

1-2 $\vec{A} = 5\vec{a}_x + 3\vec{a}_y + 4\vec{a}_z$, $\vec{B} = 2\vec{a}_y + \vec{a}_z$, $\vec{C} = -6\vec{a}_z$

a) $\vec{D} = \vec{A} + \vec{B} + \vec{C} = 5\vec{a}_x + 5\vec{a}_y - \vec{a}_z$

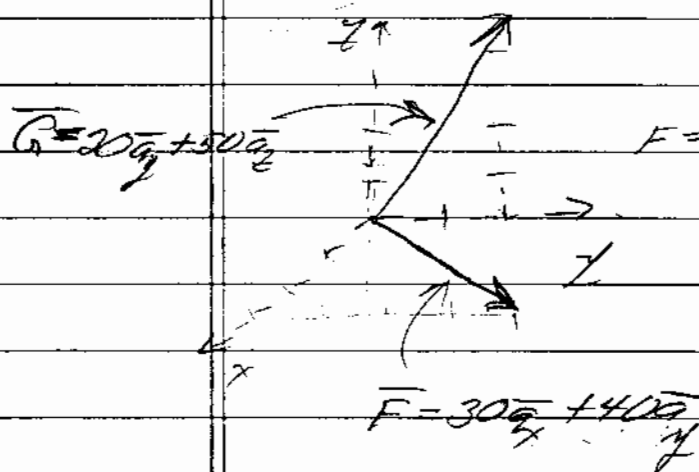
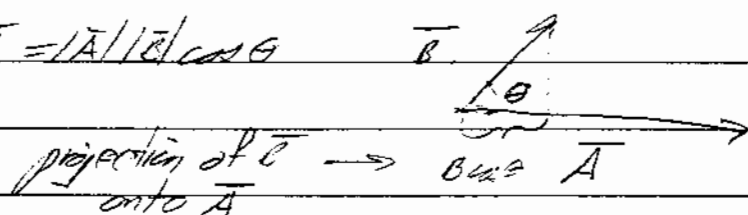
b) $|\vec{A}| = \sqrt{25+9+16} = 7.07$

$|\vec{D}| = \sqrt{25+25+1} = 7.14$

c) $2\vec{A} - \vec{C} = \vec{E} = 10\vec{a}_x + 6\vec{a}_y + 14\vec{a}_z$

$|\vec{E}| = \sqrt{100+36+196} = 18.22$

1-8 $\vec{A} \cdot \vec{B} = |\vec{A}| |\vec{B}| \cos \theta$



$\vec{F} \cdot \vec{G} = 800 = FG \cos \theta$

$F = 50$

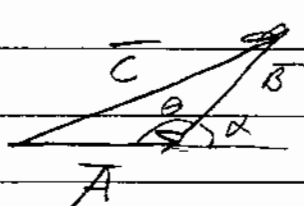
but $G = \sqrt{400+2500} = 53.85$

$\therefore \cos \theta = \frac{800}{53.85} = 14.85$

$\cos \theta = \frac{800}{FG} = 0.297$

$\boxed{50 \theta = 72.72^\circ}$

1-11



$\vec{A} + \vec{B} = \vec{C}$

$\vec{C} \cdot \vec{C} = (\vec{A} + \vec{B}) \cdot (\vec{A} + \vec{B}) = A^2 + B^2 + 2AB \cos \alpha$

but $\alpha = 180^\circ - \theta$

so $\cos \alpha = \cos(\pi - \theta)$

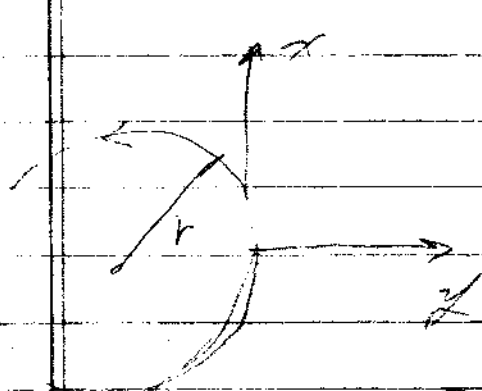
$= -\cos \theta$

$= -\cos \theta$

$\therefore \vec{C} \cdot \vec{C} = C^2 = \boxed{A^2 + B^2 - 2AB \cos \theta}$

1-25 $q = -e$, $\vec{v} = 10^5 \hat{a}_x$, $\vec{B} = 10^{-4} \hat{a}_z$

$$\vec{F} = q(\vec{E} + \vec{v} \times \vec{B})$$

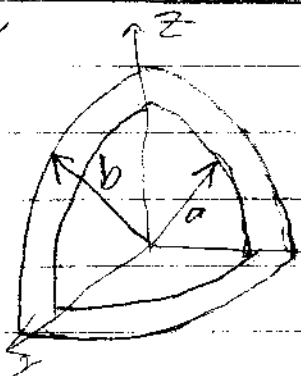


Constant $\vec{E}$ and $\vec{v}$ produces a circular trajectory with $r = \frac{mv^2}{F}$

$$\therefore r = \frac{9.1 \times 10^{-31} \times 10^{10}}{1.6 \times 10^{-19} \times 10^5 \times 10^{-4}} = 5.69 \times 10^{-3} \text{ m}$$

for no deflection $\vec{E} = -\vec{v} \times \vec{B} = -10^5 \hat{a}_x \times 10^{-4} \hat{a}_z = 10 \hat{a}_y$

1-28



$$\oint \vec{E} \cdot d\vec{s} = \oint \rho_v dV$$

$\vec{E} = E_r(r) \hat{a}_r$ from symmetry

for $r < a$ $\rho_v = 0$

$$\therefore 4\pi r^2 \epsilon_0 E_r = 0 \text{ or } E_r = 0$$

for $a < r < b$ $4\pi r^2 \epsilon_0 E_r = \rho_v \int_0^{2\pi} \int_0^\pi \int_a^r r'^2 \sin\theta' d\theta' d\phi' dr' = \left(\frac{r^3 - a^3}{3}\right) 4\pi \rho_v$

$$\therefore E_r = \frac{\rho_v}{3\epsilon_0 r^2} (r^3 - a^3)$$

for $r > b$ $4\pi r^2 \epsilon_0 E_r = \left(\frac{r^3 - a^3}{3}\right) 4\pi \rho_v$

$$\text{or } E_r = \frac{\rho_v}{3\epsilon_0 r^2} (b^3 - a^3)$$

1-29 for $r < a$ $\rho_v = \rho_0(1+kr)$

$q_{\text{total}} = \text{total charge} = \int_{r=0}^a \int_{\phi=0}^{2\pi} \int_{\theta=0}^{\pi} \rho_0(1+kr) r^2 \sin\theta d\theta d\phi dr$

$q_{\text{total}} = \frac{4}{3}\pi a^3 \rho_0 + k\rho_0 \frac{a^4}{4} 4\pi = 0$ when $\frac{1}{3} = -\frac{k a}{4}$ or $k = -\frac{4}{3a}$

for $r > a$ in this case Gauss's law gives.

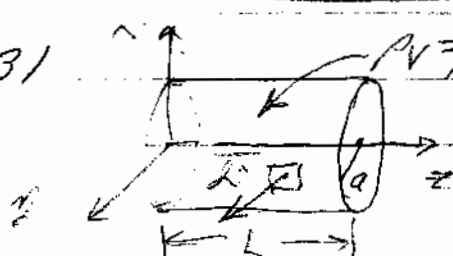
$\epsilon_0 E_r 4\pi r^2 = 0 \implies E_r = 0$

for $r < a$ $\epsilon_0 E_r 4\pi r^2 = \int_{r=0}^r \int_{\phi=0}^{2\pi} \int_{\theta=0}^{\pi} \rho_0(1-\frac{4r}{3a}) r^2 \sin\theta d\theta d\phi dr$

$= 4\pi \rho_0 \left[\frac{r^3}{3} - \frac{4r^4}{4 \cdot 3a} \right]$

so $E_r = \frac{\rho_0}{\epsilon_0} \left[\frac{r}{3} - \frac{r^2}{3a} \right]$

1-31



$\rho = \rho_0 \left(\frac{a}{r} \right)^2$

$Q = \int_{z=0}^L \int_{\phi=0}^{2\pi} \int_{\rho=0}^a \rho_0 \left(\frac{a}{r} \right)^2 r \rho dr d\phi dz$

$Q = L \int_{\phi=0}^{2\pi} \int_{\rho=0}^a \frac{\rho_0}{a^2} \cdot \frac{a^4}{r^2} = \rho_0 L \frac{\pi a^2}{2}$

Gauss's law $\rho > a$ $\int_{\phi=0}^{2\pi} \int_{z=0}^L \epsilon_0 E_p dz d\phi = Q = \epsilon_0 E_p L \rho 2\pi$

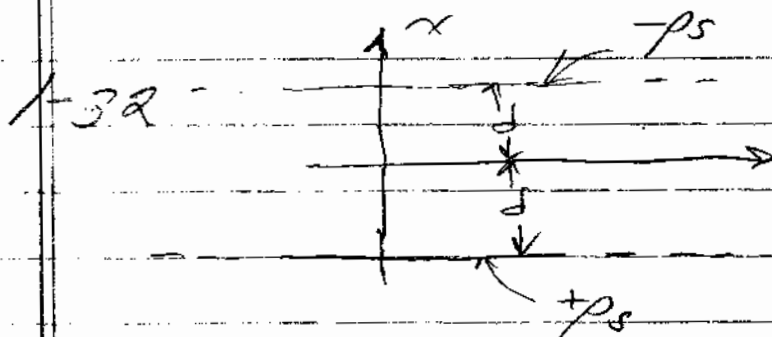
so $E_p = \frac{Q}{2\pi \epsilon_0 \rho L} = \frac{\rho_0 a^2}{4\pi \epsilon_0 \rho} = \frac{\rho_0 a^2}{4\epsilon_0 \rho}$

or $E_p = \frac{\rho_0}{2\pi \epsilon_0 \rho}$

for $\rho < a$ $\int_{\phi=0}^{2\pi} \int_{z=0}^L \epsilon_0 E_p dz d\phi = \int_{z=0}^L \int_{\phi=0}^{2\pi} \int_{\rho=0}^{\rho} \rho_0 \left(\frac{a}{r} \right)^2 r \rho dr d\phi dz$

or $\epsilon_0 E_p \rho 2\pi = \rho_0 \frac{\pi a^2}{2}$

so $E_p = \frac{\rho_0 a^3}{4\epsilon_0 a^2}$



- a) between the charged sheets both sheets produce a constant E_x in the positive x direction

$$\text{for } -d < x < d \quad E_x = \frac{\rho_s}{\epsilon_0} \quad \leftarrow$$

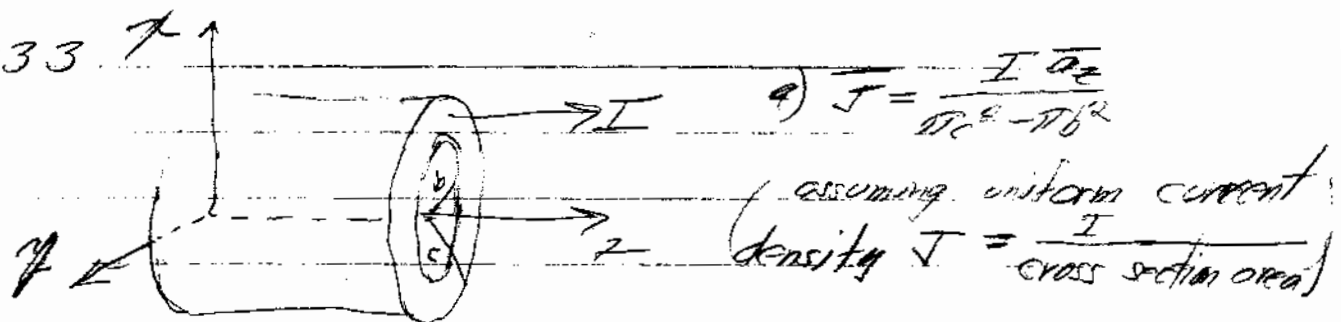
for $x > d$ or $x < -d$ fields cancel so $E_x = 0 \quad \leftarrow$

