EE 565: Position, Navigation and Timing

Navigation Equations: ECI Mechanization

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ECI Mechanization



- Determine the position, velocity and attitude of the body frame wrt the inertial frame
 - **Position** Vector from the origin of the inertial frame to the origin of the body frame resolved in the inertial frame: \vec{r}_{ib}^i
 - **Velocity** Velocity of the body frame *wrt* the inertial frame resolved in the inertial frame: \vec{v}_{ib}^{i}
 - Attitude Orientation of the body frame wrt the inertial frame: C_b^i or \bar{q}_b^i

ECI Mechanization

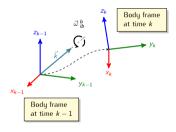


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 - **Velocity** Velocity of the body frame *wrt* the inertial frame resolved in the inertial frame: \vec{v}_{ib}^{i}
 - Attitude Orientation of the body frame wrt the inertial frame: C_b^i or \bar{q}_b^i
- The inputs are $\vec{\omega}_{ib}^{\ b}$ and $\vec{f}_{ib}^{\ b}$



• Body orientation frame at time "k" wrt time "k-1"

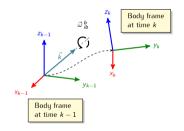
$$\dot{C}_b^i = C_b^i \Omega_{ib}^b$$





- Body orientation frame at time "k" wrt time "k-1"

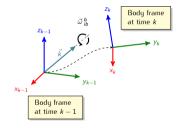
$$\dot{C}_b^i = C_b^i \Omega_{ib}^b
= \lim_{\Delta t \to 0} \left(\frac{C_b^i(k) - C_b^i(k-1)}{\Delta t} \right) = C_b^i(k-1)\Omega_{ib}^b$$





- Body orientation frame at time "k" wrt time "k-1"

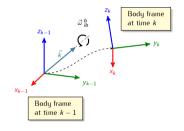
$$egin{aligned} \dot{C}_b^i &= C_b^i \Omega_{ib}^b \ &= \lim_{\Delta t o 0} \left(rac{C_b^i(k) - C_b^i(k-1)}{\Delta t}
ight) = C_b^i(k-1) \Omega_{ib}^b \ &C_b^i(+) - C_b^i(-) pprox C_b^i(-) \Omega_{ib}^b \Delta t \end{aligned}$$





- Body orientation frame at time "k" wrt time "k-1"

$$\begin{split} \dot{C}_b^i &= C_b^i \Omega_{ib}^b \\ &= \lim_{\Delta t \to 0} \left(\frac{C_b^i(k) - C_b^i(k-1)}{\Delta t} \right) = C_b^i(k-1) \Omega_{ib}^b \\ &C_b^i(+) - C_b^i(-) \approx C_b^i(-) \Omega_{ib}^b \Delta t \\ &C_b^i(+) \approx C_b^i(-) \left(\mathcal{I} + \Omega_{ib}^b \Delta t \right) \end{split}$$

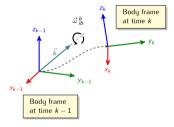




- Body orientation frame at time "k" wrt time "k-1"

$$C_{b(k)}^{i} = C_{b(k-1)}^{i} C_{b(k)}^{b(k-1)}$$

$$\vec{\omega}_{ib}^{\ b} \Delta t = \vec{k} \Delta \theta$$



$$\Re = [\vec{k} \times]$$

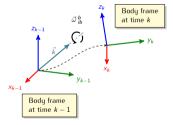


- Body orientation frame at time "k" wrt time "k-1"

$$C_{b(k)}^{i} = C_{b(k-1)}^{i} C_{b(k)}^{b(k-1)}$$

$$C_{b(k)}^{b(k-1)} = e^{\Omega_{ib}^b \Delta t} = e^{\mathfrak{K}\Delta \theta}$$

$$\vec{\omega}_{ib}^{\ b} \Delta t = \vec{k} \Delta \theta$$



$$\mathfrak{K} = [\vec{k} \times]$$

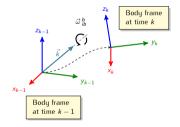


- Body orientation frame at time "k" wrt time "k-1"

