

$$1-2 \quad \vec{A} = 5\vec{a}_x + 3\vec{a}_y + 4\vec{a}_z, \quad \vec{B} = 2\vec{a}_y + \vec{a}_z, \quad \vec{C} = -6\vec{a}_z$$

$$a) \vec{A} + \vec{B} + \vec{C} = 5\vec{a}_x + 5\vec{a}_y - \vec{a}_z$$

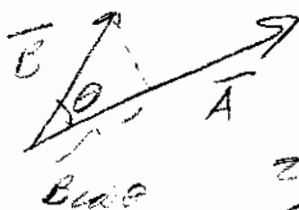
$$b) |\vec{A}| = \sqrt{5^2 + 3^2 + 4^2} = \sqrt{50} = 7.07$$

$$|\vec{B}| = \sqrt{51} = 7.14$$

$$c) 2\vec{A} - \vec{C} = \vec{E} = 10\vec{a}_x + 6\vec{a}_y + 14\vec{a}_z$$

$$|\vec{E}| = \sqrt{332} = 18.22$$

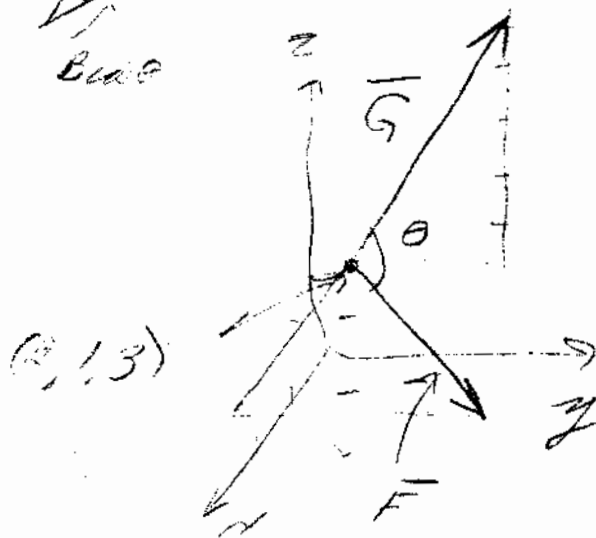
1-8



$$a) \vec{A} \cdot \vec{B} = AB \cos \theta = |\vec{A}| \times \text{projection of } \vec{B} \text{ on } \vec{A}$$

$$\vec{F} = 30\vec{a}_x + 40\vec{a}_y; \quad \vec{G} = 20\vec{a}_y + 50\vec{a}_z$$

b)



$$\vec{F} \cdot \vec{G} = 800 = FG \cos \theta$$

$$= FG \cos \theta \times \sqrt{2900}$$

$$\text{or } FG \cos \theta = \frac{800}{\sqrt{2900}} = 14.96$$

$$\cos \theta = \frac{14.96}{FG} = 0.297$$

$$\therefore \theta = 72.72^\circ$$

1-11



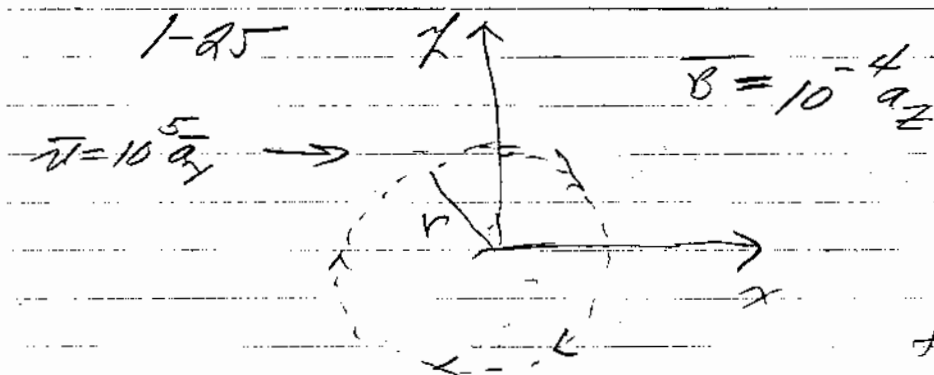
$$\vec{C} = \vec{A} + \vec{B}$$

$$\vec{C} \cdot \vec{C} = \vec{A} \cdot \vec{A} + \vec{B} \cdot \vec{B} + 2\vec{A} \cdot \vec{B} \cos \alpha = C^2$$

$$\text{but } \alpha = 180^\circ - \theta$$

$$\cos(180^\circ - \theta) = -\cos \theta$$

$$\therefore C^2 = A^2 + B^2 - 2AB \cos \theta$$

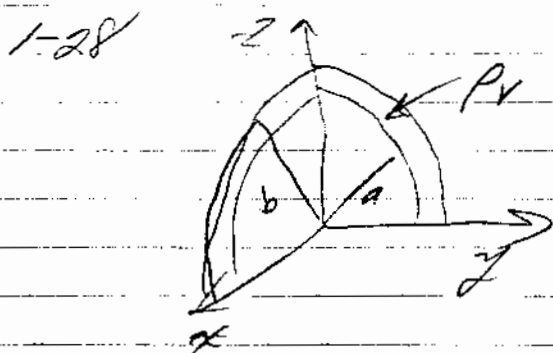


$$[\vec{F}_{\text{initial}} = -q\vec{v} \times \vec{B} = 10^2 \hat{a}_y]$$

force is always normal to $\vec{v}$ and constant so path is a circle ($|\vec{v}| = \text{constant}$)

$$r = ? = \frac{mv^2}{F} = \frac{9.1 \times 10^{-31} \times 10^{10}}{1.6 \times 10^{-19} \times 10} = 5.688 \times 10^{-3} \text{ m}$$

for no deflection $\vec{E} = \vec{v} \times \vec{B} = -10^5 \hat{a}_x \times 10^{-4} \hat{a}_z = 10 \hat{a}_y$



for $r < a$ charge enclosed = 0 and for any spherical charge distribution $\vec{E} = E(r) \hat{a}_r$

$$\therefore 4\pi r^2 \epsilon_0 E_r = 0 \quad \text{for } r < a$$

$$\text{so } E_r = 0 \quad \text{for } r < a$$

for $a < r < b$ we have: $4\pi r^2 \epsilon_0 E_r = \int_a^r \int_0^\pi \int_0^{2\pi} \rho_v r'^2 \sin\theta' d\theta' d\phi' dr'$

or $4\pi r^2 \epsilon_0 E_r = 4\pi \rho_v \left\{ \frac{r^3}{3} - \frac{a^3}{3} \right\}$

$$\text{and } E_r = \frac{\rho_v}{\epsilon_0} \left\{ \frac{r}{3} - \frac{a^3}{3r^2} \right\}$$

for $r > b$ $4\pi r^2 \epsilon_0 E_r = 4\pi \rho_v \left\{ \frac{b^3}{3} - \frac{a^3}{3} \right\}$

$$\text{or } E_r = \frac{\rho_v}{3\epsilon_0 r^2} \{b^3 - a^3\}$$

1-29 for $r < a$ $\rho_v = \rho_0(1+kr)$

$$q_{\text{total}} = \text{total charge} = \int_{r=0}^a \int_{\phi=0}^{2\pi} \int_{\theta=0}^{\pi} \rho_0(1+kr) r^2 \sin\theta d\theta d\phi dr$$

$$q_{\text{total}} = \frac{4}{3}\pi a^3 \rho_0 + k\rho_0 \frac{a^4}{4} 4\pi = 0 \quad \text{when } \frac{1}{3} = -k\frac{a}{4} \text{ or } \boxed{k = -\frac{4}{3a}}$$

for $r > a$ in this case Gauss's Law gives:

