

EE 565: Position, Navigation and Timing

Navigation Equations: Tangential Mechanization

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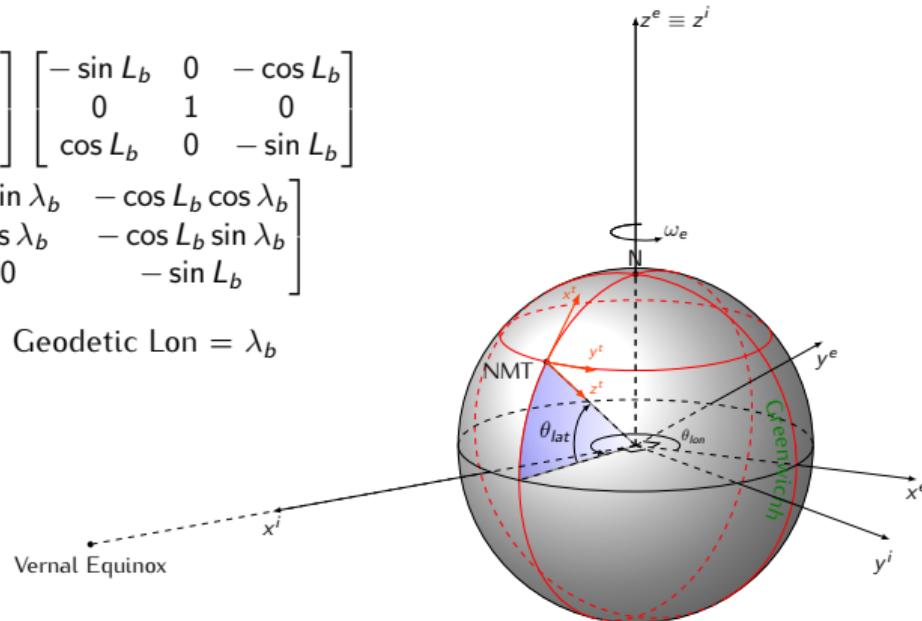
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- Determine the position, velocity and attitude of the **body** frame *wrt* the **tangential** frame.
 - **Position** — Vector from the origin of the tangential frame to the origin of the body frame resolved in the tangential frame: \vec{r}_{tb}^t
 - **Velocity** — Velocity of the body frame *wrt* the tangential frame resolved in the tangential frame: \vec{v}_{tb}^t
 - **Attitude** — Orientation of the body frame *wrt* the tangential frame: C_b^t

- Description of the tangential frame
 - Orientation of the t -frame wrt the e -frame

$$\begin{aligned}
C_t^e &= R_{(\vec{z}, \lambda_b)} R_{(\vec{y}, -L_b - 90^\circ)} \\
&= \begin{bmatrix} \cos \lambda_b & -\sin \lambda_b & 0 \\ \sin \lambda_b & \cos \lambda_b & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} -\sin L_b & 0 & -\cos L_b \\ 0 & 1 & 0 \\ \cos L_b & 0 & -\sin L_b \end{bmatrix} \\
&= \begin{bmatrix} -\sin L_b \cos \lambda_b & -\sin \lambda_b & -\cos L_b \cos \lambda_b \\ -\sin L_b \sin \lambda_b & \cos \lambda_b & -\cos L_b \sin \lambda_b \\ \cos L_b & 0 & -\sin L_b \end{bmatrix}
\end{aligned}$$

where geodetic Lat = L_b and Geodetic Lon = λ_b



Attitude — Method A

- Body orientation frame at time “ k ” wrt time “ $k - 1$ ”
 - $\Delta t = t_k - t_{k-1}$
- Start with angular velocity