$$C_{b(k)}^{i} = C_{b(k-1)}^{i} C_{b(k)}^{b(k-1)}$$

$$\vec{\omega}_{ib}^{\ b} \Delta t = \vec{k} \Delta \theta$$

$$egin{aligned} C_{b(k)}^{b(k-1)} &= e^{\Omega_{ib}^b \Delta t} = e^{\mathfrak{K} \Delta heta} \ &= \mathcal{I} + \mathfrak{K} \Delta heta + rac{\mathfrak{K}^2 \Delta heta^2}{2!} + rac{\mathfrak{K}^3 \Delta heta^3}{3!} + \dots \end{aligned}$$



$$\mathfrak{K} = [\vec{k} \times]$$

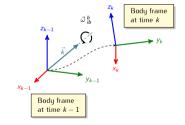


- Body orientation frame at time "k" wrt time "k-1"

$$C_{b(k)}^{i} = C_{b(k-1)}^{i} C_{b(k)}^{b(k-1)}$$

$$\vec{\omega}_{ib}^{\,b} \Delta t = \vec{k} \Delta \theta$$

$$egin{aligned} C_{b(k)}^{b(k-1)} &= \mathrm{e}^{\Omega_{ib}^b \Delta t} = \mathrm{e}^{\mathfrak{K}\Delta heta} \ &= \mathcal{I} + \mathfrak{K}\Delta heta + rac{\mathfrak{K}^2 \Delta heta^2}{2!} + rac{\mathfrak{K}^3 \Delta heta^3}{3!} + \dots \ &= \mathcal{I} + \sin(\Delta heta)\mathfrak{K} + \left[1 - \cos(\Delta heta)\right]\mathfrak{K}^2 \end{aligned}$$



$$\mathfrak{K} = [\vec{k} \times]$$



- Body orientation frame at time "k" wrt time "k-1"

$$C_{b(k)}^{i} = C_{b(k-1)}^{i} C_{b(k)}^{b(k-1)}$$

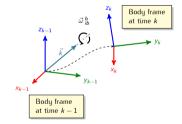
$$\vec{\omega}_{ib}^{\ b} \Delta t = \vec{k} \Delta \theta$$

$$C_{b(k)}^{b(k-1)} = e^{\Omega_{ib}^b \Delta t} = e^{\mathfrak{K}\Delta \theta}$$

$$= \mathcal{I} + \mathfrak{K}\Delta \theta + \frac{\mathfrak{K}^2 \Delta \theta^2}{2!} + \frac{\mathfrak{K}^3 \Delta \theta^3}{3!} + \dots$$

$$= \mathcal{I} + \sin(\Delta \theta) \mathfrak{K} + [1 - \cos(\Delta \theta)] \mathfrak{K}^2$$

$$C_b^i(+) = C_b^i(-) C_{b(k)}^{b(k-1)}$$



$$\mathfrak{K} = [\vec{k} \times]$$



- Body orientation frame at time "k" wrt time "k-1"

$$C^{i}_{b(k)} = C^{i}_{b(k-1)} C^{b(k-1)}_{b(k)}$$

$$\vec{\omega}_{ib}^{\ b} \Delta t = \vec{k} \Delta \theta$$

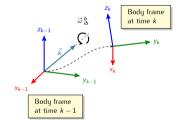
$$C_{b(k)}^{b(k-1)} = e^{\Omega_{ib}^{b}\Delta t} = e^{\Re \Delta \theta}$$

$$= \mathcal{I} + \Re \Delta \theta + \frac{\Re^{2}\Delta \theta^{2}}{2!} + \frac{\Re^{3}\Delta \theta^{3}}{3!} + \dots$$

$$= \mathcal{I} + \sin(\Delta \theta)\Re + [1 - \cos(\Delta \theta)]\Re^{2}$$

$$C_{b}^{i}(+) = C_{b}^{i}(-)C_{b(k)}^{b(k-1)}$$

$$\approx C_{b}^{i}(-)\left(\mathcal{I} + \Omega_{ib}^{b}\Delta t\right)$$



$$\mathfrak{K} = [\vec{k} \times]$$



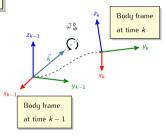
• Body orientation frame at time "k" wrt time "k-1"

$$\begin{array}{c} \bullet \ \Delta t = t_k - t_{k-1} \\ \bar{q}^{\,i}_{\,b(k)} = \bar{q}^{\,i}_{\,b(k-1)} \otimes \bar{q}^{\,b(k-1)}_{\,b(k)} \\ \\ \bar{q}^{\,b(k-1)}_{\,b(k)} = \begin{bmatrix} \cos(\frac{\Delta\theta}{2}) \\ \vec{k}\sin(\frac{\Delta\theta}{2}) \end{bmatrix} \end{array}$$