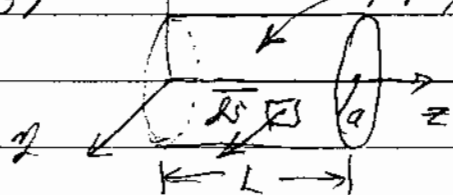
$$\epsilon_0 E_r 4\pi r^2 = 0 \quad \therefore \quad E_r = 0 \quad \leftarrow$$

for $r < a$ $\epsilon_0 E_r 4\pi r^2 = \int_{r=0}^r \int_{\phi=0}^{2\pi} \int_{\theta=0}^{\pi} \rho_0(1-\frac{4r}{3a}) r^2 \sin\theta d\theta d\phi dr$

$$= 4\pi \rho_0 \left[\frac{r^3}{3} - \frac{4r^4}{4 \cdot 3a} \right]$$

$$\text{so } E_r = \frac{\rho_0}{\epsilon_0} \left[\frac{r}{3} - \frac{r^2}{3a} \right] \quad \leftarrow$$

1-31 $\rho_v = \rho_0 \left(\frac{r}{a}\right)^2$



$$Q = \int_{z=0}^L \int_{\phi=0}^{2\pi} \int_{\rho=0}^a \rho_0 \left(\frac{r}{a}\right)^2 d\rho d\phi dz$$

$$Q = L 2\pi \frac{\rho_0}{a^2} \cdot \frac{a^4}{4} = \boxed{\rho_0 L \frac{\pi a^2}{2}} \quad \leftarrow$$

Gauss's Law $\rho > a$ $\int_{\phi=0}^{2\pi} \int_{z=0}^L \epsilon_0 E_p dz d\phi = Q = \epsilon_0 E_p L 2\pi$

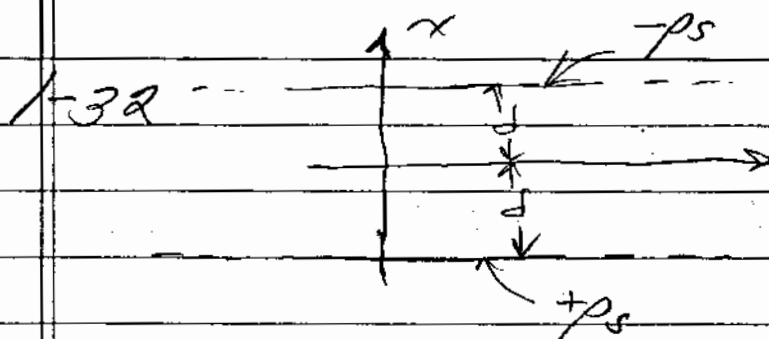
$$\therefore E_p = \frac{Q}{2\pi \epsilon_0 \rho L} = \frac{\rho_0 \pi a^2}{4\pi \epsilon_0 \rho} = \boxed{\frac{\rho_0 a^2}{4\epsilon_0 \rho}} \quad \leftarrow$$

or $\boxed{E_p = \frac{\rho}{2\pi \epsilon_0 \rho}} \quad \leftarrow$

for $\rho < a$ $\int_{\phi=0}^{2\pi} \int_{z=0}^L \epsilon_0 E_p dz d\phi = \int_{z=0}^L \int_{\phi=0}^{2\pi} \int_{\rho=0}^{\rho} \rho_0 \left(\frac{r}{a}\right)^2 d\rho d\phi dz$

$$\text{or } \epsilon_0 E_p \cancel{L} 2\pi \cancel{\rho} = \cancel{L} 2\pi \frac{\rho}{4a^2}$$

$$\therefore \boxed{E_p = \frac{\rho \rho}{4\epsilon_0 a^2}} \quad \leftarrow$$



- a) between the charged sheets both sheets produce a constant E_x in the positive x direction

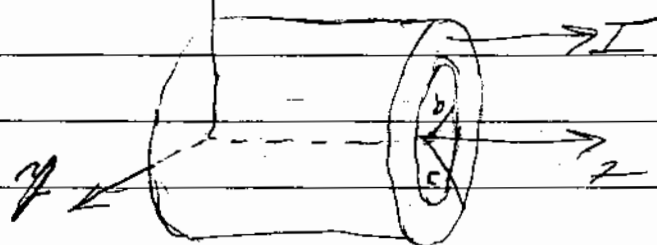
$$\therefore -d < x < d \quad \boxed{E_x = \frac{\rho_s}{\epsilon_0}} \quad \rightarrow$$

for $x > d$ or $x < -d$ fields cancel so $\boxed{E_x = 0}$ $\rightarrow$

- b) both sheets positively charged

$$\left. \begin{array}{ll} x > d & E_x = \frac{\rho_s}{\epsilon_0} \\ x < -d & E_x = -\frac{\rho_s}{\epsilon_0} \\ -d < x < d & E_x = 0 \end{array} \right\} \quad \leftarrow$$

EE 333



$$a) \vec{J} = \frac{I \vec{a}_z}{\pi c^2 - \pi b^2}$$

(assuming uniform current density $J = \frac{I}{\text{cross section area}}$)

$$b) \oint \frac{\vec{B}}{\mu_0} \cdot d\vec{l} = I \quad \text{for } \rho > c$$

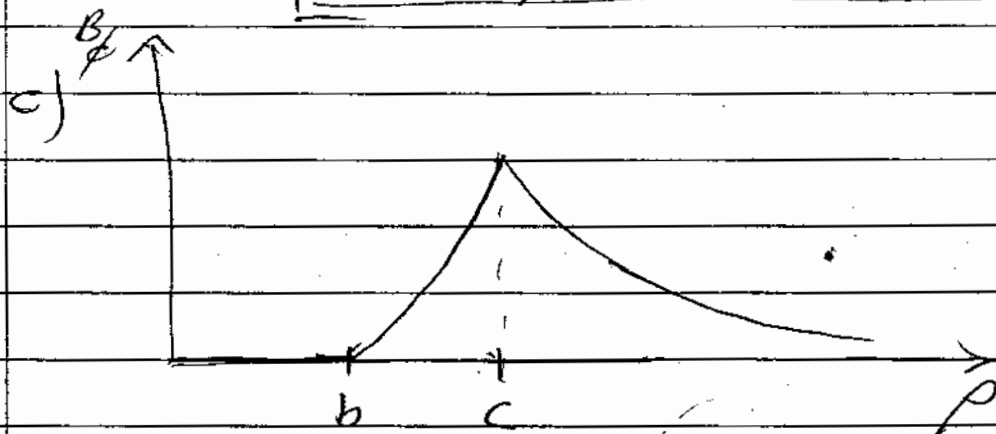
$$\int_0^{2\pi} \frac{B_\phi}{\mu_0} \rho d\phi = I \quad \text{or} \quad B_\phi = \frac{\mu_0 I}{2\pi \rho} \quad \text{for } \rho > c$$

$$\text{for } \rho < b \quad 2\pi \rho \frac{B_\phi}{\mu_0} = 0 \quad \text{or } B_\phi = 0$$