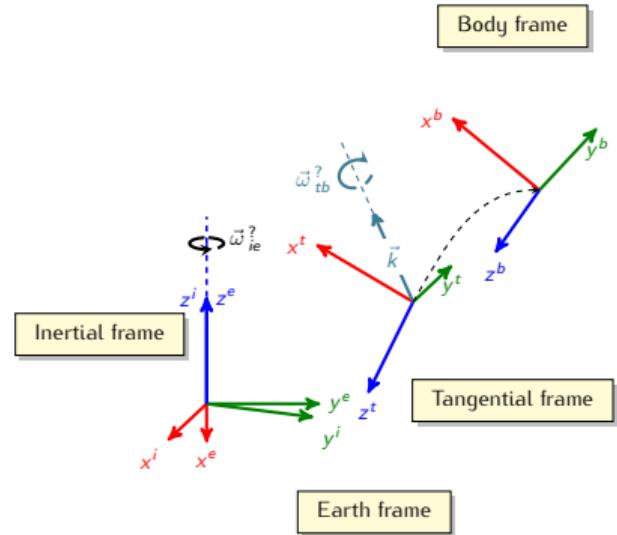
$$\vec{\omega}_{ib}^t = \vec{\omega}_{ie}^t + \vec{\omega}_{et}^t + \vec{\omega}_{tb}^t$$

$$\vec{\omega}_{tb}^t = C_b^t \vec{\omega}_{ib}^b - C_e^t \vec{\omega}_{ie}^e$$

$$\Omega_{tb}^t = C_b^t \Omega_{ib}^b C_t^b - C_e^t \Omega_{ie}^e C_t^e$$

$$C_b^t(+) - C_b^t(-) \approx \Delta t \Omega_{tb}^t C_b^t(-)$$

$$\begin{aligned} C_b^t(+) &\approx C_b^t(-) + \Delta t \left(C_b^t \Omega_{ib}^b C_t^b - C_e^t \Omega_{ie}^e C_t^e \right) C_b^t(-) \\ &= C_b^t(-) \left(\mathcal{I} + \Omega_{ib}^b \Delta t \right) - \Omega_{ie}^t C_b^t(-) \Delta t \end{aligned}$$



Attitude — Method B

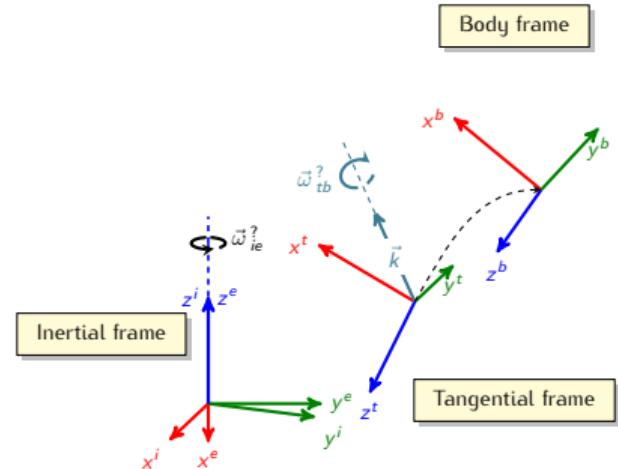
- Body orientation frame at time "k" wrt time "k - 1"
 - $\Delta t = t_k - t_{k-1}$
- Start with the angular velocity

$$\Omega_{tb}^t = C_b^t \Omega_{ib}^b C_t^b - \Omega_{ie}^t$$

$$C_b^t(+) = C_b^t(-) e^{\Omega_{tb}^t \Delta t} = e^{\Omega_{tb}^t \Delta t} C_b^t(-)$$

$$C_b^t(+) = [\mathcal{I} + \sin(\Delta\theta)\hat{\kappa} + [1 - \cos(\Delta\theta)]\hat{\kappa}^2] C_b^t(-)$$

$$e^{\Omega_{tb}^t \Delta t} = e^{\hat{\kappa}\theta}$$



- Body orientation frame at time “ k ” wrt time “ $k - 1$ ”