 $ar{q}_{\ b}^{\ i}(+) = ar{q}_{\ b}^{\ i}(-) \otimes ar{q}_{\ b(k)}^{\ b(k-1)}$

Need to periodically renormalize $ar{q}$

$$\vec{\omega}_{ib}^{\ b} \Delta t = \vec{k} \Delta \theta$$



Attitude Update— Summary



$$\vec{\omega}_{ib}^{\ b} \Delta t = \vec{k} \Delta \theta$$

$$\mathfrak{K}=[\vec{k}\times]$$

High fidelity

$$C_b^i(+) = C_b^i(-) \left[\mathcal{I} + \sin(\Delta\theta) \mathfrak{K} + \left[1 - \cos(\Delta\theta) \right] \mathfrak{K}^2 \right] \tag{1}$$

or

$$\bar{q}_{b}^{i}(+) = \bar{q}_{b}^{i}(-) \otimes \begin{bmatrix} \cos(\frac{\Delta\theta}{2}) \\ \vec{k}\sin(\frac{\Delta\theta}{2}) \end{bmatrix}$$
 (2)

Low fidelity

$$C_b^i(+) \approx C_b^i(-) \left(\mathcal{I} + \Omega_{ib}^b \Delta t \right)$$
 (3)

Steps 2-4



- Specific force transformation
 - Simply coordinatize the specific force

$$\vec{f}_{ib}^{i} = C_{b}^{i}(+)\vec{f}_{ib}^{b} \tag{4}$$

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- Specific force transformation
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$$\vec{f}_{ib}^{i} = C_{b}^{i}(+)\vec{f}_{ib}^{b} \tag{4}$$

- Velocity update
 - Assuming that we are in space (i.e., no centrifugal component)

$$\vec{f}_{ib}^{i} = \vec{a}_{ib}^{i} - \vec{\gamma}_{ib}^{i}$$

$$ec{a}_{ib}^{i}=ec{f}_{ib}^{i}+ec{\gamma}_{ib}^{i}$$

• Thus, by simple numerical integration

$$ec{v}_{ib}^{\ i}(+) = ec{v}_{ib}^{\ i}(-) + ec{s}_{ib}^{\ i}\Delta t$$

(5)

(6)

Steps 2-4



- Specific force transformation
 - Simply coordinatize the specific force

$$\vec{f}_{ib}^{i} = C_{b}^{i}(+)\vec{f}_{ib}^{b} \tag{4}$$

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 - Assuming that we are in space (i.e., no centrifugal component)

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• Thus, by simple numerical integration

gration
$$ec{v}_{ib}^{\ i}(+)=ec{v}_{ib}^{\ i}(-)+ec{a}_{ib}^{\ i}\Delta t$$
 (6)

- Position update
 - by simple numerical integration

$$\vec{r}_{ib}^{i}(+) = \vec{r}_{ib}^{i}(-) + \vec{v}_{ib}^{i}(-)\Delta t + \vec{a}_{ib}^{i} \frac{\Delta t^{2}}{2}$$
(7)

(5)

ECI Mechanization Summary



$$C_b^i(+) = C_b^i(-) \left[\mathcal{I} + \sin(\Delta \theta) \mathfrak{K} + \left[1 - \cos(\Delta \theta) \right] \mathfrak{K}^2 \right]$$

or

$$C_b^i(+) pprox C_b^i(-) \left(\mathcal{I} + \Omega_{ib}^b \Delta t\right)$$

or

$$ar{q}_{b}^{i}(+) = ar{q}_{b}^{i}(-) \otimes egin{bmatrix} \cos(rac{\Delta heta}{2}) \ \vec{k}\sin(rac{\Delta heta}{2}) \end{bmatrix}$$