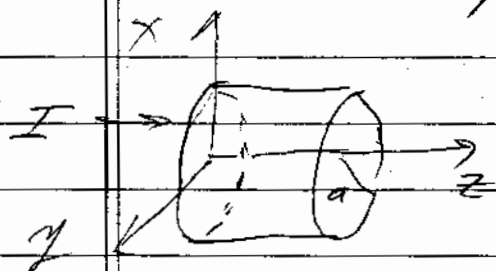
$$\text{for } a < \rho < b \quad 2\pi \rho \frac{B_\phi}{\mu_0} = \int_{\phi=0}^{2\pi} \int_{\rho=b}^{\rho} \frac{I \vec{a}_z}{\pi c^2 - \pi b^2} \cdot \rho d\phi d\rho$$

$$\text{or } 2\pi \rho \frac{B_\phi}{\mu_0} = \frac{2\pi I}{\pi(c^2 - b^2)} \cdot \frac{\rho^2}{2} \Big|_b^\rho = I \frac{\rho^2 - b^2}{c^2 - b^2}$$

$$\text{so } B_\phi = \frac{\mu_0 I}{2\pi \rho} \left[\frac{\rho^2 - b^2}{c^2 - b^2} \right] \quad b < \rho < c$$



1-35 from example 1-15



$$B_\phi = \frac{\mu_0 I}{2\pi p} \quad \text{for } p > b$$

$$B_\phi = \frac{\mu_0 I p}{2\pi(b^2 - a^2)} \quad \text{for } p < a$$

Using our solution to problem 1-33 and superposition we have

$$B_\phi = \frac{\mu_0 I p}{2\pi a^2} \quad \text{for } p < a$$

$$B_\phi = \frac{\mu_0 I}{2\pi p} \quad \text{for } a < p < b$$

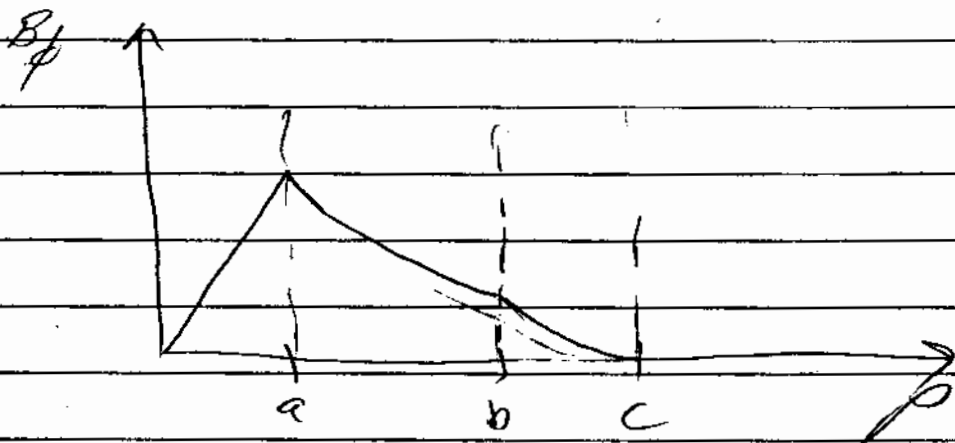
$$B_\phi = \frac{\mu_0 I}{2\pi p} - \frac{\mu_0 I}{2\pi p} \left[\frac{p^2 - b^2}{c^2 - b^2} \right] = \frac{\mu_0 I}{2\pi p} \left[\frac{c^2 - b^2 p^2 + b^2}{c^2 - b^2} \right]$$

$$B_\phi = \frac{\mu_0 I}{2\pi p} \left[\frac{c^2 - p^2}{c^2 - b^2} \right] \quad b < p < c$$

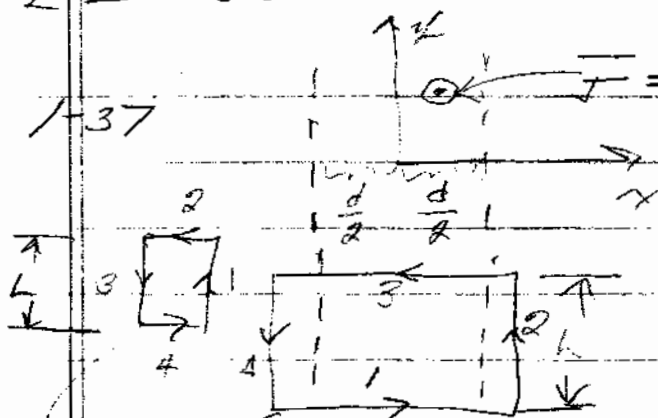
Same as
answer to
1-34

$$B_\phi = 0 \quad \text{for } p > c$$

(no current enclosed)



1-37



$$\vec{J} = J_z \vec{a}_z$$

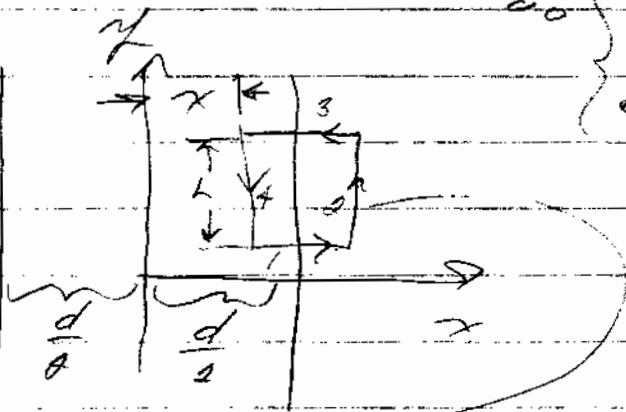
From direct current problem we know that $\vec{B}$ is only in the $\pm y$ direction

for this constant

$$\frac{B_{y1}}{\mu_0} - \frac{B_{y2}}{\mu_0} = 0 \quad \Rightarrow \quad \left\{ \begin{array}{l} B_y = \text{constant} \\ \text{outside of slab} \end{array} \right.$$