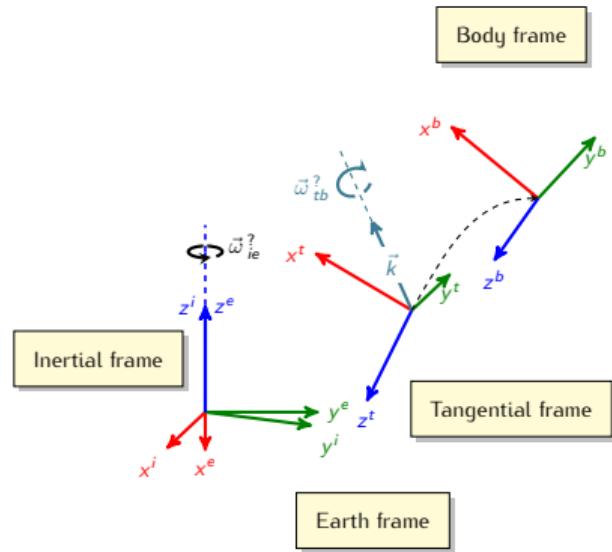
- $\Delta t = t_k - t_{k-1}$

$$\vec{\omega}_{tb}^t \Delta t = \vec{k} \Delta \theta$$

$$\bar{q}_b^t(+) = \Delta \bar{q}_b^t \otimes \bar{q}_b^t(-)$$

$$\Delta \bar{q}_b^t = \begin{bmatrix} \cos(\frac{\Delta \theta}{2}) \\ \vec{k} \sin(\frac{\Delta \theta}{2}) \end{bmatrix}$$

Need to periodically renormalize \bar{q}



$$\vec{\omega}_{tb}^t \Delta t = \vec{k} \Delta \theta$$

$$\mathfrak{K} = [\vec{k} \times]$$

- High fidelity

$$C_b^t(+) = [\mathcal{I} + \sin(\Delta\theta)\mathfrak{K} + [1 - \cos(\Delta\theta)]\mathfrak{K}^2] C_b^t(-) \quad (1)$$

or

$$\bar{q}_b^t(+) = \begin{bmatrix} \cos(\frac{\Delta\theta}{2}) \\ \vec{k} \sin(\frac{\Delta\theta}{2}) \end{bmatrix} \otimes \bar{q}_b^t(-) \quad (2)$$

- Low fidelity

$$C_b^t(+) \approx C_b^t(-) \left(\mathcal{I} + \Omega_{ib}^b \Delta t \right) - \Omega_{ie}^t C_b^t(-) \Delta t \quad (3)$$

② Specific force transformation

- Simply coordinatize the specific force

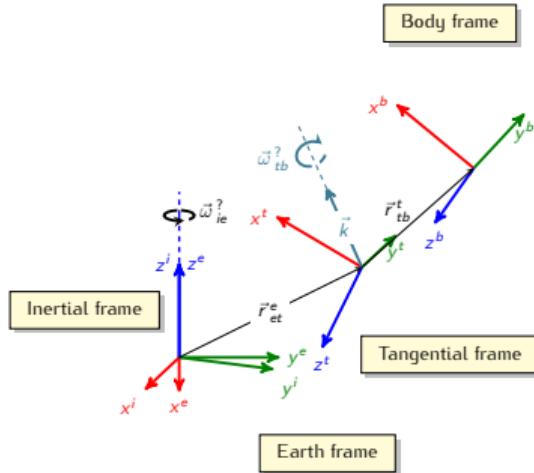
$$\vec{f}_{ib}^t = C_b^t (+) \vec{f}_{ib}^b \quad (4)$$

③ Velocity update

~~$\vec{r}_{ib}^i = \vec{r}_{ie}^i + C_e^i \vec{r}_{et}^e + C_t^i \vec{r}_{tb}^t$~~

$$\Rightarrow \vec{r}_{tb}^t = C_i^t \vec{r}_{ib}^i - C_e^t \vec{r}_{et}^e$$

$$\begin{aligned}\vec{v}_{tb}^t &= \dot{\vec{r}}_{tb}^t \\ &= \dot{C}_i^t \vec{r}_{ib}^i + C_i^t \dot{\vec{r}}_{ib}^i \\ &= \Omega_{ei}^t C_i^t \vec{r}_{ib}^i + C_i^t \vec{v}_{ib}^i \\ &= -\Omega_{ie}^t (\vec{r}_{et}^t + \vec{r}_{tb}^t) + C_i^t \vec{v}_{ib}^i\end{aligned}$$