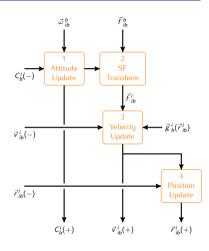
and

$$\vec{f}_{ib}^{i} = C_{b}^{i}(+)\vec{f}_{ib}^{b}$$

$$\vec{a}_{ib}^{i} = \vec{f}_{ib}^{i} + \vec{\gamma}_{ib}^{i}$$

$$\vec{v}_{ib}^{i}(+) = \vec{v}_{ib}^{i}(-) + \vec{a}_{ib}^{i}\Delta t$$

$$\vec{r}_{ib}^{i}(+) = \vec{r}_{ib}^{i}(-) + \vec{v}_{ib}^{i}(-)\Delta t + \vec{a}_{ib}^{i}\frac{\Delta t^{2}}{2}$$



ECI Mechanization Summary



$$C_b^i(+) = C_b^i(-) \left[\mathcal{I} + \sin(\Delta \theta) \mathfrak{K} + \left[1 - \cos(\Delta \theta) \right] \mathfrak{K}^2 \right]$$

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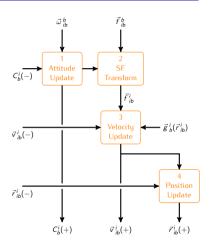
$$C_b^i(+) pprox C_b^i(-) \left(\mathcal{I} + \Omega_{ib}^b \Delta t\right)$$

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$$\begin{split} \vec{f}_{ib}^{i} &= C_{b}^{i}(+)\vec{f}_{ib}^{b} \\ \vec{a}_{ib}^{i} &= \vec{f}_{ib}^{i} + \vec{\gamma}_{ib}^{i} \\ \vec{v}_{ib}^{i}(+) &= \vec{v}_{ib}^{i}(-) + \vec{a}_{ib}^{i} \Delta t \\ \vec{r}_{ib}^{i}(+) &= \vec{r}_{ib}^{i}(-) + \vec{v}_{ib}^{i}(-) \Delta t + \vec{a}_{ib}^{i} \frac{\Delta t^{2}}{2} \end{split}$$



What is the importance of Δt ?

ECI Mechanization — Continuous Case



- In continuous time notation
 - Attitude: $\dot{C}_b^i = C_b^i \Omega_{ib}^b$ or $\dot{\bar{q}}_b^i = \frac{1}{2} [\breve{\omega}_{ib}^b \circledast] \bar{q}_b^i(t)$
 - Velocity: $\dot{\vec{v}}_{ib}^{i} = C_b^i \vec{f}_{ib}^{b} + \vec{\gamma}_{ib}^{i}$
 - Position: $\dot{\vec{r}}_{ib}^{i} = \vec{v}_{ib}^{i}$
- In State-space notation

$$\begin{bmatrix} \vec{r}_{ib}^i \\ \dot{\vec{v}}_{ib}^i \\ \dot{C}_b^i \end{bmatrix} = \begin{bmatrix} \vec{v}_{ib}^i \\ C_b^i \vec{f}_{ib}^b + \vec{\gamma}_{ib}^i \\ C_b^i \Omega_{ib}^b \end{bmatrix}$$

or

$$\begin{bmatrix} \vec{r}_{ib}^{i} \\ \dot{\vec{v}}_{ib}^{i} \\ \dot{\bar{q}}_{b}^{i} \end{bmatrix} = \begin{bmatrix} \vec{v}_{ib}^{i} \\ C_{b}^{i} \vec{f}_{ib}^{b} + \vec{\gamma}_{ib}^{i} \\ \frac{1}{2} [\breve{\omega}_{ib}^{b} \circledast] \bar{q}_{b}^{i}(t) \end{bmatrix}$$

Appendix



$$[ar{q} \otimes] = egin{bmatrix} q_s & -q_x & -q_y & -q_z \ q_x & q_s & -q_z & q_y \ q_y & q_z & q_s & -q_x \ q_z & -q_y & q_x & q_s \end{bmatrix}$$

$$[ar{q}\circledast] = egin{bmatrix} q_s & -q_x & -q_y & -q_z \ q_x & q_s & q_z & -q_y \ q_y & -q_z & q_s & q_x \ q_z & q_y & -q_x & q_s \end{bmatrix}$$