- b) both sheets positively charged

$$x > d \quad E_x = \frac{\rho_s}{\epsilon_0}$$

$$x < -d \quad E_x = -\frac{\rho_s}{\epsilon_0} \quad \leftarrow$$

$$-d < x < d \quad E_x = 0$$

1-33 $\uparrow$ 

b) $\oint \frac{\vec{B}}{\mu_0} \cdot d\vec{l} = I$ for $\rho > c$

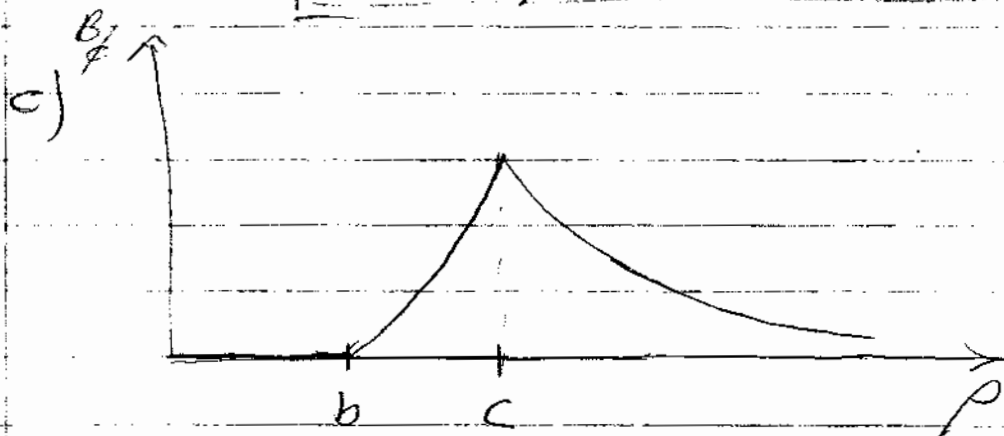
$$\int_{\phi=0}^{2\pi} \frac{B_{\phi}}{\mu_0} \rho d\phi = I \quad \text{or} \quad B_{\phi} = \frac{\mu_0 I}{2\pi \rho} \quad \text{for } \rho > c$$

for $\rho < b$ $2\pi \rho \frac{B_{\phi}}{\mu_0} = 0$ or $B_{\phi} = 0$

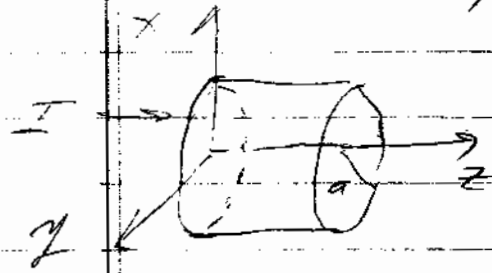
for $b < \rho < c$ $2\pi \rho \frac{B_{\phi}}{\mu_0} = \int_{\phi=0}^{2\pi} \int_{\rho=b}^{\rho} \frac{I \vec{a}_z}{\pi c^2 - \pi b^2} \cdot \rho d\phi d\rho$

or $2\pi \rho \frac{B_{\phi}}{\mu_0} = \frac{2\pi I}{\pi(c^2 - b^2)} \cdot \frac{\rho^2}{2} \Big|_b^{\rho} = I \frac{\rho^2 - b^2}{c^2 - b^2}$

so $B_{\phi} = \frac{\mu_0 I}{2\pi \rho} \left[\frac{\rho^2 - b^2}{c^2 - b^2} \right] \quad b < \rho < c$



1-35 from Example 1-15



$$B_\phi = \frac{\mu_0 I}{2\pi p} \quad \text{for } p > b$$

$$B_\phi = \frac{\mu_0 I p}{2\pi (b^2 - a^2)} \quad \text{for } p < a$$

Using our solution to problem 1-30 and superposition we have

$$B_\phi = \frac{\mu_0 I p}{2\pi (b^2 - a^2)} \quad \text{for } p < a$$

$$B_\phi = \frac{\mu_0 I}{2\pi p} \quad \text{for } a < p < b$$

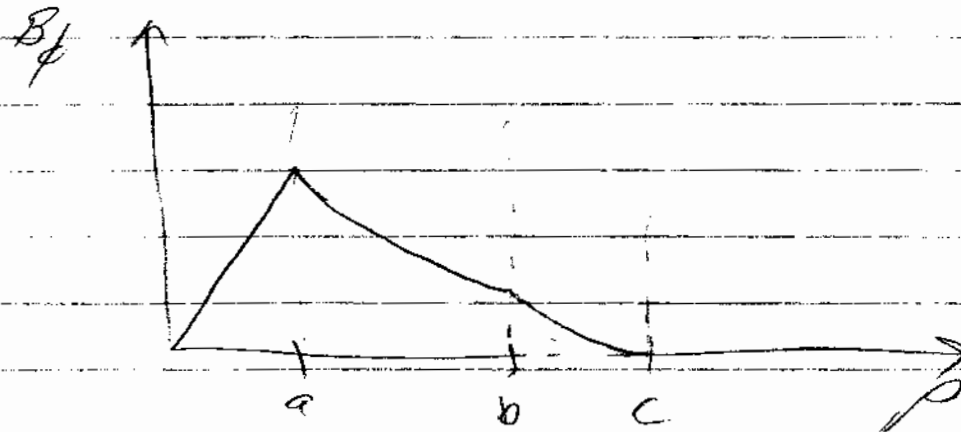
$$B_\phi = \frac{\mu_0 I}{2\pi p} - \frac{\mu_0 I}{2\pi p} \left[\frac{p^2 - b^2}{c^2 - b^2} \right] = \frac{\mu_0 I}{2\pi p} \left[\frac{c^2 - b^2 - p^2 + b^2}{c^2 - b^2} \right]$$

$$B_\phi = \frac{\mu_0 I}{2\pi p} \left[\frac{c^2 - p^2}{c^2 - b^2} \right] \quad b < p < c$$

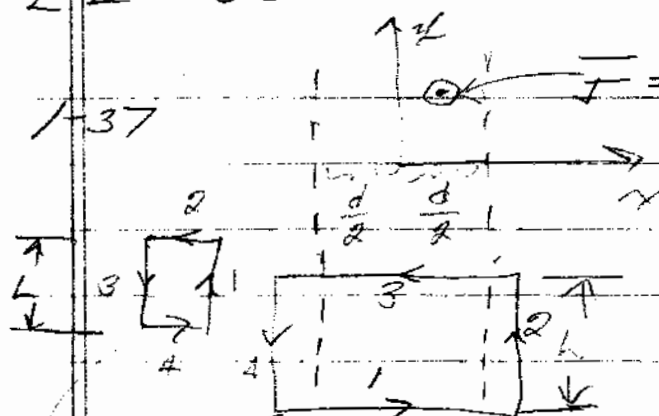
Same as
answer for
1-34

$$B_\phi = 0 \quad \text{for } p > c$$

(no current enclosed)



1-37



$$\vec{J} = J_z \hat{a}_z$$

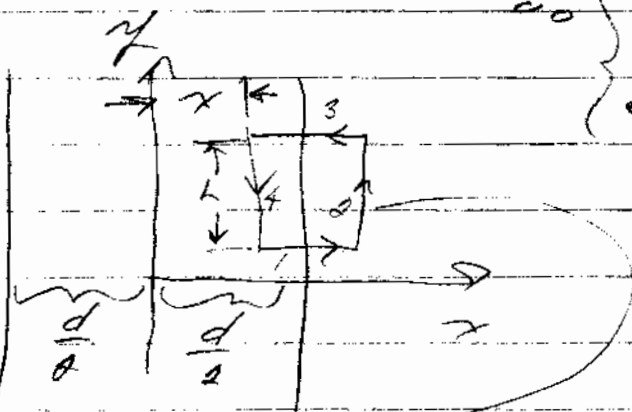
From direct current problem we know that $\vec{B}$ is only in the $\pm y$ direction

for this contour

$$\frac{B_{y1}}{\mu_0} l - \frac{B_{y2}}{\mu_0} l = 0 \quad \text{so} \quad \begin{cases} B_y = \text{constant} \\ \text{outside of slab} \end{cases}$$

$$\frac{B_{y1}}{\mu_0} l + \frac{B_{y2}}{\mu_0} l = J_z l d$$

$$\begin{cases} B_{y1} = \frac{\mu_0 J_z d}{2} & \text{for } x > d \\ B_{y2} = -\frac{\mu_0 J_z d}{2} & \text{for } x < -d \end{cases}$$



$$\frac{\mu_0 J_z d}{\mu_0} l - \frac{B_{y4}}{\mu_0} l = J_z l \left(\frac{d}{2} - x \right)$$

$$\text{so } B_{y4} = \frac{\mu_0 J_z d}{2} - \mu_0 J_z \left(\frac{d}{2} - x \right) = \mu_0 J_z x \quad \text{for } x < \frac{d}{2}$$

$$2-17 \quad \vec{E} = \frac{\rho_0}{\epsilon_0} \left(\frac{r}{3} - \frac{r^2}{3a} \right) \hat{a}_r$$

$$\nabla \cdot \vec{E} = \frac{1}{r^2} \frac{d}{dr} \left[\frac{\rho_0}{\epsilon_0} \left(\frac{r^3}{3} - \frac{r^4}{3a} \right) \right] = \frac{\rho_0}{r^2 \epsilon_0} \left[r^2 - \frac{4r^3}{3a} \right]$$

$$\text{or } \nabla \cdot \vec{E} = \frac{\rho_v}{\epsilon_0}$$

2-41 $\vec{E}_x^+ = 1885 e^{-j\beta_0 z}$ $f = 10^8$

- a) amplitude = 1885 V/m
 traveling in +z direction
 vector direction $\vec{a}_x$ (x polarization)

b) $E_x = 1885 \cos(\omega t - \beta_0 z) = 1885 \cos(2\pi \times 10^8 t - \beta_0 z)$

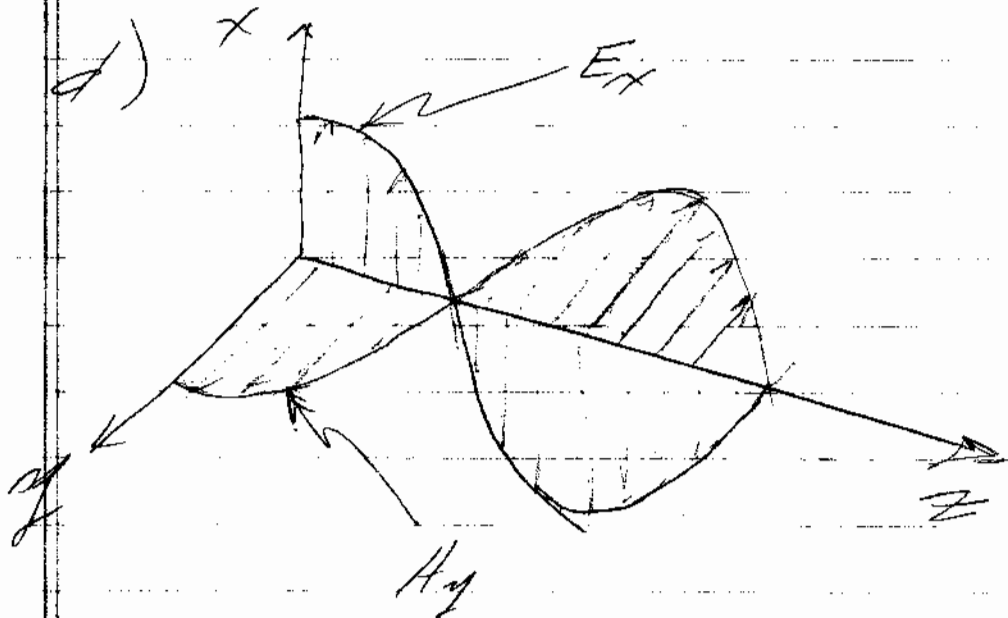
where $\beta_0 = \frac{\omega}{c} = \frac{2\pi \times 10^8}{3 \times 10^8} = 2.094$

$\lambda = \frac{c}{f} = \frac{3 \times 10^8}{1 \times 10^8} = 3 \text{ m}$

c) $\vec{B}_y^+ = \frac{1885}{c} e^{-j\beta_0 z} = 2\pi \times 10^{-6} e^{-j\beta_0 z}$