$$\frac{B_{y1}}{\mu_0} x + \frac{B_{y2}}{\mu_0} x = J_z x d$$

$$\left\{ \begin{array}{l} B_{y1} = \frac{\mu_0 J_z d}{2} \text{ for } x > d \\ B_{y2} = -\frac{\mu_0 J_z d}{2} \text{ for } x < d \end{array} \right.$$



$$\frac{\mu_0 J_z d}{\mu_0} x - \frac{B_{y1}}{\mu_0} x = J_z x \left(\frac{d}{2} - x \right)$$

$$\text{so } B_{y1} = \frac{\mu_0 J_z d}{2} - \mu_0 J_z \left(\frac{d}{2} - x \right) = \mu_0 J_z x \quad \text{or } B_{y1} = \mu_0 J_z x$$

$$2-17 \quad \vec{E} = \frac{\rho_0}{\epsilon_0} \left(\frac{r}{3} - \frac{r^2}{3a} \right) \vec{a}_r$$

$$\nabla \cdot \vec{E} = \frac{1}{r^2} \frac{d}{dr} \left[\frac{\rho_0}{\epsilon_0} \left(\frac{r^3}{3} - \frac{r^4}{3a} \right) \right] = \frac{\rho_0}{r^2 \epsilon_0} \left[r^2 - \frac{4}{3} r^3 \right]$$

$$\text{or } \nabla \cdot \vec{E} = \frac{\rho_v}{\epsilon_0}$$

2-41 $\vec{E}_r^+ = 1225 e^{-j\beta_0 z}$ $f = 10^8$

- a) amplitude = 1225 V/m
 traveling in +z direction
 vector direction $\hat{a}_x$ (x polarization)

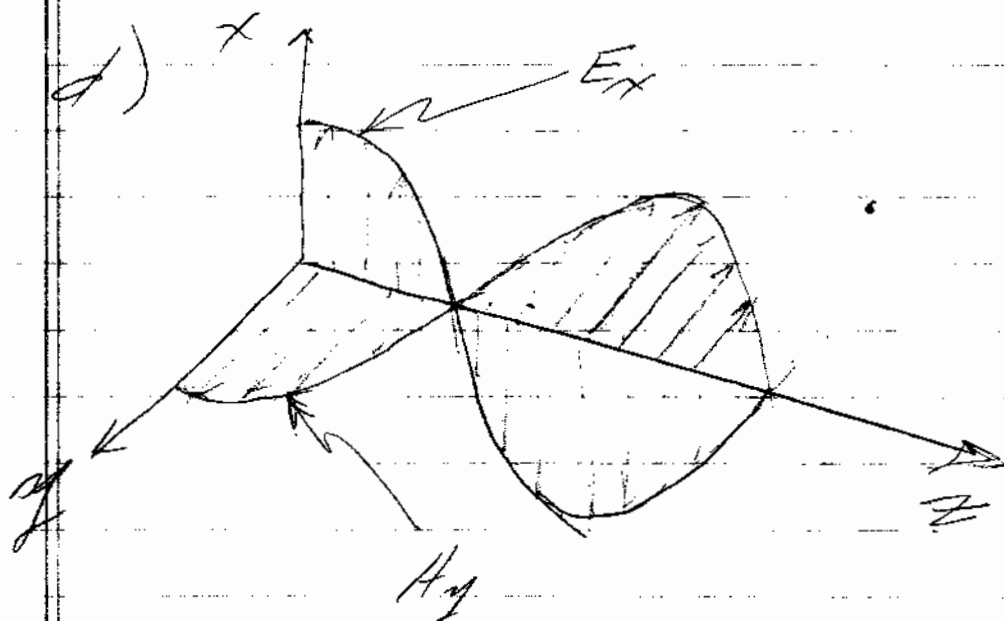
b) $E_x = 1225 \cos(\omega t - \beta_0 z) = 1225 \cos(2\pi \times 10^8 t - \beta_0 z)$
 where $\beta_0 = \frac{\omega}{c} = \frac{2\pi \times 10^8}{3 \times 10^8} = 2.094$

$$\lambda = \frac{c}{f} = \frac{3 \times 10^8}{10^8} = 3 \text{ m}$$

c) $\vec{B}_y^+ = \frac{1225}{c} e^{-j\beta_0 z} = \frac{1225}{3 \times 10^8} e^{-j\beta_0 z} = 4.08 \times 10^{-7} e^{-j\beta_0 z}$

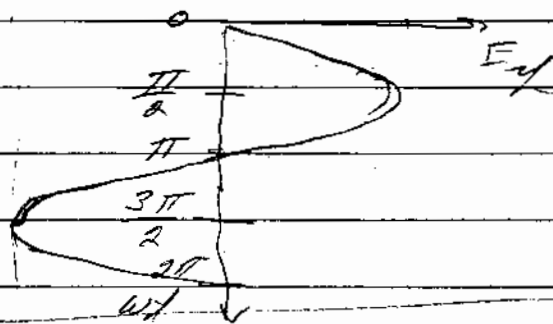
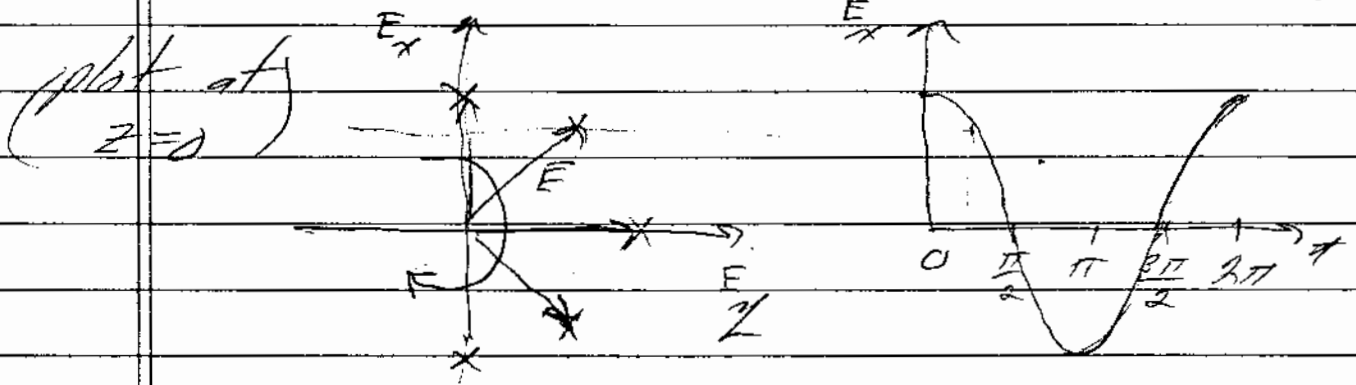
$\vec{H}_y^+ = \frac{1225}{377} e^{-j\beta_0 z} = 3.25 e^{-j\beta_0 z}$

so $H_y = 3.25 \cos(2\pi \times 10^8 t - \beta_0 z)$



2-46 $\vec{E}(z) = 500 e^{-j\beta_0 z} (\vec{a}_x - j\vec{a}_y)$

$$\vec{E} = 500 \cos(\omega t - \beta_0 z) \vec{a}_x + 500 \sin(\omega t - \beta_0 z) \vec{a}_y$$



right hand or
clockwise circular
polarization

$$\vec{H}_z = \frac{500}{\eta_0} e^{-j\beta_0 z} \vec{a}_y + j \frac{500}{\eta_0} e^{-j\beta_0 z} \vec{a}_x$$

