}_{ib}^{i} + \vec{\gamma}_{ib}^{i}$$

$$\vec{v}_{ib}^{i}(+) = \vec{v}_{ib}^{i}(-) + \vec{a}_{ib}^{i}\Delta t$$

$$\vec{r}_{ib}^{i}(+) = \vec{r}_{ib}^{i}(-) + \vec{v}_{ib}^{i}(-)\Delta t + \vec{a}_{ib}^{i}\frac{\Delta t^{2}}{2}$$



What is the importance of Δt ?

ECI Mechanization — Continuous Case



- In continuous time notation
 - Attitude: $\dot{C}_b^i = C_b^i \Omega_{ib}^b$ or $\dot{\bar{q}}_b^i = \frac{1}{2} [\breve{\omega}_{ib}^b \circledast] \bar{q}_b^i(t)$
 - Velocity: $\dot{\vec{v}}_{ib}^{\ i} = C_b^i \vec{f}_{ib}^{\ b} + \vec{\gamma}_{ib}^{\ i}$
 - Position: $\dot{\vec{r}}_{ib}^{i} = \vec{v}_{ib}^{i}$
- In State-space notation

$$\begin{bmatrix} \vec{r}_{ib}^{\ i} \\ \dot{\vec{v}}_{ib}^{\ i} \\ \dot{C}_{b}^{\ i} \end{bmatrix} = \begin{bmatrix} \vec{v}_{ib}^{\ i} \\ C_{b}^{\ i} \vec{f}_{ib}^{\ b} + \vec{\gamma}_{ib}^{\ i} \\ C_{b}^{\ i} \Omega_{ib}^{\ b} \end{bmatrix}$$

or

$$\begin{bmatrix} \vec{r}_{ib}^i \\ \dot{\vec{v}}_{ib}^i \\ \dot{\bar{q}}_b^i \end{bmatrix} = \begin{bmatrix} \vec{v}_{ib}^i \\ C_b^i \vec{f}_{ib}^b + \vec{\gamma}_{ib}^i \\ \frac{1}{2} [\breve{\omega}_{ib}^b \circledast] \bar{q}_b^i(t) \end{bmatrix}$$

Appendix



$$[ar{q}\otimes] = egin{bmatrix} q_s & -q_x & -q_y & -q_z \ q_x & q_s & -q_z & q_y \ q_y & q_z & q_s & -q_x \ q_z & -q_y & q_x & q_s \end{bmatrix}$$

$$[\bar{q}\circledast] = egin{bmatrix} q_s & -q_x & -q_y & -q_z \ q_x & q_s & q_z & -q_y \ q_y & -q_z & q_s & q_x \ q_z & q_y & -q_x & q_s \end{bmatrix}$$