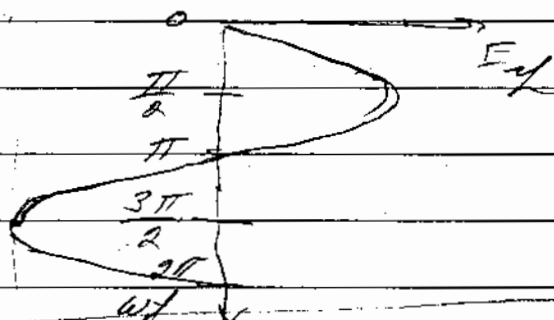
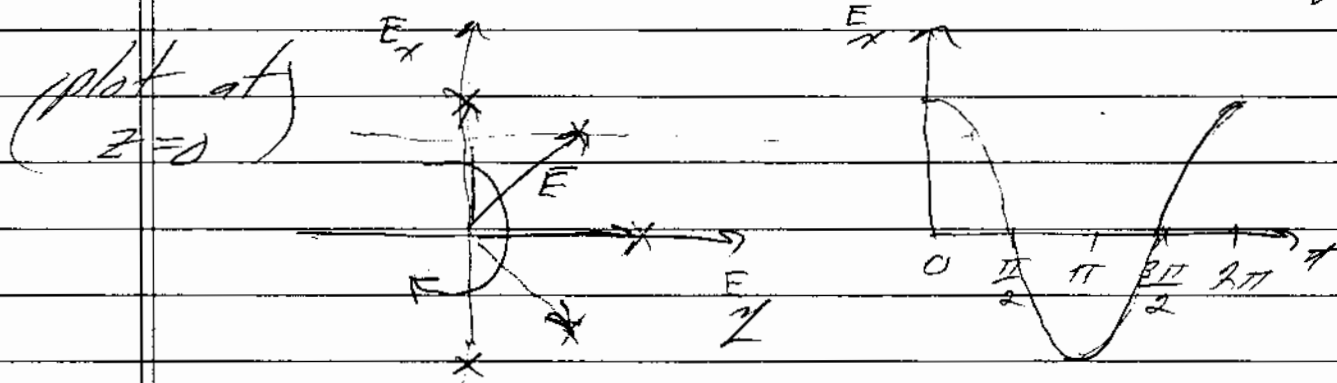
$\vec{H}_y^+ = \frac{1885}{377} e^{-j\beta_0 z} = 5 e^{-j\beta_0 z}$

so $\vec{H}_y^+ = 5 \cos(2\pi \times 10^8 t - \beta_0 z)$



$$2-46 \quad \vec{E}(z) = 500 e^{-j\beta_0 z} (\vec{a}_x - j\vec{a}_y)$$

$$\vec{E} = 500 \cos(\omega t - \beta_0 z) \vec{a}_x + 500 \sin(\omega t - \beta_0 z) \vec{a}_y$$



right hand or
clockwise circular
polarization

$$\vec{H}_z = \frac{500}{\eta_0} e^{-j\beta_0 z} \vec{a}_y + j \frac{500}{\eta_0} e^{-j\beta_0 z} \vec{a}_x$$

$$3.1 \quad n = 10^{29} ; \sigma = 5.8 \times 10^7 \text{ mho/m}$$

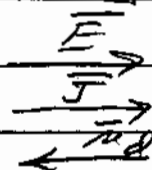
$$a) \mu_e = \frac{2\tau_c}{m} ; \sigma = \frac{n e^2}{m} \tau_c$$

$$\sigma / \mu_e = \sigma \left(\frac{1}{n e} \right) = \frac{5.8 \times 10^7}{10^{29} \times 1.6 \times 10^{-19}} = 3.625 \times 10^{-3}$$

$$b) \text{ charge density} = -10^{29} \frac{\text{elec}}{\text{m}^3} \times \frac{1.6 \times 10^{-19} \text{ C}}{\text{elec}} \times \frac{1 \text{ m}^3}{10^9 \text{ mm}^3} = -16 \frac{\text{C}}{\text{mm}^3}$$

$$c) \vec{E} = 2 \vec{a}_x ; \vec{v}_d = -\mu_e \vec{E} = -3.625 \times 10^{-3} \text{ m/sec}$$

$$\vec{J} = \sigma \vec{E} = 5.8 \times 10^7 \vec{a}_x \text{ A/m}^2$$



3.3 He $10^{25} \text{ atoms/m}^3$; $\chi_0 = 1.5 \times 10^{-4}$; $E = 10^3 \text{ V/m}$

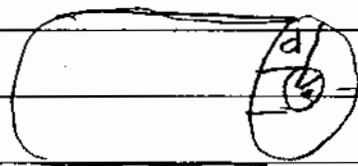
a) $\bar{P} = \epsilon_0 \chi_0 E = \frac{10^{-9}}{36\pi} \times 1.5 \times 10^{-4} \times 10^3 = \boxed{1.33 \times 10^{-12}} \leftarrow$

b) $\rho_v^+ = \overset{2 \text{ electrons/atom}}{2} \times 10^{25} \times 1.6 \times 10^{-19} = \boxed{3.2 \times 10^6 \text{ C/m}^3}$

$\bar{P} = \rho_v^+ \ell_{\text{ave}} \therefore \ell_{\text{ave}} = \frac{1.33 \times 10^{-12}}{3.2 \times 10^6} = \boxed{0.416 \times 10^{-18} \text{ m}}$

c) $\epsilon_r = 1 + \chi_0 = \boxed{1.00015} \leftarrow$

3-12



$\oint \vec{D} \cdot d\vec{s} = \rho_s L \quad \text{charge/m}$

$\int_{z=0}^L \int_{\phi=0}^{2\pi} D_{\phi} \rho \delta\phi dz = \rho_s L$

or $2\pi \rho \delta \phi = \rho_s \delta \phi \therefore D_{\phi} = \frac{\rho_s}{2\pi \rho} \Rightarrow \boxed{E_{\phi} = \frac{\rho_s}{2\pi \epsilon \rho}} \leftarrow$

a) E_r is constant if $\boxed{\epsilon = \frac{K}{\rho}} \leftarrow$

want $\epsilon = \epsilon_1$ @ $\rho = d \therefore \boxed{K = d\epsilon_1} \leftarrow$

and $\boxed{E_{\rho} = \frac{\rho_s}{2\pi \epsilon_1 d}} \leftarrow$

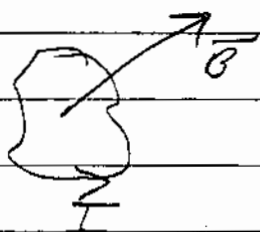
b) $\rho = \epsilon_0 E_{\rho} + \rho_s$ so $\rho = 0 - \epsilon_0 E_{\rho} = \frac{\rho_s}{2\pi \rho} - \frac{\epsilon_0 \rho_s}{2\pi \epsilon_1 d}$

$\boxed{\rho_{\rho} = \frac{\rho_s}{2\pi} \left(\frac{1}{\rho} - \frac{\epsilon_0}{\epsilon_1 d} \right)}$

$\rho_{\rho} = -\nabla \cdot \bar{P} = -\frac{1}{\rho} \frac{\partial}{\partial \rho} \left(\frac{\rho_s \epsilon_0 \rho}{2\pi \epsilon_1 d} \right) = \boxed{\frac{\rho_s \epsilon_0}{2\pi \epsilon_1 d \rho}} \leftarrow$

c) Use layers that approximate $\frac{\epsilon_0 d}{\rho}$ variation $\leftarrow$

3.16



$$\vec{F} = \oint \vec{I} d\vec{\ell} \times \vec{B}$$

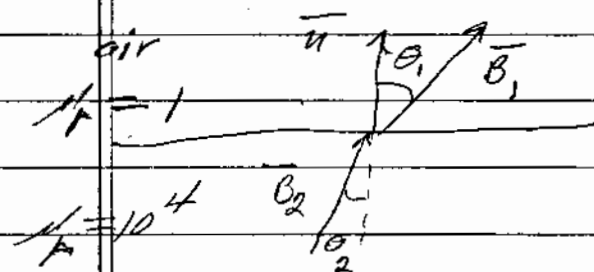
$$\vec{F} = \oint I d\vec{\ell} \times \vec{B} = -I \oint \vec{B} \times d\vec{\ell}$$

$$\vec{F} = -I \vec{B} \times \oint d\vec{\ell} \equiv 0 \quad \leftarrow$$

3.25

$$H_{t1} = H_{t2}$$

$$B_{n1} = B_{n2}$$

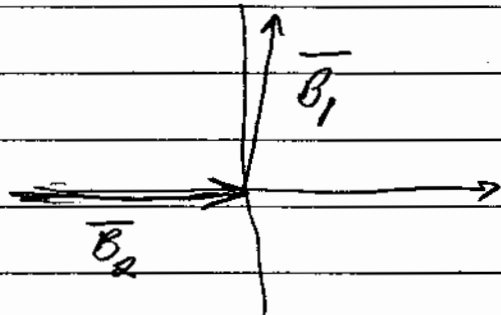


$$\tan \theta_2 = \frac{\mu_2}{\mu_1} \tan \theta_1 \quad (3.76)$$

$$\text{or } \theta_1 = \tan^{-1} [10^{-4} \tan \theta_2]$$

θ_2	θ_1
0°	0°
45°	$5.7 \times 10^{-3}^\circ$
89°	0.328°
89.9°	3.27°
89.9675°	10° ✓

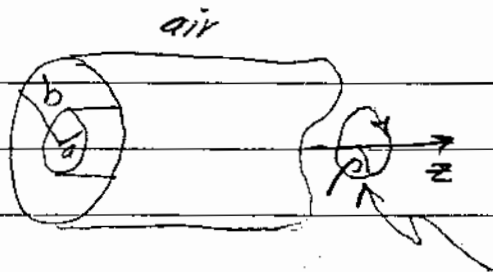
①



②

29, 33

3-28



I carried in conductors
 of radius " a " ($\mu = \mu_0$)
 for $a < p < b$ $\mu = \mu$

$\oint \vec{H} \cdot d\vec{l} = \int \vec{J} \cdot d\vec{A}$ Integrate around circular contour

a) for $p < a$ $H \oint 2\pi p = \frac{I}{\pi a^2} \pi p^2$ or $H \oint = \frac{I p}{2\pi a^2}$

$$B_{\phi} = \frac{\mu_0 I p}{2\pi a^2}$$

for $a < p < b$

$$H_{\phi} = \frac{I}{2\pi p}$$

$$B_{\phi} = \frac{\mu I}{2\pi p}$$

for $p > b$

$$H_{\phi} = \frac{I}{2\pi p}$$

$$B_{\phi} = \frac{\mu_0 I}{2\pi p}$$

b) $M = \frac{B}{\mu_0} - H = \frac{1}{\mu_0} \left[\frac{\mu I}{2\pi p} - \frac{I}{2\pi p} \right] = \frac{I}{2\pi p} [\mu - 1] \hat{\phi}$

H_{ϕ} is continuous across all boundaries ($H_{\text{tangential}}$)

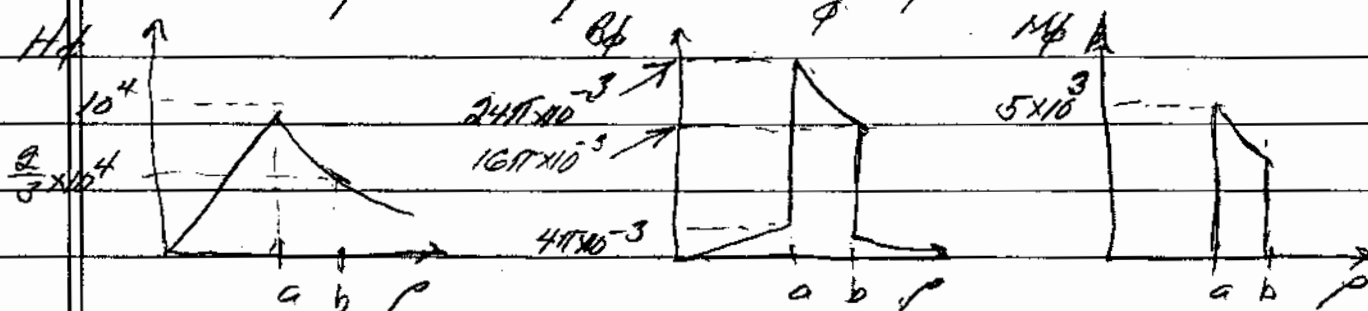
B_{ϕ} is discontinuous

@ $p = a$ $H_{\phi} = \frac{628}{2\pi \times 10^{-2}} = 10^4$; $B_{\phi} = 84\pi \times 10^{-3}$ ($p = a^+$)
 $B_{\phi} = 4\pi \times 10^{-3}$ ($p = a^-$)

$p = b$ $H_{\phi} = \frac{628}{2\pi \times 15 \times 10^{-2}} = \frac{2}{3} \times 10^4$; $B_{\phi} = 4\pi \times 10^{-7} \times 16 \times \frac{2}{3} \times 10^4 = 16\pi \times 10^{-3}$ ($p = b^-$)
 $B_{\phi} = \frac{2}{3} \pi \times 10^{-3}$ ($p = b^+$)