3.1 $n = 10^{29}$; $\sigma = 5.8 \times 10^7 \text{ mho/m}$

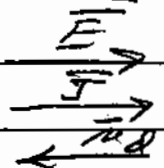
a) $\mu_e = \frac{2\pi\epsilon_0}{m}$; $\sigma = \frac{n e^2}{m} \tau_c$

$$\frac{\sigma}{\omega} \mu_e = \sigma \left(\frac{1}{\omega^2} \right) = \frac{5.8 \times 10^7}{10^{29} \times 1.6 \times 10^{-19}} = 3.625 \times 10^{-3}$$

b) charge density = $-10^{29} \frac{\text{elec}}{\text{m}^3} \times \frac{1.6 \times 10^{-19} \text{C}}{\text{elec}} \times \frac{1 \text{m}^3}{10^9 \text{mm}^3} = -16 \frac{\text{C}}{\text{mm}^3}$

c) $E = 1 \vec{a}_x$; $\vec{D} = \epsilon_0 \vec{E} = 3.625 \times 10^{-3} \text{ m/sec}$

$$\vec{J} = \sigma \vec{E} = 5.8 \times 10^7 \vec{a}_x \text{ A/m}^2$$



Homework 6 (alternate solution)

$$2-46 \quad \vec{E}_z = 500 e^{-j\beta_0 z} (\hat{a}_x - j\hat{a}_y)$$

$$\nabla \times \vec{E} = -j\omega \vec{B}$$

$$\begin{vmatrix} \hat{a}_x & \hat{a}_y & \hat{a}_z \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ \hat{E}_x & \hat{E}_y & \hat{E}_z \end{vmatrix} = -j\omega (\hat{B}_x \hat{a}_x + \hat{B}_y \hat{a}_y + \hat{B}_z \hat{a}_z)$$

$$\text{or } \frac{\partial \hat{E}_y}{\partial z} = j\omega \hat{B}_x$$

$$\frac{\partial \hat{E}_x}{\partial z} = -j\omega \hat{B}_y$$

$$\hat{B}_z = 0$$

∴ for above $\vec{E}$ field we have:

$$\hat{B}_x = \frac{1}{j\omega} \frac{\partial \hat{E}_y}{\partial z} = \frac{1}{j\omega} (-j) (-j\beta_0) 500 e^{-j\beta_0 z}$$

$$\hat{B}_x = j \frac{\omega \sqrt{\mu_0 \epsilon_0}}{\omega} 500 e^{-j\beta_0 z}$$

$$\text{or } \hat{B}_x = j \frac{500}{\eta_0} e^{-j\beta_0 z} \quad \leftarrow$$

$$\text{similarly } \hat{B}_y = \frac{-1}{j\omega} 500 (j\beta_0) e^{-j\beta_0 z}$$

$$\hat{B}_y = \frac{500}{\eta_0} e^{-j\beta_0 z}$$

$$\text{and } \hat{B}_y = \frac{300}{\eta_0} e^{-j\beta_0 z} \quad \leftarrow$$

3.3 He $10^{25} \text{ atoms/m}^3$; $\chi_e = 1.5 \times 10^{-4}$; $E = 10^3 \text{ V/m}$

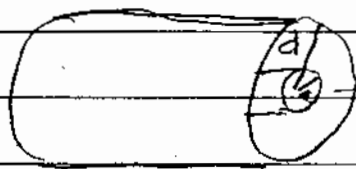
a) $\bar{P} = \epsilon_0 \chi_e \bar{E} = \frac{10^{-9}}{36\pi} \times 1.5 \times 10^{-4} \times 10^3 = \boxed{1.33 \times 10^{-12}} \leftarrow$

b) $\rho_v^+ = \overset{2 \text{ electrons/atom}}{2} \times 10^{25} \times 1.6 \times 10^{-19} = \boxed{3.2 \times 10^6 \text{ C/m}^3}$

$\bar{P} = \rho_v^+ \bar{\ell}_{\text{ave}} \therefore \bar{\ell}_{\text{ave}} = \frac{1.33 \times 10^{-12}}{3.2 \times 10^6} = \boxed{4.16 \times 10^{-19} \text{ m}}$

c) $\epsilon_r = 1 + \chi_e = \boxed{1.00015} \leftarrow$

3-12



$\oint \vec{D} \cdot d\vec{s} = \rho_L L$ charge/m
 $\int_{z=0}^L \int_{\phi=0}^{2\pi} D_{\phi} \rho d\phi dz = \rho_L L$

or $2\pi \rho L D_{\phi} = \rho_L L \therefore D_{\phi} = \frac{\rho_L}{2\pi \rho} ; \boxed{E_{\phi} = \frac{\rho_L}{2\pi \epsilon \rho}} \leftarrow$

a) E_r is constant if $\boxed{\epsilon = \frac{K}{\rho}} \leftarrow$

want $\epsilon = \epsilon_1$ @ $\rho = d \therefore \boxed{K = d\epsilon_1} \leftarrow$

and $\boxed{E_p = \frac{\rho_L}{2\pi \epsilon_1 d}} \leftarrow$

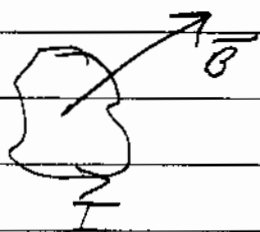
b) $\rho_p = \epsilon_0 E_p + \rho$ so $\rho = \rho - \epsilon_0 E_p = \frac{\rho_L}{2\pi \rho} - \frac{\epsilon_0 \rho_L}{2\pi \epsilon_1 d}$

$\boxed{\rho = \frac{\rho_L}{2\pi} \left(\frac{1}{\rho} - \frac{\epsilon_0}{\epsilon_1 d} \right)}$