Steps 2–4

$$\begin{aligned}
 \vec{a}_{tb}^t &= \dot{\vec{v}}_{tb}^t = \frac{d}{dt} (-\Omega_{ie}^t (\vec{r}_{et}^t + \vec{r}_{tb}^t) + C_i^t \vec{v}_{ib}^i) \\
 &= -\Omega_{ie}^t \dot{\vec{r}}_{tb}^t + C_i^t \vec{v}_{ib}^i + C_i^t \dot{\vec{v}}_{ib}^i \\
 &= -\Omega_{ie}^t \vec{v}_{tb}^t + \Omega_{ti}^t C_i^t \vec{v}_{ib}^i + C_i^t \vec{a}_{ib}^i \\
 &= -\Omega_{ie}^t \vec{v}_{tb}^t - \Omega_{it}^t [\vec{v}_{tb}^t + \Omega_{ie}^t (\vec{r}_{et}^t + \vec{r}_{tb}^t)] + C_i^t \vec{a}_{ib}^i \\
 &= -2\Omega_{ie}^t \vec{v}_{tb}^t - \Omega_{ie}^t \Omega_{ie}^t \vec{r}_{eb}^t + \vec{a}_{ib}^t \\
 &= -2\Omega_{ie}^t \vec{v}_{tb}^t + \vec{f}_{ib}^t + \vec{g}_b^t
 \end{aligned}$$

$$\begin{aligned}
 \vec{v}_{tb}^t(+) &= \vec{v}_{tb}^t(-) + \vec{a}_{tb}^t \Delta t \\
 &= \vec{v}_{tb}^t(-) + [\vec{f}_{ib}^t + \vec{g}_b^t - 2\Omega_{ie}^t \vec{v}_{tb}^t(-)] \Delta t \quad (5)
 \end{aligned}$$

$$\dot{\vec{r}}_{et}^t = 0$$

$$\vec{\omega}_{it}^t = \vec{\omega}_{ie}^t$$

$$C_i^t \vec{v}_{ib}^i = \Omega_{ie}^t (\vec{r}_{et}^t + \vec{r}_{tb}^t) + \vec{v}_{tb}^t$$

$$\vec{f}_{ib}^? = \vec{a}_{ib}^? - \vec{\gamma}_{ib}^?$$

$$\vec{a}_{ib}^t = \vec{f}_{ib}^t + \vec{\gamma}_{ib}^t$$

$$\vec{g}_b^t = \vec{\gamma}_{ib}^t - \Omega_{ie}^t \Omega_{ie}^t \vec{r}_{eb}^t$$

$$\vec{a}_{ib}^t = \vec{f}_{ib}^t + \vec{g}_b^t + \Omega_{ie}^t \Omega_{ie}^t \vec{r}_{eb}^t$$

4 Position update

- by simple numerical integration

$$\vec{r}_{tb}^t(+) = \vec{r}_{tb}^t(-) + \vec{v}_{tb}^t(-)\Delta t + \vec{a}_{tb}^t \frac{\Delta t^2}{2} \quad (6)$$

Tangential Mechanization Summary

$$C_b^t(+) = [\mathcal{I} + \sin(\Delta\theta)\hat{\kappa} + [1 - \cos(\Delta\theta)]\hat{\kappa}^2] C_b^t(-)$$

or

$$\bar{q}_b^t(+) = \begin{bmatrix} \cos(\frac{\Delta\theta}{2}) \\ \vec{k} \sin(\frac{\Delta\theta}{2}) \end{bmatrix} \otimes \bar{q}_b^t(-)$$

or

$$C_b^t(+) \approx C_b^t(-) \left(\mathcal{I} + \Omega_{ib}^b \Delta t \right) - \Omega_{ie}^t C_b^t(-) \Delta t$$