$M = 0$ for $p < a$ and $p > b$

$M = \frac{50}{p}$ $0 < p < b$

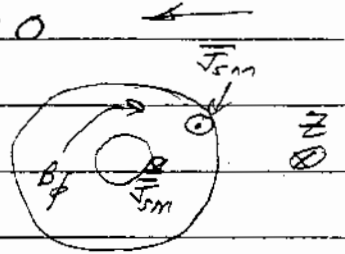


3.28 continued: $\vec{J}_m = \nabla \times \vec{M}$

$$\therefore \vec{J}_m = \vec{a}_\rho \left(-\frac{\partial M_z}{\partial z} \right) + \vec{a}_z \left(\frac{1}{\rho} \frac{\partial}{\partial \rho} (\rho M_\phi) \right) = 0$$

$$\vec{J}_{sm}(\rho=0) = \vec{a}_\rho \times \vec{M} = 5 \times 10^3 \vec{a}_z$$

$$\vec{J}_{sm}(\rho=b) = -\vec{a}_\rho \times \vec{M} = -\frac{10}{3} \times 10^3 \vec{a}_z$$



3.29

Region 1

$\epsilon = \epsilon_0$

$$\vec{n} = \vec{a}_z$$

$$\vec{E}_1 = -15\vec{a}_x + 20\vec{a}_y + 30\vec{a}_z$$

$$\begin{cases} E_{tang,1} = E_{tang,2} \\ D_{norm,1} = D_{norm,2} \end{cases}$$

Region 2 $\epsilon = 4\epsilon_0$

$$a) \boxed{\vec{E}_2 = -15\vec{a}_x + 20\vec{a}_y + \frac{15}{2}\vec{a}_z} \leftrightarrow \begin{cases} D_{z,1} = 30\epsilon_0 = D_{z,2} \\ E_{z,2} = \frac{D_{z,2}}{4\epsilon_0} = \frac{30}{4} \end{cases}$$

$$\vec{D}_1 = \epsilon_0 \vec{E}_1$$

$$\vec{D}_2 = 4\epsilon_0 \vec{E}_2$$

$$b) \vec{n} \cdot \vec{E}_1 = |\vec{E}_1| \cos \theta_1 = 30 \quad \therefore \theta_1 = \cos^{-1} \left\{ \frac{30}{\sqrt{15^2 + 20^2 + 30^2}} \right\} = 39.8^\circ$$

$$\theta_2 = \cos^{-1} \left\{ \frac{\frac{15}{2}}{\sqrt{15^2 + 20^2 + 7.5^2}} \right\} = 73.3^\circ$$

$$c: \tan \alpha = \frac{\epsilon_2}{\epsilon_1} \tan \theta_1$$

$$3.333 = 4 \times 0.833$$

$$3.333 = 3.333 \quad !$$

$$3-33 \quad \alpha = \frac{\omega \sqrt{\mu \epsilon}}{\sqrt{2}} \left[\sqrt{1 + \left(\frac{\sigma}{\omega \epsilon} \right)^2} - 1 \right]^{\frac{1}{2}}$$

$$\beta = \frac{\omega \sqrt{\mu \epsilon}}{\sqrt{2}} \left[\sqrt{1 + \left(\frac{\sigma}{\omega \epsilon} \right)^2} + 1 \right]^{\frac{1}{2}}$$

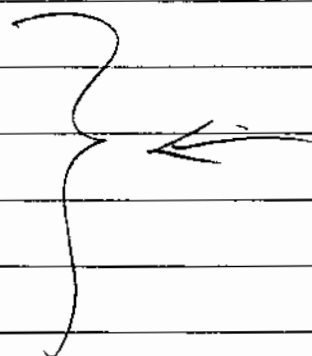
$$\eta = \sqrt{\frac{\mu}{\epsilon - j \frac{\sigma}{\omega}}}$$

For $\sigma = 0$, $\mu = \mu_0$, $\epsilon = \epsilon_0$ these give?

$$\alpha = 0$$

$$\beta = \omega \sqrt{\mu_0 \epsilon_0}$$

$$\eta = \sqrt{\frac{\mu_0}{\epsilon_0}}$$



3.38 $E_m^+ = 1$ @ $z=0$; $\epsilon_r = 81$ for sea water $\sigma = 4$
 $f = 10^4$
 $\frac{\sigma}{\omega\epsilon} = \frac{4 \times 36\pi}{10^{-9} \times 2\pi \times 10^4} = 7.2 \times 10^6 \gg 1$ $\therefore$ good conductor

so $\alpha = \beta = \sqrt{\frac{\omega\mu}{2}} = \sqrt{\frac{2\pi \times 10^4 \times 4 \times 4\pi \times 10^{-7}}{2}} = 0.397$

for $e^{-\alpha z} = 0.05$; $z_{5\%} = -\frac{\ln 0.05}{\alpha} = 7.5 \text{ m}$

for $f = 10^3$ $\frac{\sigma}{\omega\epsilon} = 7.2 \times 10^7$ (good conductor)

$\alpha = \beta = 4\pi \times 10^{-2} = 0.1257$

$z_{5\%} = -\frac{\ln 0.05}{0.1257} = 23.8 \text{ m}$

RF communication in sea water is only possible at very low frequencies.

6 3.37 $E_m^+ = 200 \text{ V/m}$; $f = 10^8 \text{ Hz}$, $\mu = \mu_0$, $\epsilon = 6\epsilon_0$, $\sigma = 10^{-2}$
 $\gamma = 0.761 + j5.187 = \alpha + j\beta$

a) $\lambda = \frac{2\pi}{\beta} = 1.21 \text{ m}$

$\delta = \frac{1}{\alpha} = 1.31 \text{ m}$

$v_{ph} = \frac{\omega}{\beta} = \frac{2\pi \times 10^8}{5.187}$

$= 1.21 \times 10^8 \text{ m/sec}$

b) $\hat{H}_y^+ = \sqrt{\frac{\mu}{\epsilon - j\frac{\sigma}{\omega}}} = \sqrt{\frac{4\pi \times 10^{-7}}{6 \times 10^{-9} - j\frac{10^{-2}}{2\pi \times 10^8}}}$

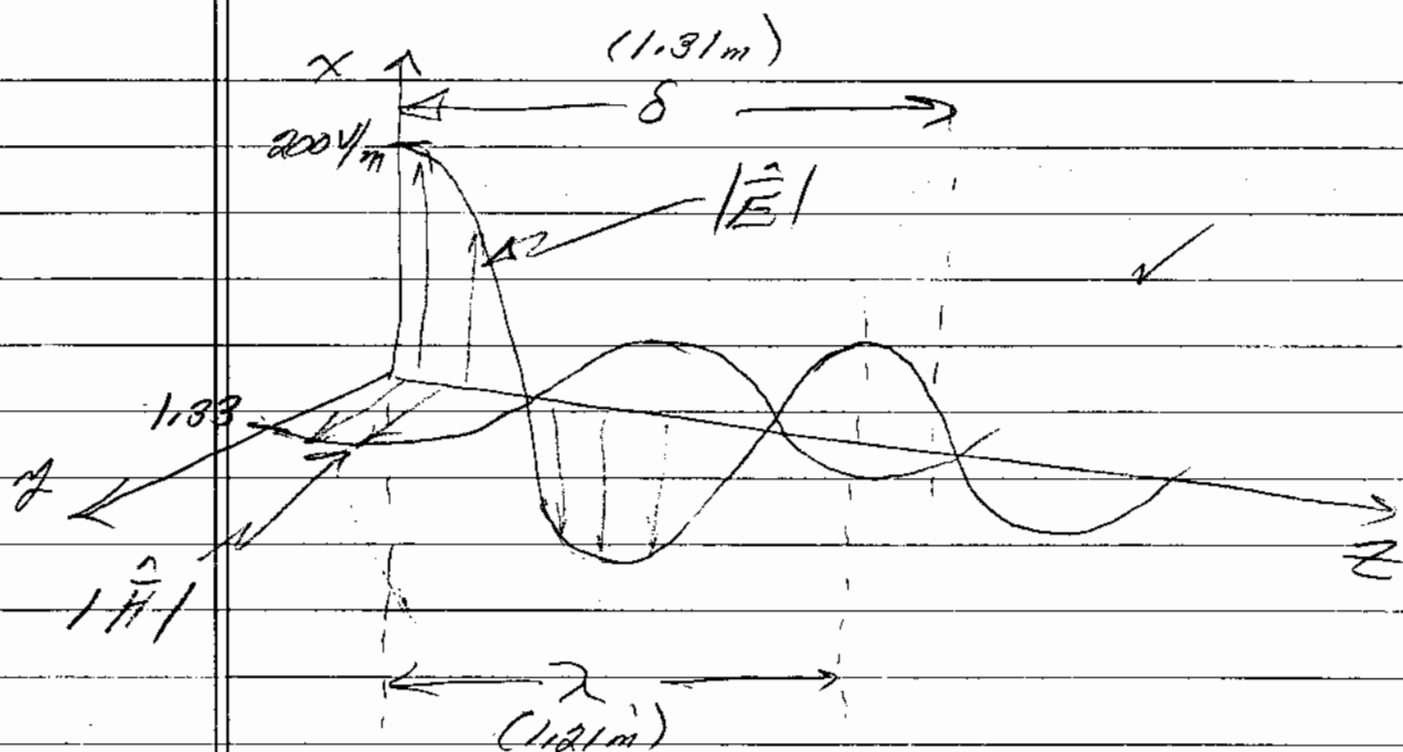
$= 1.506 \times 10^0 \angle 8.34^\circ$

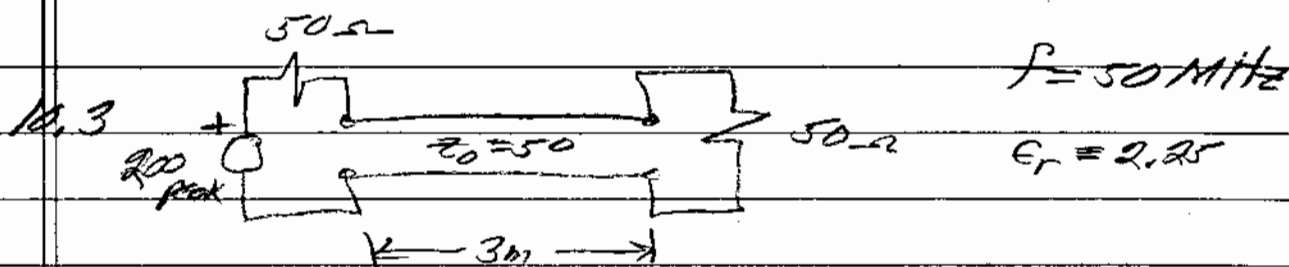
$\rightarrow$ so $H_y^+ = \frac{200}{\hat{H}_y^+} = 1.33 \angle -8.34^\circ \text{ A/m}$

EE 333

Homework 9

(page 2)





$$v_{ph} = \frac{3 \times 10^8}{\sqrt{2.25}} = 2 \times 10^8 \text{ m/sec} ; \lambda = \frac{2 \times 10^8}{5 \times 10^7} = 4 \text{ m}$$

$$\text{so line length} = \frac{3}{4} \lambda$$

$$a) \Gamma(z) = \frac{Z_L - Z_0}{Z_L + Z_0} = 0 \quad \therefore \Gamma(z) \text{ is zero at all points on the line}$$

$$Z(z) = Z_0 \frac{1 + \Gamma(z)}{1 - \Gamma(z)} = Z_0 \text{ everywhere}$$

$$b) \hat{V}(z) = \hat{V}_m^+ e^{-j\beta z} ; \hat{I}(z) = \frac{\hat{V}_m^+}{Z_0} e^{-j\beta z}$$

these become $\hat{V}_m^+$ and $\hat{V}_m^+/Z_0$ at $z=0$

$$c) \hat{I}_m = \hat{I}_m^+ = \frac{\hat{V}_m^+}{Z_0} = \frac{200}{100} = 2 \text{ A} ; \hat{V}_m = \hat{V}_m^+ = 100$$

$$\therefore \left. \begin{aligned} \hat{V}(z) &= 100 e^{-j\beta z} = 100 e^{-j \frac{2\pi}{\lambda} z} \\ \hat{I}(z) &= 2 e^{-j\beta z} = 2 e^{-j \frac{2\pi}{\lambda} z} \end{aligned} \right\}$$