$\rho_p = -\nabla \cdot \vec{P} = -\frac{1}{\rho} \frac{\partial}{\partial \rho} \left(\frac{\rho_L \epsilon_0 \rho}{2\pi \epsilon_1 d} \right) = \boxed{\frac{\rho_L \epsilon_0}{2\pi \epsilon_1 d \rho}} \leftarrow$

c) Use layers that approximate $\frac{\epsilon_0}{\rho}$ variation $\leftarrow$

3.16



$$\vec{F} = \oint \vec{dl} \times \vec{B}$$

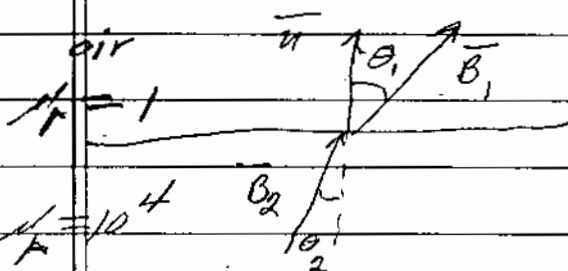
$$\vec{F} = \oint I \vec{dl} \times \vec{B} = -I \oint \vec{B} \times \vec{dl}$$

$$\vec{F} = -I \vec{B} \times \oint \vec{dl} \equiv 0 \quad \leftarrow$$

3.25

$$H_1 = H_2$$

$$B_{n1} = B_{n2}$$

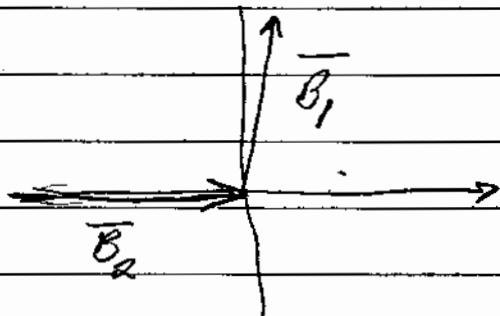


$$\tan \theta_2 = \frac{\mu_2}{\mu_1} \tan \theta_1 \quad (3.76)$$

$$\text{or } \theta_1 = \tan^{-1} [10^{-4} \tan \theta_2]$$

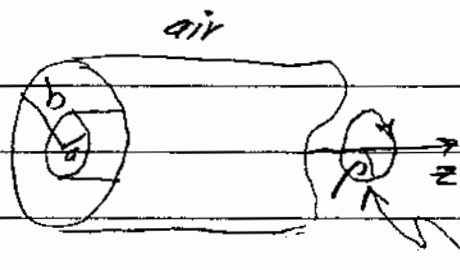
θ_2	θ_1
0°	0
45°	$5.7 \times 10^{-3}^\circ$
89°	0.338°
89.9°	3.27°
89.9675°	10° ✓

①



②

3-28



I carried in conductor of radius " a " ($\mu = \mu_0$)

for $a < p < b$ $\mu = \mu$

$$\oint \vec{H} \cdot d\vec{l} = \int \vec{J} \cdot d\vec{S} \quad \text{Integrate around circular contour}$$

a) for $p < a$ $H \phi 2\pi p = \frac{I}{\pi a^2} \pi p^2$ or $H \phi = \frac{I p}{2\pi a^2}$

$$B \phi = \frac{\mu_0 I p}{2\pi a^2}$$

for $a < p < b$

$$H \phi = \frac{I}{2\pi p}$$

$$B \phi = \frac{\mu I}{2\pi p}$$

for $p > b$

$$H \phi = \frac{I}{2\pi p}$$

$$B \phi = \frac{\mu_0 I}{2\pi p}$$

b) $M = \frac{B}{\mu_0} - H = \frac{1}{\mu_0} \left[\frac{\mu I}{2\pi p} - \frac{I}{2\pi p} \right] = \frac{I}{2\pi p} [\mu - \mu_0]$

$H \phi$ is continuous across all boundaries (H-tangential)

$B \phi$ is discontinuous

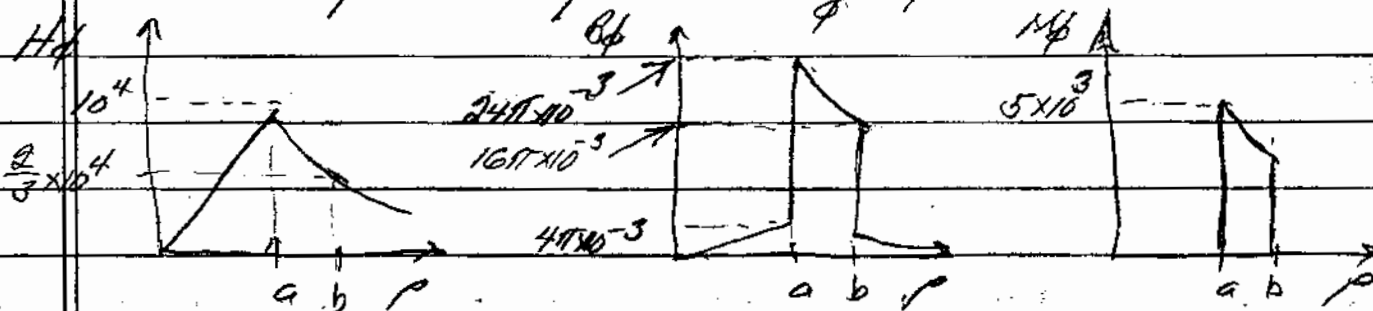
$$B \phi = 84\pi \times 10^{-3} \quad (p = a^+)$$

@ $p = a$ $H \phi = \frac{628}{2\pi \times 10^{-2}} = 10^4$; $B \phi = 4\pi \times 10^{-3} \quad (p = a^-)$

$p = b$ $H \phi = \frac{628}{2\pi \times 1.5 \times 10^{-2}} = \frac{2}{3} \times 10^4$; $B \phi = 4\pi \times 10^{-7} \times 6 \times \frac{2}{3} \times 10^4 = 16\pi \times 10^{-3}$

$$B \phi = \frac{2}{3} \pi \times 10^{-3} \quad (p = b^+)$$

$M = 0$ for $p < a$ and $p > b$ $M = \frac{50}{p} \quad a < p < b$

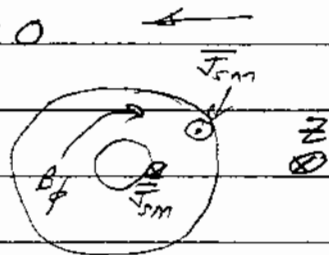


3.28 continued: $\vec{J}_m = \nabla \times \vec{M}$

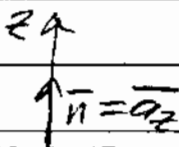
$$\therefore \vec{J}_m = \vec{a}_\rho \left(-\frac{\partial M_\phi}{\partial z} \right) + \vec{a}_z \left(\frac{1}{\rho} \frac{\partial}{\partial \rho} (\rho M_\phi) \right) = 0$$

$$\vec{J}_{sm}(\rho=a) = \vec{a}_\rho \times \vec{M} = 5 \times 10^3 \vec{a}_z$$

$$\vec{J}_{sm}(\rho=b) = -\vec{a}_\rho \times \vec{M} = -\frac{10}{3} \times 10^3 \vec{a}_z$$