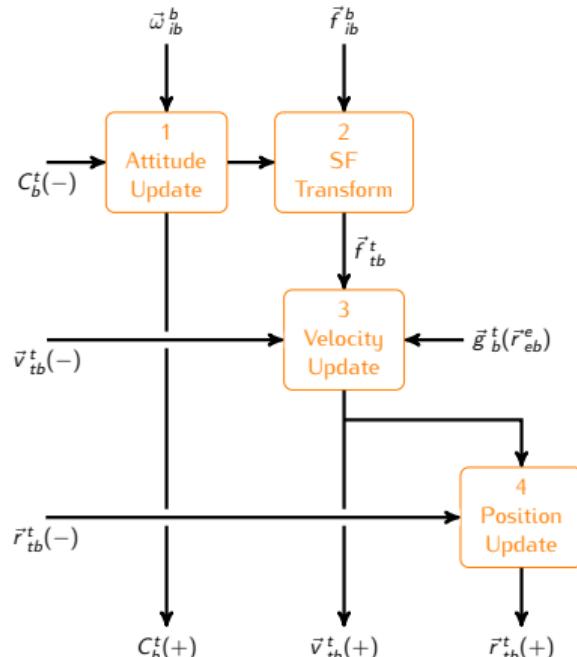
and

$$\vec{f}_{ib}^t = C_b^t(+) \vec{f}_{ib}^b$$

$$\vec{a}_{tb}^t = -2\Omega_{ie}^t \vec{v}_{tb}^t + \vec{f}_{ib}^t + \vec{g}_b^t$$

$$\vec{v}_{tb}^t(+) = \vec{v}_{tb}^t(-) + \left[\vec{f}_{ib}^t + \vec{g}_b^t - 2\Omega_{ie}^t \vec{v}_{tb}^t(-) \right] \Delta t$$

$$\vec{r}_{tb}^t(+) = \vec{r}_{tb}^t(-) + \vec{v}_{tb}^t(-) \Delta t + \vec{a}_{tb}^t \frac{\Delta t^2}{2}$$



- In continuous time notation

- Attitude: $\dot{C}_b^t = C_b^t \Omega_{tb}^b$ or $\dot{\bar{q}}_b^t = \frac{1}{2}[\vec{\omega}_{tb}^b \otimes] \bar{q}_b^t(t)$
- Velocity: $\dot{\vec{v}}_{tb}^t = C_b^t \vec{f}_{ib}^b + \vec{g}_b^t - 2\Omega_{ie}^t \vec{v}_{tb}^t$
- Position: $\dot{\vec{r}}_{ib}^t = \vec{v}_{tb}^t$

$$\vec{\omega}_{ib}^b = \vec{\omega}_{ie}^b + \vec{\omega}_{tb}^b$$

- In State-space notation

$$\Omega_{tb}^b = \Omega_{ib}^b - \Omega_{ie}^b$$

$$\begin{bmatrix} \dot{\vec{r}}_{tb}^t \\ \dot{\vec{v}}_{tb}^t \\ \dot{C}_b^t \end{bmatrix} = \begin{bmatrix} \vec{v}_{tb}^t \\ C_b^t \vec{f}_{ib}^b + \vec{g}_b^t - 2\Omega_{ie}^t \vec{v}_{tb}^t \\ C_b^t \Omega_{tb}^b \end{bmatrix} \quad (7)$$

or

$$\begin{bmatrix} \dot{\vec{r}}_{tb}^t \\ \dot{\vec{v}}_{tb}^t \\ \dot{\bar{q}}_b^t \end{bmatrix} = \begin{bmatrix} \vec{v}_{tb}^t \\ C_b^t \vec{f}_{ib}^b + \vec{g}_b^t - 2\Omega_{ie}^t \vec{v}_{tb}^t \\ \frac{1}{2}[\vec{\omega}_{tb}^b \otimes] \bar{q}_b^t(t) \end{bmatrix} \quad (8)$$

$$[\bar{q} \otimes] = \begin{bmatrix} q_s & -q_x & -q_y & -q_z \\ q_x & q_s & -q_z & q_y \\ q_y & q_z & q_s & -q_x \\ q_z & -q_y & q_x & q_s \end{bmatrix}$$

$$[\bar{q} \circledast] = \begin{bmatrix} q_s & -q_x & -q_y & -q_z \\ q_x & q_s & q_z & -q_y \\ q_y & -q_z & q_s & q_x \\ q_z & q_y & -q_x & q_s \end{bmatrix}$$