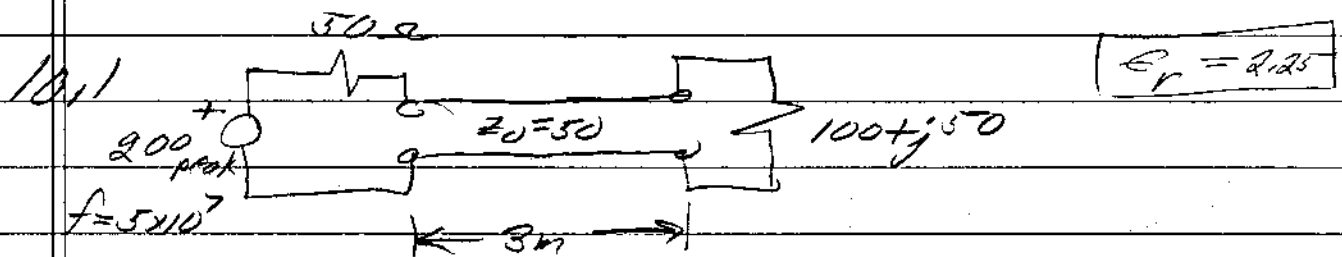
$$P_{in} = \frac{1}{2} 100 \times 2 = 100 \text{ Watts}$$

$$\hat{V}_{load} = 100 e^{-j \frac{2\pi}{\lambda} (\frac{3\lambda}{4})} = 100 e^{-j \frac{3\pi}{2}} = j100$$

so $\hat{I}_{load} = j2$

$$\text{and } P_{load} = \frac{1}{2} \text{Re}\{j100 (-j2)\} = 100 \text{ Watts}$$

$$\text{or } P_{load} = \frac{1}{2} |\hat{I}|^2 50 = \frac{1}{2} \frac{100^2}{50} = 100 \text{ W}$$



$$\beta = j\omega \sqrt{\mu\epsilon} = j\omega \frac{\sqrt{2.25}}{3 \times 10^8} = j2\pi \times 5 \times 10^7 \frac{1.5}{3 \times 10^8} = j\frac{1}{2}\pi$$

$$v_p = \frac{3 \times 10^8}{\sqrt{\epsilon_r}} = 2 \times 10^8 \text{ m/sec} ; \lambda = \frac{2\pi}{\beta} = 4 \text{ m} \quad \text{line length} = \frac{3}{4}\lambda$$

$$\Gamma_{\text{load}} = \frac{Z_L - Z_0}{Z_L + Z_0} = \frac{50 + j50}{150 + j50} = 0.4 + j0.2 = 0.4472 \angle 26.565^\circ$$

$$\Gamma_{\text{in}} = \Gamma_{\text{load}} e^{-j2\beta \frac{3\lambda}{4}} = (0.4 + j0.2) e^{-j3\pi} = -(0.4 + j0.2) = -0.4472 \angle 26.56^\circ$$

$\therefore$ approximately 45% voltage reflection

$$Z_{\text{in}} = 50 \frac{1 + \Gamma_{\text{in}}}{1 - \Gamma_{\text{in}}} = 50 \frac{0.6 - j0.2}{1.4 + 0.2} = 20 - j10$$

$$I_{\text{in}} = \frac{200}{50 + Z_{\text{in}}} = \frac{200}{70 - j10} = 2.828 \angle 8.113^\circ$$

$$P_{\text{in}} = \frac{1}{2} |I_{\text{in}}|^2 R_{\text{in}} = \frac{1}{2} (2.828)^2 (20) = 79.98 \text{ Watts}$$

$$\hat{I} = \hat{I}_{\text{in}} e^{-j\beta z} [1 - \Gamma(z)] \quad \therefore \hat{I}_{\text{in}}^+ = \frac{\hat{I}_{\text{in}}}{1 - \Gamma(0)}$$

$$\text{so } \hat{I}_{\text{load}} = \hat{I}_{\text{in}} e^{-j\frac{3\pi}{4}} [1 - \Gamma_{\text{load}}] = \hat{I}_{\text{in}} e^{-j\frac{3\pi}{4}} \frac{1 - \Gamma_{\text{load}}}{1 - \Gamma_{\text{in}}}$$

$$\text{or } \hat{I}_{\text{load}} = 2.828 \angle 8.113^\circ \frac{0.6 - j0.2}{1.4 + j0.2} = 1.2647 \angle 71.56^\circ$$

$$\therefore P_{\text{load}} = \frac{1}{2} (1.2647)^2 \times 100 = 79.97 \text{ Watts}$$

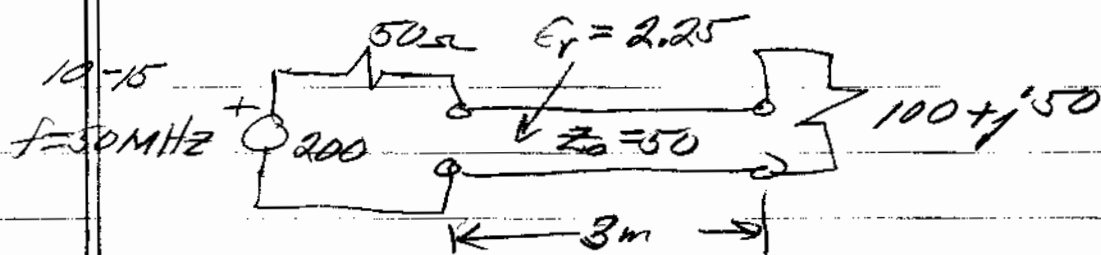
$$10.2 \quad P_{ave} = \frac{1}{2} \operatorname{Re} \left\{ \hat{V}_m^+ e^{-j\beta z} [1 + \Gamma] \frac{\hat{V}_m^+}{Z_0} e^{+j\beta z} [1 - \Gamma^*] \right\}$$

$$P_{ave} = \frac{1}{2} \operatorname{Re} \left\{ \frac{|\hat{V}_m^+|^2}{Z_0} [1 - \Gamma^* + \Gamma - |\Gamma|^2] \right\}$$

$$\text{so } P_{ave} = \frac{|\hat{V}_m^+|^2}{2Z_0} [1 - |\Gamma|^2]$$

$$\Gamma = \frac{\hat{V}_m^-}{\hat{V}_m^+} e^{-j2\beta z} \quad \text{so } |\Gamma| = \frac{|\hat{V}_m^-|}{|\hat{V}_m^+|}$$

$$\text{so } P_{ave} = \frac{|\hat{V}_m^+|^2}{2Z_0} - \frac{|\hat{V}_m^-|^2}{2Z_0} = P_{ave}^+ - P_{ave}^-$$

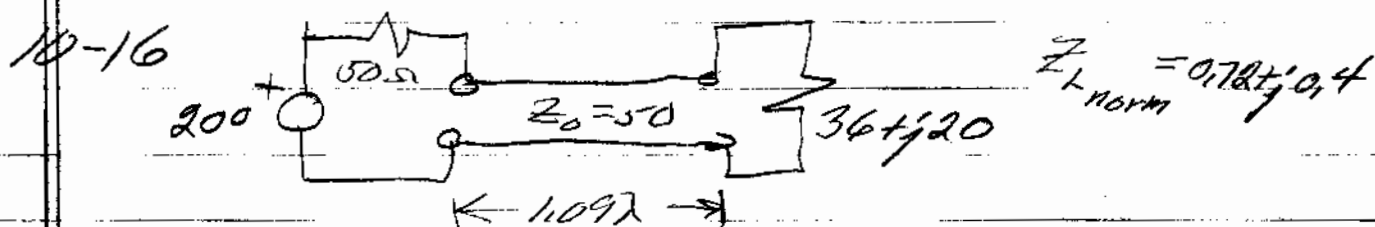


$$\lambda = \frac{3 \times 10^8}{5 \times 10^7 \times \sqrt{2.25}} = 4m \quad \therefore \text{line length} = \frac{3}{4} \lambda$$

$$Z_{L, \text{norm}} = 2 + j1 \quad ; \text{ from chart: } \Gamma_L = 0.46 \angle 26^\circ \leftarrow$$

$$[\text{chart scales } 0.214 + 0.25 = 0.464\lambda]$$

$$\text{from chart: } \left\{ \begin{array}{l} \Gamma_{in} = 0.46 \angle 15^\circ \\ Z_{in, \text{norm}} = 0.4 - j0.195 \text{ or } Z_{in} = 20 - j9.75 \end{array} \right\} \leftarrow$$



$$\text{from chart: } \Gamma_L = 0.89 \angle 112^\circ$$

$$\text{chart rotation} = 0.094 + 0.09 = 0.184\lambda$$

$$\text{from chart: } \Gamma_{in} = 0.89 \angle 48^\circ \text{ and } Z_{in, \text{norm}} = 1.32 + j0.58$$

$$\text{or } \boxed{Z_{in} = 66 + j29} \leftarrow$$

$$10-21 \quad Z_L = 36 + j20 \quad ; \quad Z_0 = 50 \quad \therefore \quad Z_{L, \text{norm}} = 0.72 + j0.4$$

$$\text{from chart } Y_{L, \text{norm}} = 1.07 - j0.59 \leftarrow$$

$$\frac{1}{Z_{L, \text{norm}}} = \frac{1}{0.72 + j0.4} = \frac{1}{0.8237 \angle 29.05^\circ} = 1.214 \angle -29.05^\circ = 1.06 - j0.59 \leftarrow$$

Problem
10-15

IMPEDANCE OR ADMITTANCE COORDINATES

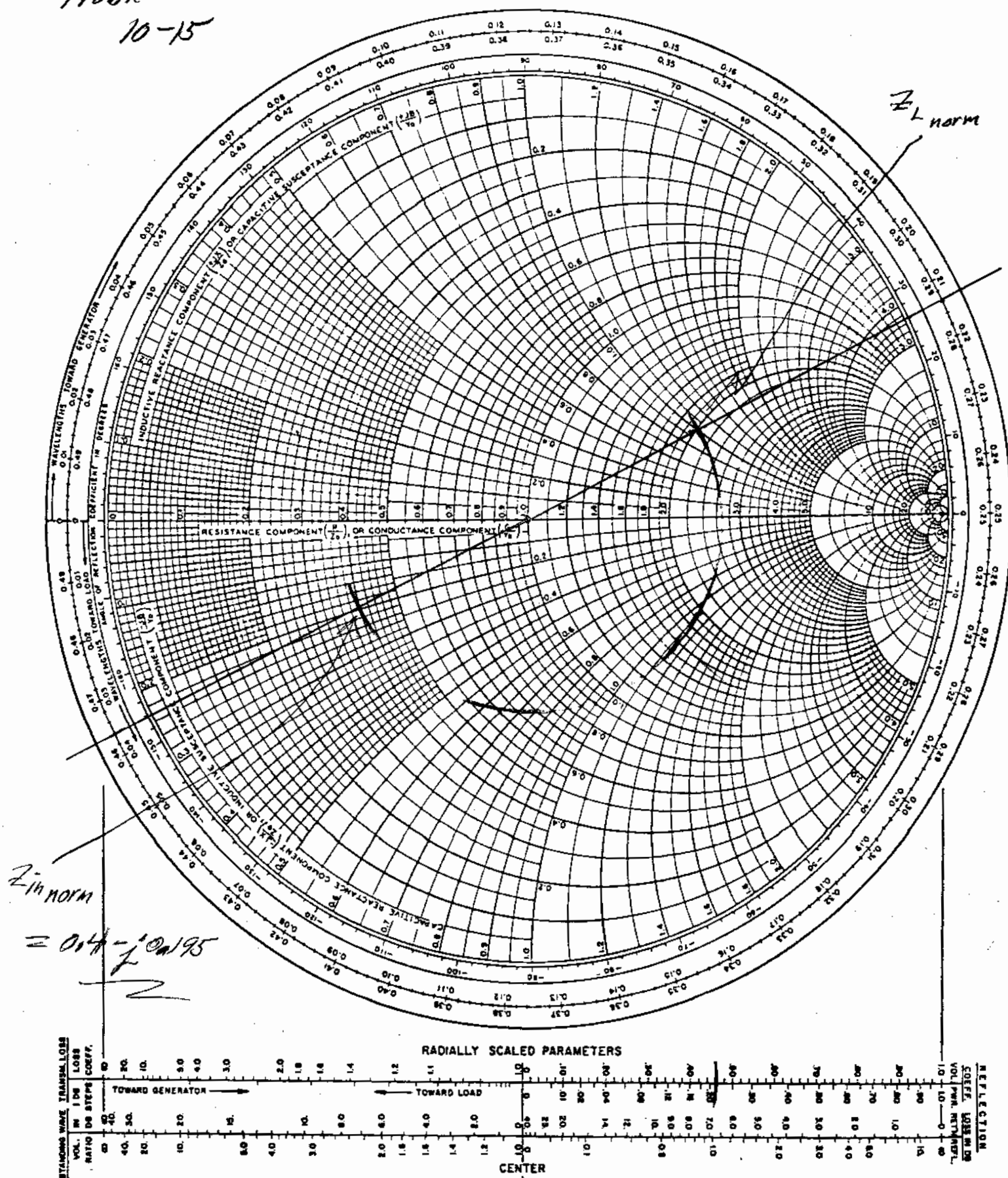


Fig. 9-3. A standard commercially available form of Smith chart graph paper. Copyrighted 1949 by Kay Electric Company, Pine Brook, N. J., and reprinted with their permission.