3.29

Region 1 $\epsilon = \epsilon_0$ Region 2 $\epsilon = 4\epsilon_0$

$$\vec{E}_1 = -15\vec{a}_x + 20\vec{a}_y + 30\vec{a}_z$$

$$\begin{cases} E_{tang,1} = E_{tang,2} \\ D_{norm,1} = D_{norm,2} \end{cases}$$

$$a) \boxed{\vec{E}_2 = -15\vec{a}_x + 20\vec{a}_y + \frac{15}{2}\vec{a}_z} \leftrightarrow \begin{cases} D_{z,1} = 30\epsilon_0 = D_{z,2} \\ E_{z,2} = \frac{D_{z,2}}{4\epsilon_0} = \frac{30}{4} \end{cases}$$

$$\vec{D}_1 = \epsilon_0 \vec{E}_1$$

$$\vec{D}_2 = 4\epsilon_0 \vec{E}_2$$

$$b) \vec{n} \cdot \vec{E}_1 = |\vec{E}_1| \cos \theta_1 = 30 \quad \therefore \theta_1 = \cos^{-1} \left\{ \frac{30}{\sqrt{15^2 + 20^2 + 30^2}} \right\} = 39.8^\circ$$

$$\theta_2 = \cos^{-1} \left\{ \frac{\frac{15}{2}}{\sqrt{15^2 + 20^2 + 7.5^2}} \right\} = 73.3^\circ$$

$$c) \tan \theta_2 = \frac{\epsilon_2}{\epsilon_1} \tan \theta_1$$

$$3.333 = 4 \times 0.833$$

$$3.333 = 3.333 \quad !$$

3-38

$$\begin{aligned} E_m^+ &= 1 \quad @ \quad z=0 \quad \left\{ \begin{array}{l} \text{sea water} \\ \epsilon_r = 81, \quad \sigma = 4 \end{array} \right\} \\ f &= 10^4 \end{aligned}$$

$$\frac{\sigma}{\omega \epsilon} = \frac{4 \times 36\pi}{81\pi \times 10^4 \times 10^{-9}} = 7.2 \times 10^5 \gg 1 \quad \therefore \text{good conductor}$$

$$\text{so } \alpha = \beta = \sqrt{\frac{\omega \mu}{2}} = \sqrt{\frac{2\pi \times 10^4 \times 4 \times 4\pi \times 10^{-7}}{2}} = 0.397 \text{ A}$$

$$\text{for } e^{-\alpha z} = 0.05 \quad (5\%) ; \quad z = -\frac{\ln 0.05}{\alpha} = 7.5 \text{ m} \leftarrow$$

$$\text{if } f = 10^3 ; \quad \frac{\sigma}{\omega \epsilon} = 7.2 \times 10^7 \quad (\text{good conductor})$$

$$\alpha = \beta = 4\pi \times 10^{-2} = 0.1257 \leftarrow$$

$$z_{5\%} = -\frac{\ln 0.05}{0.1257} = 23.8 \text{ m} \leftarrow$$

Thus demonstrating the rf communication in sea water is only possible at very low frequencies.

3-37 $\hat{E}_m^+ = 200 \text{ V/m}$; $f = 10^8 \text{ Hz}$, $\mu = \mu_0$
 $\epsilon = 6\epsilon_0$, $\sigma = 10^{-2} \text{ S/m}$

$$\gamma = 0.761 + j5.187$$

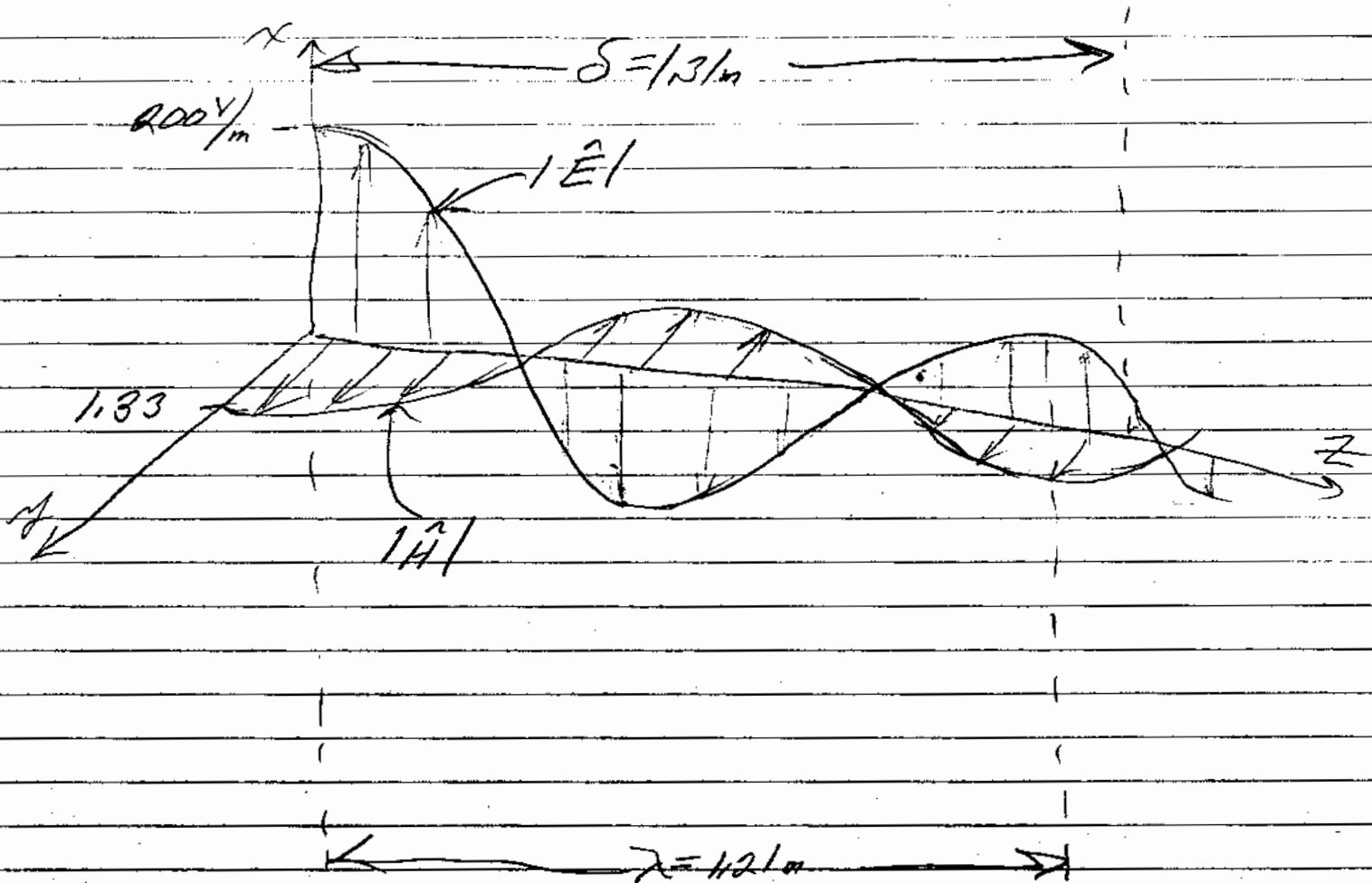
a) $\lambda = \frac{2\pi}{\beta} = 1.2 \text{ m}$