10-16

IMPEDANCE OR ADMITTANCE COORDINATES

$$Z_{in\text{ norm}} = 1.32 + j'0.58$$

$$Z_{in} = 66 + j'29$$

$$\Gamma_m = 0.29 \angle 49^\circ$$

$$Z_{L\text{ norm}} = 0.72 + j'0.4$$

$$\Gamma_L = 0.29 \angle 19^\circ$$

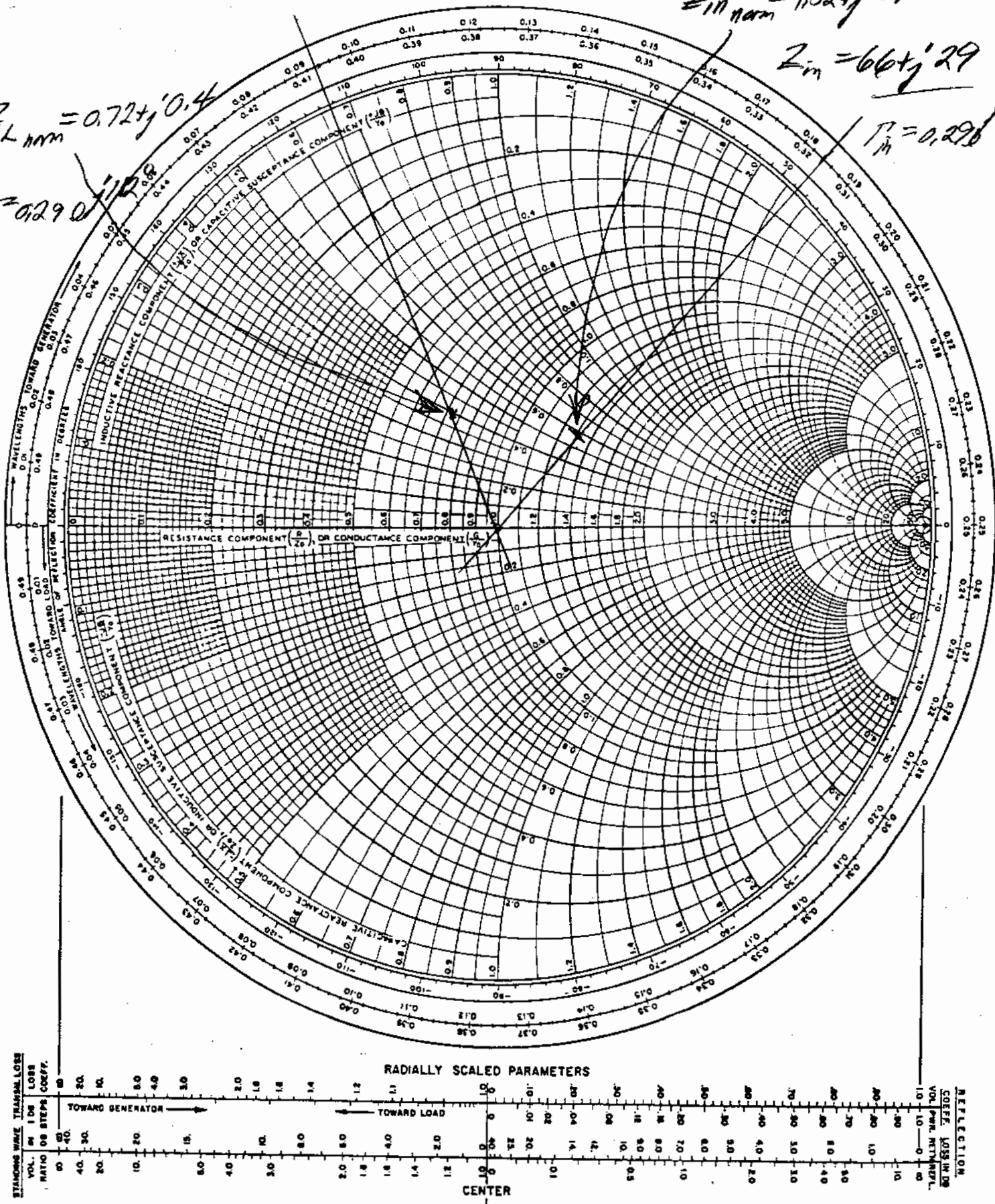


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Problem
10-21

IMPEDANCE OR ADMITTANCE COORDINATES

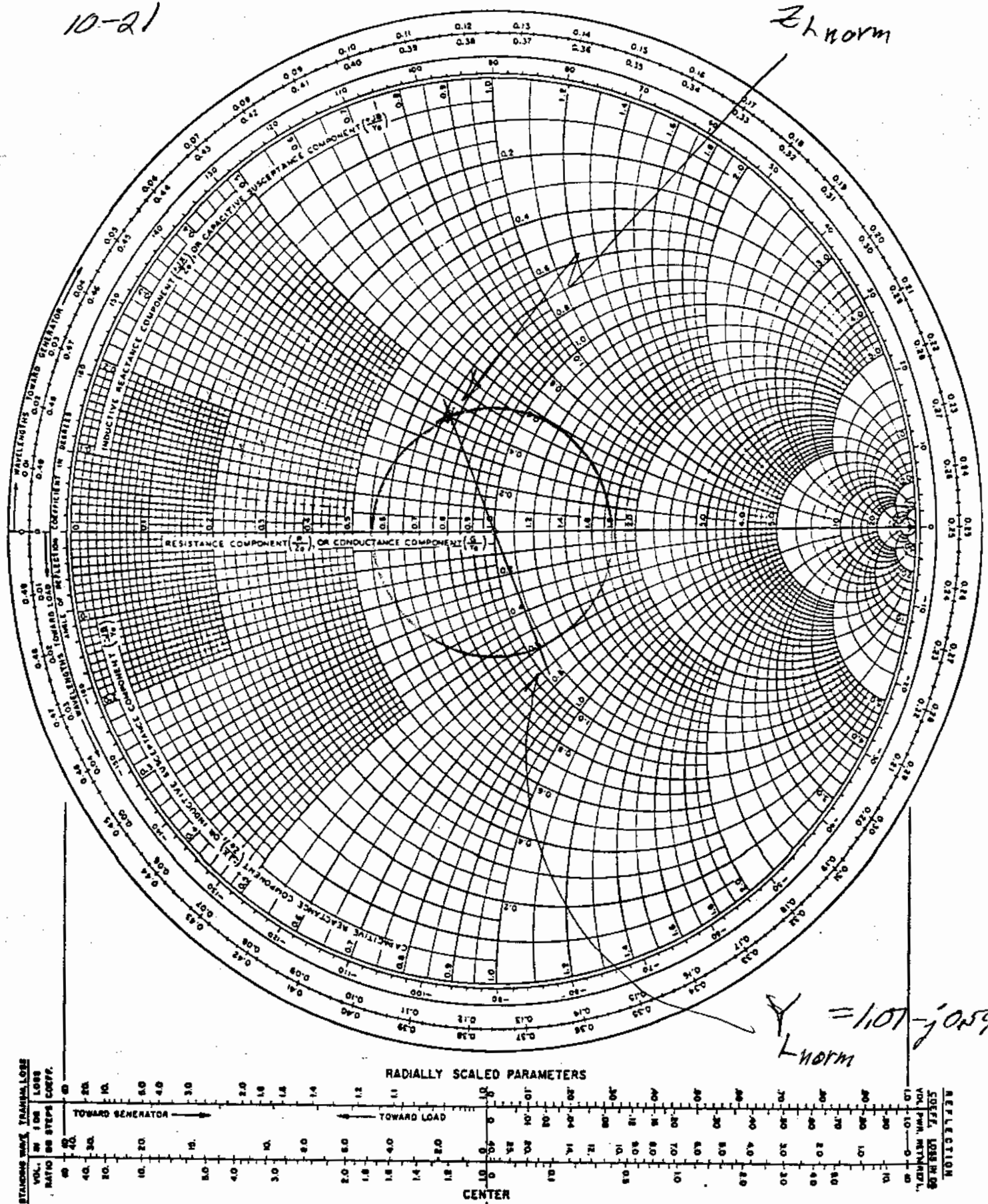
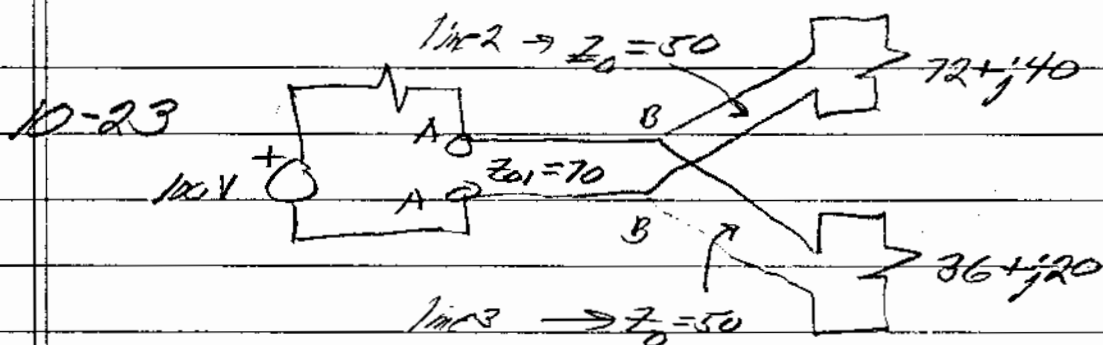


Fig. 9-3. A standard commercially available form of Smith chart graph paper. Copyrighted 1949 by Kay Electric Company, Pine Brook, N. J., and reprinted with their permission.



from example 10-6 $P_{ave} = 8.5 \text{ Watts}$
into A-A

$$Y_{in @ BB} = G_2 + jB_2 \quad ; \quad Y_{in @ BB} = G_3 + jB_3$$

$$P_{ave} = \frac{1}{2} \Re \{ \tilde{V} \tilde{I}^* \} = \frac{1}{2} \Re \{ \tilde{V} \tilde{V}^* Y^* \} = \frac{1}{2} |\tilde{V}|^2 G$$

$$\frac{P_{ave2}}{P_{ave1}} = \frac{G_2}{G_3} \quad \leftarrow$$

$$\frac{1}{2} |\tilde{V}_{BB}|^2 (G_2 + G_3) = 8.5 = \frac{1}{2} |\tilde{V}|^2 G_2 \left(1 + \frac{G_3}{G_2} \right)$$

$$= P_{ave2} \left(1 + \frac{G_3}{G_2} \right)$$

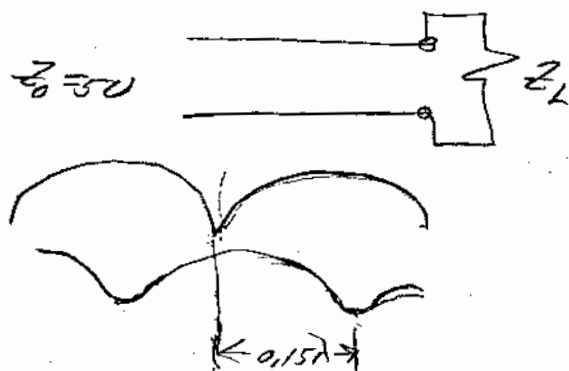
but from example: $G_2 = 0.0366$ + $G_3 = 0.012$

$$\text{so } P_{ave2} = \frac{8.5}{1 + \frac{0.012}{0.0366}} = \boxed{6.4 \text{ Watts}} \quad \leftarrow$$

$$P_{ave3} = 8.5 - 6.4 = \boxed{2.1 \text{ Watts}} \quad \leftarrow$$

↑
lossless lines

10-27

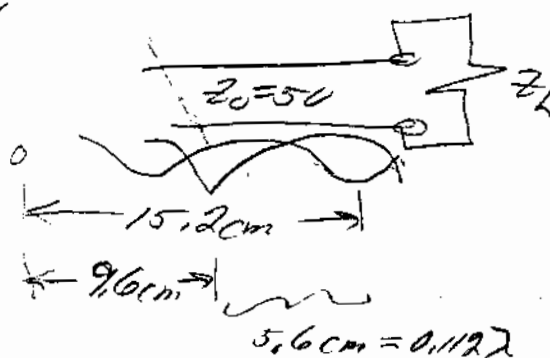


$$SWR = 4.0$$

$$\text{from chart } Z_{L_{\text{norm}}} = 0.67 + j1.14$$

$$\therefore \boxed{Z_L = 33.5 + j57}$$

10.28



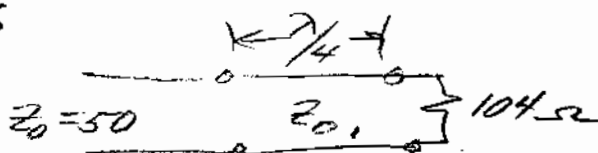
$$f = 600 \text{ MHz} ; SWR = 3.5$$

$$\lambda = \frac{3 \times 10^8}{6 \times 10^8} = 0.5 \text{ m}$$

$$\text{from chart } Z_{L_{\text{norm}}} = 0.475 + j0.73$$

$$\text{or } \boxed{Z_L = 23.75 + j36.5}$$

10.36

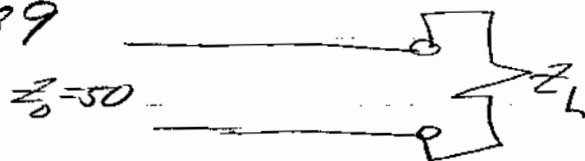


$$f = 500 \text{ MHz} , \epsilon_r = 2.26$$

$$\boxed{Z_{01} = \sqrt{50 \times 104} = 72.1 \Omega}$$

$$\lambda = \frac{3 \times 10^8}{\sqrt{2.26} \cdot 5 \times 10^8} = \frac{0.6}{1.5} = 0.4 \text{ m} \quad \therefore \boxed{\lambda/4 = 0.1 \text{ m}}$$

10.39



$$f = 500 \text{ MHz} ; \lambda = 60 \text{ cm}$$

$$SWR = 3.5$$

(see chart)

place stub $(0.25 - 0.171)\lambda = 0.08\lambda = 4.8 \text{ cm}$ either direction from V_{min}

a) For stub toward the load $Y_{\text{norm stub}} = -j1.3$; stub length = $0.335 - 0.25 = 0.105$
or stub $\boxed{\text{length} = 6.3 \text{ cm}}$

SWR from generator to stub = 1

b) SWR from stub to load = 3.5

c) For stub toward the generator $Y_{\text{norm stub}} = +j1.3$; stub length = $(0.145 + 0.25)\lambda = 23.7 \text{ cm}$

IMPEDANCE OR ADMITTANCE COORDINATES

$$Z_{\text{load}} = 0.25$$

$$Z_{\text{in}} = 0.67 + j1.14$$

Problem 10.27

0.152

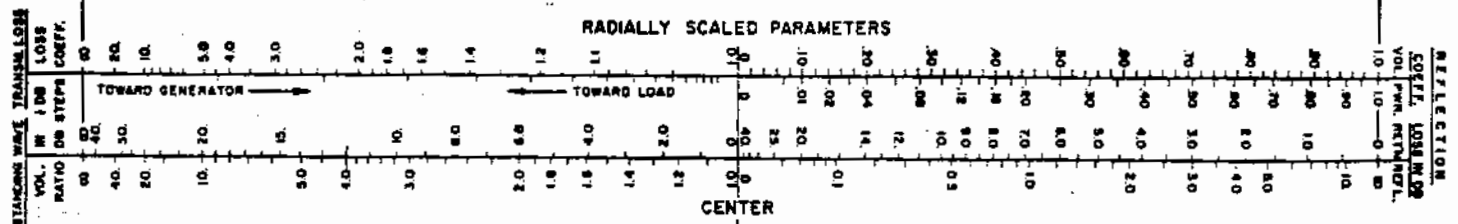


Fig. 9-3. A standard commercially available form of Smith chart graph paper. Copyrighted 1949 by Kay Electric Company, Pine Brook, N. J., and reprinted with their permission.

IMPEDANCE OR ADMITTANCE COORDINATES

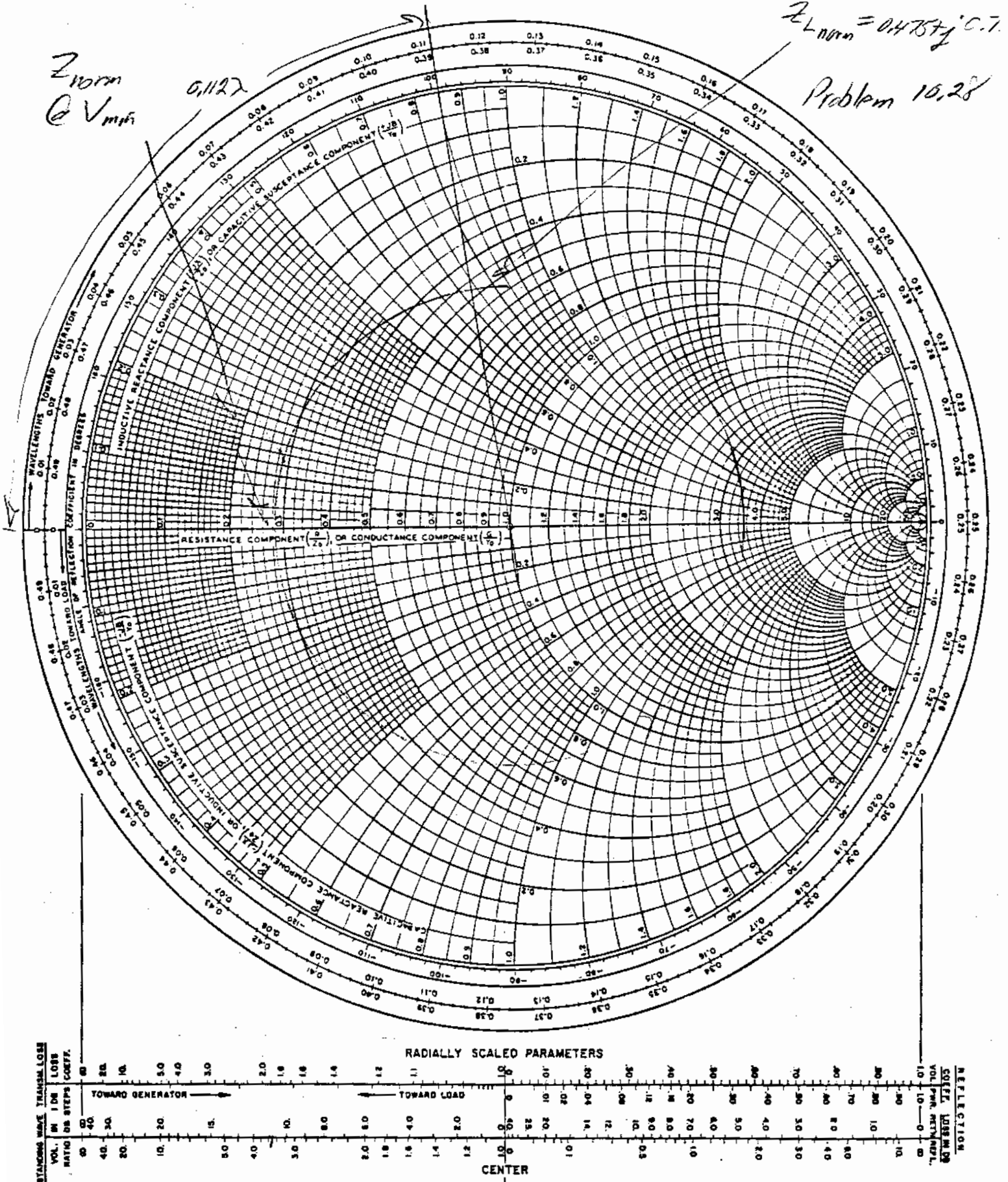


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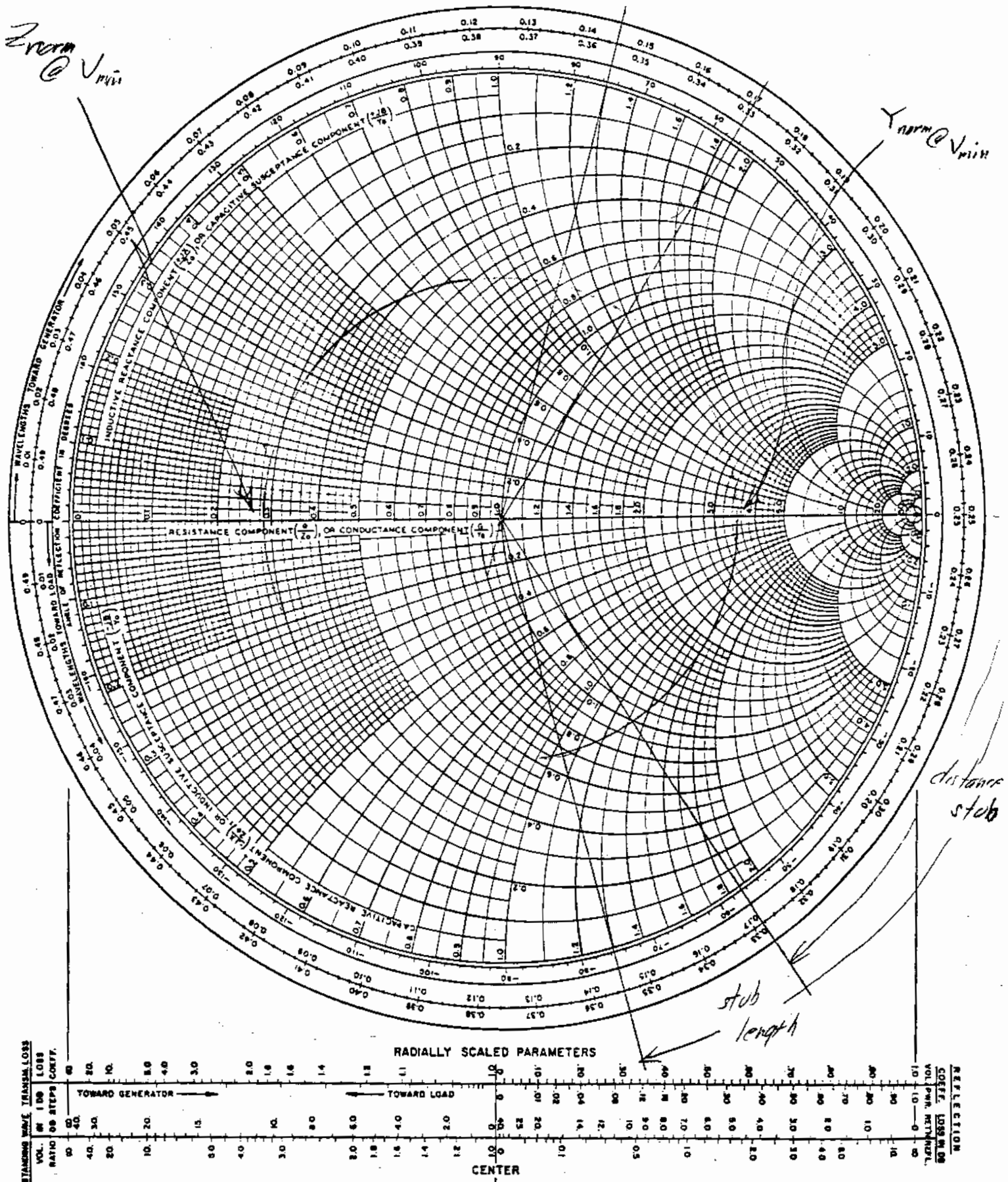
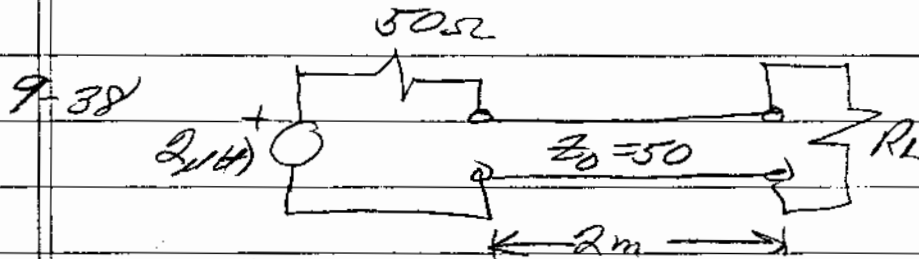
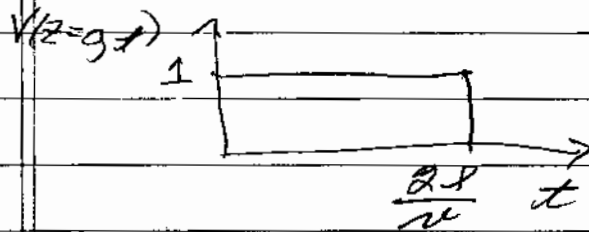


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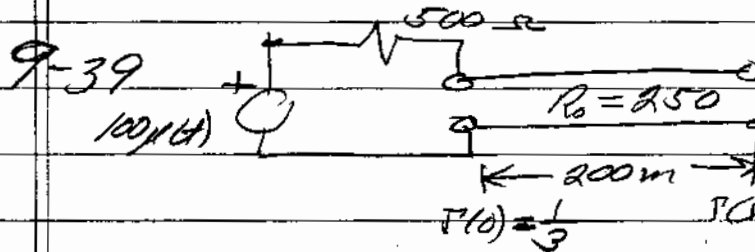
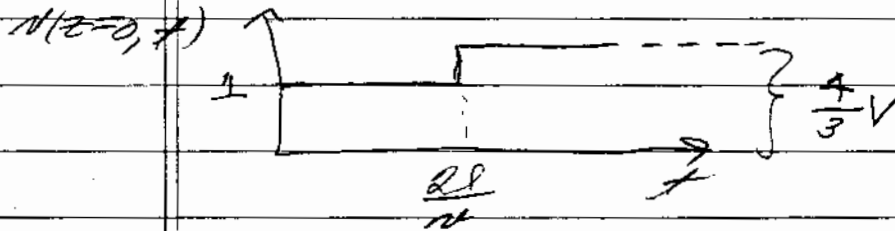


a) $R_L = 0$, $\Gamma_L = -1$

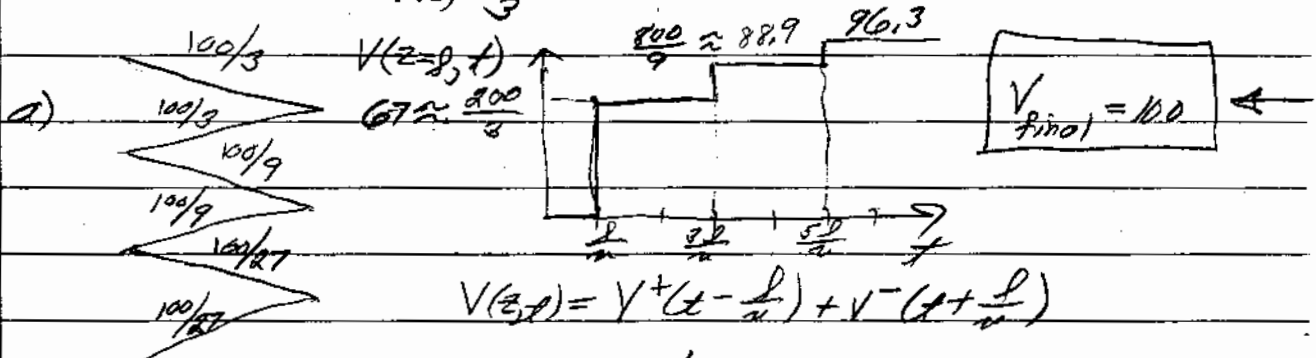


where $\frac{l}{v} = \frac{2}{3 \times 10^8} = \frac{2}{3} \times 10^{-8}$

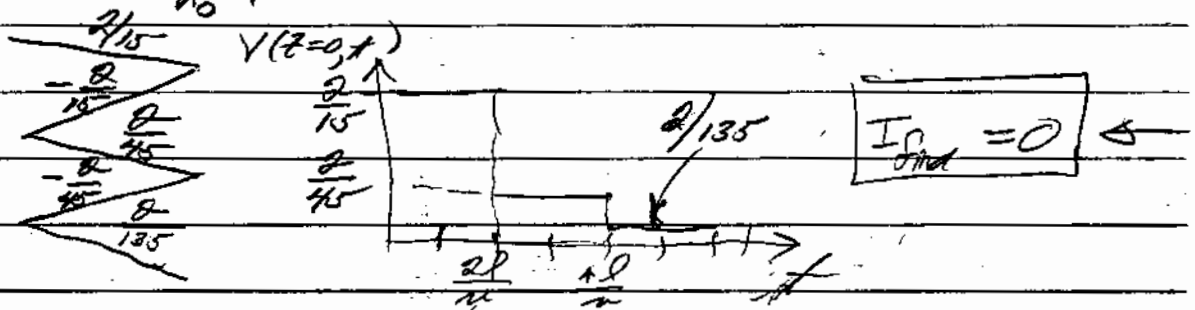
b) $R_L = 100$, $\Gamma_L = \frac{100-50}{100+50} = \frac{1}{3}$



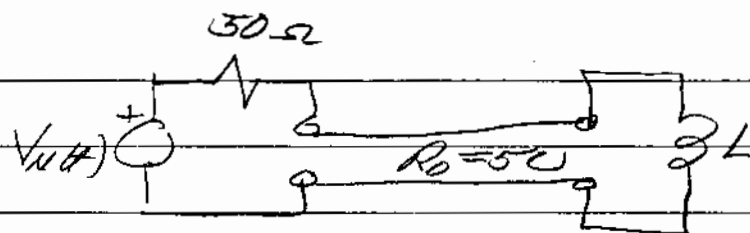
$V^+(z=0, t) = 100(\frac{1}{3})V$
 $I^+(z=0, t) = \frac{V^+}{Z_0} = \frac{2}{15}A$



b) $I(z, t) = \frac{1}{Z_0} \{ V^+ - V^- \} = \frac{V^+}{Z_0} \{ 1 - \Gamma \}$



9-40



@ load $V^+(t - \frac{l}{u}) = \frac{V}{2} u(t - \frac{l}{u}) = \frac{V}{2} u(t')$; $t' = t - \frac{l}{u}$

so at load we have:

$$V = iR_0 + L \frac{di'}{dt'}$$

$i_{\text{hom}} = A e^{st}$; $s = -\frac{R_0}{L}$ so $i_h = A e^{-\frac{R_0 t'}{L}}$

$i_{\text{particular}} = K = \frac{V}{R_0}$ so $i' = A e^{-\frac{R_0 t'}{L}} + \frac{V}{R_0}$

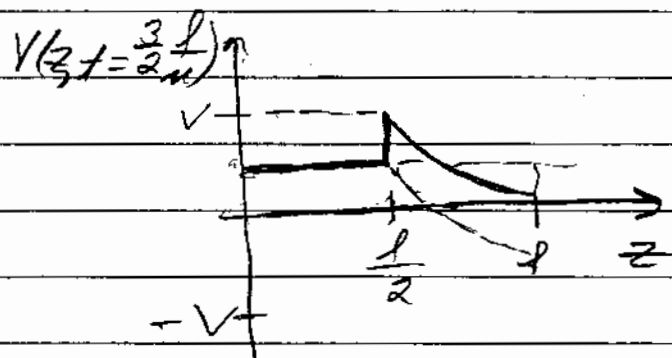
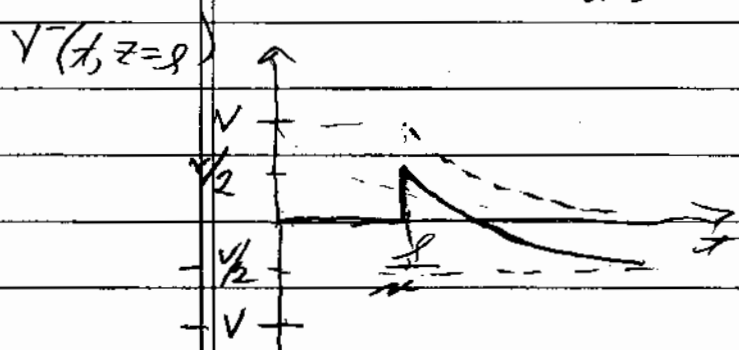
Assuming no initial energy storage [$i(0^-) = 0$]

$$i = \frac{V}{R_0} (1 - e^{-\frac{R_0 t'}{L}}) = \left[V^+(t - \frac{l}{u}) - V^-(t + \frac{l}{u}) \right] \frac{1}{R_0}$$

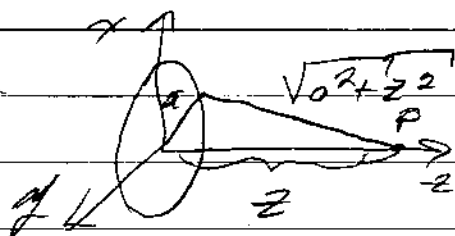
giving $V^-(t + \frac{l}{u}) = V^+(t - \frac{l}{u}) - V(1 - e^{-\frac{R_0 (t - \frac{l}{u})}{L}})$

or $V^-(t + \frac{l}{u}) = \frac{V}{2} u(t - \frac{l}{u}) - V(1 - e^{-\frac{R_0 (t - \frac{l}{u})}{L}}) u(t - \frac{l}{u})$

$$V^-(t + \frac{l}{u}) = \left[-\frac{V}{2} + V e^{-\frac{R_0 (t - \frac{l}{u})}{L}} \right] u(t - \frac{l}{u})$$



4-12



$$a) \Phi_P = \int_{\phi=0}^{2\pi} \frac{q \rho \rho d\phi}{4\pi\epsilon (a^2 + z^2)^{1/2}}$$

$$\Phi_P = \frac{q \rho \rho}{2\epsilon (a^2 + z^2)^{1/2}}$$

$$\vec{E} = -\nabla \Phi = -\frac{\partial \Phi}{\partial z} \vec{a}_z = \frac{q \rho \rho \cdot 2z}{4\epsilon (a^2 + z^2)^{3/2}} \vec{a}_z$$

on z axis

$$b) \Phi(z) = -\int_{\infty}^z \frac{q \rho \rho \cdot \vec{a}_z \cdot d\vec{z}}{2\epsilon (a^2 + z^2)^{3/2}} = -\int_{\infty}^z \frac{q \rho \rho \cdot du}{4\epsilon u^{3/2}}$$

let $u = a^2 + z^2$
 $du = 2z dz$

$$\Phi(z) = + \frac{q \rho \rho \cdot 2}{4\epsilon u^{1/2}} \Big|_{\infty}^{a^2 + z^2}$$

$$\text{so } \Phi(z) = \frac{q \rho \rho}{2\epsilon (a^2 + z^2)^{1/2}}$$

$$4-16 \text{ for coax } C/m = \frac{2\pi\epsilon}{\ln(b/a)} = 96.8 \times 10^{-12}$$

$$\boxed{C_1 = 8.26}$$

$$\text{so } \ln(b/a) = \frac{2\pi \times 10^{-9} \times 8.26}{36\pi \times 96.8 \times 10^{-12}} = 1.297$$

$$\therefore \frac{b}{a} = 3.6585, \text{ so } \boxed{b = 0.713 \text{ in or } 1.81 \text{ cm}}$$

$$4.29 \quad U_2 = \iiint \vec{D} \cdot \vec{E} dV = \frac{1}{2} \int_0^{2\pi} \int_0^b \int_0^l \frac{\epsilon_1 V^2 \rho d\phi dz dp}{\rho^2 [\ln(b/a)]^2}$$

[using (4-71)]

$$+ \frac{1}{2} \int_{-\pi}^{0} \int_a^b \int_0^l \frac{\epsilon_2 V^2 \rho d\phi dz dp}{\rho^2 [\ln(b/a)]^2}$$

$$U_2 = \frac{\pi V^2 l}{2 (\ln(b/a))^2} (\epsilon_1 + \epsilon_2) = \frac{1}{2} C V^2$$

$$\therefore C = \frac{\pi l}{\ln(b/a)} (\epsilon_1 + \epsilon_2)$$

4-61

 $30 \rightarrow 500 \text{ pF}$ in 0 to 260°

$$V = 5000 \text{ V}$$

$$T = \frac{\partial U_e}{\partial \theta} = \frac{\Delta U_e}{\Delta \theta}$$

$$\text{and } U_e = \frac{1}{2} CV^2.$$

$$\text{so } \Delta U_e = \frac{1}{2} V^2 (30 - 500) \times 10^{-12} = -V^2 \frac{470}{2} \times 10^{-12}$$

$$T = - \frac{85 \times 10^6 \times 470 \times 10^{-12}}{2 \times 260 \times \pi / 180} = 1.294 \times 10^{-3} \text{ N-m}$$