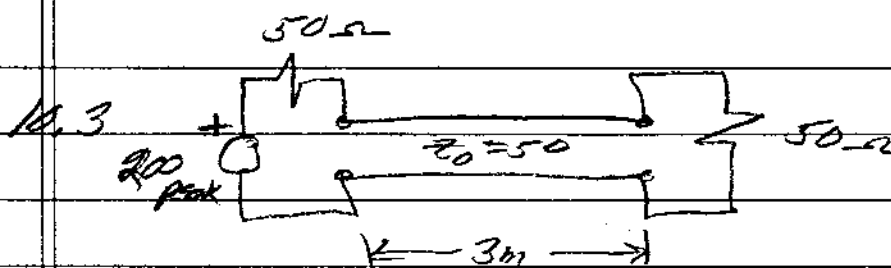
$\delta = \frac{1}{\alpha} = 1.3 \text{ m}$

$v_{ph} = \frac{\omega}{\beta} = \frac{2\pi \times 10^8}{5.187} = 1.21 \times 10^8 \text{ m/sec}$

b) $\hat{\eta} = \sqrt{\frac{\mu}{\epsilon - j\frac{\sigma}{\omega}}} = \sqrt{\frac{4\pi \times 10^{-7}}{\frac{6 \times 10^{-9}}{360\pi} - j \frac{10^{-2}}{2\pi \times 10^8}}} = 1.506 \times 10^2 \angle -8.34^\circ$

$\therefore \frac{\hat{H}^+}{\hat{E}^+} = \frac{200}{\hat{\eta}} = 1.33 \angle -8.34^\circ$





$$f = 50 \text{ MHz}$$

$$\epsilon_r = 2.25$$

$$v_{ph} = \frac{3 \times 10^8}{\sqrt{2.25}} = 2 \times 10^8 \text{ m/sec} ; \lambda = \frac{2 \times 10^8}{5 \times 10^7} = 4 \text{ m}$$

$$\text{so line length} = \frac{3}{4} \lambda$$

$$a) \Gamma(z) = \frac{Z_L - Z_0}{Z_L + Z_0} = 0 \quad \therefore \Gamma(z) \text{ is zero at all points on the line}$$

$$Z(z) = Z_0 \frac{1 + \Gamma(z)}{1 - \Gamma(z)} = Z_0 \text{ everywhere}$$

$$b) \hat{V}(z) = \hat{V}_m^+ e^{-j\beta z} ; \hat{I}(z) = \frac{\hat{V}_m^+}{Z_0} e^{-j\beta z}$$

$$\text{these become } \hat{V}_m^+ \text{ and } \hat{V}_m^+/Z_0 \text{ at } z=0$$

$$c) \hat{I}_{in} = \hat{I}_m^+ = \frac{\hat{V}_m^+}{Z_0} = \frac{200}{100} = 2 \text{ A} ; \hat{V}_m = \hat{V}_m^+ = 100$$

$$\therefore \hat{V}(z) = 100 e^{-j\beta z} = 100 e^{-j \frac{2\pi}{\lambda} z}$$

$$\hat{I}(z) = 2 e^{-j\beta z} = 2 e^{-j \frac{2\pi}{\lambda} z}$$

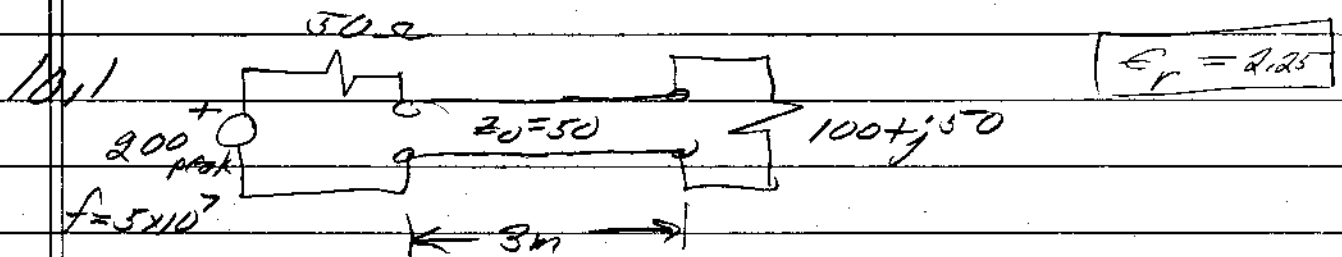
$$P_{in, ave} = \frac{1}{2} 100 \times 2 = 100 \text{ Watts}$$

$$\hat{V}_{load} = 100 e^{-j \frac{2\pi}{\lambda} (\frac{3\lambda}{4})} = 100 e^{-j \frac{3\pi}{2}} = j100$$

$$\text{so } \hat{I}_{load} = j2$$

$$\text{and } P_{load} = \frac{1}{2} \text{Re}\{j100 (-j2)\} = 100 \text{ Watts}$$

$$\text{or } P_{load} = \frac{1}{2} |\hat{I}|^2 50 = \frac{1}{2} \frac{100^2}{50} = 100 \text{ W}$$



$$\beta = j\omega \sqrt{\mu\epsilon} = j\omega \frac{\sqrt{2.25}}{3 \times 10^8} = j2\pi \times 5 \times 10^7 \frac{1.5}{3 \times 10^8} = j\frac{1}{2}\pi$$

$$v_p = \frac{3 \times 10^8}{\sqrt{\epsilon_r}} = 2 \times 10^8 \text{ m/sec} ; \lambda = \frac{2\pi}{\beta} = 4 \text{ m} \quad \text{line length} = \frac{3}{4}\lambda$$

$$\Gamma_{\text{load}} = \frac{Z_L - Z_0}{Z_L + Z_0} = \frac{50 + j50}{150 + j50} = 0.4 + j0.2 = 0.4472 \angle 26.565^\circ$$

$$\Gamma_{\text{in}} = \Gamma_{\text{load}} e^{-j2\beta(\frac{3\lambda}{4})} = (0.4 + j0.2) e^{-j3\pi} = -(0.4 + j0.2) = -0.4472 \angle 26.56^\circ$$

$\therefore$ approximately 45% voltage reflection

$$Z_{\text{in}} = 50 \frac{1 + \Gamma_{\text{in}}}{1 - \Gamma_{\text{in}}} = 50 \frac{0.6 - j0.2}{1.4 + j0.2} = 20 - j10$$

$$I_{\text{in}} = \frac{200}{50 + Z_{\text{in}}} = \frac{200}{70 - j10} = 2.828 \angle 8.13^\circ$$

$$P_{\text{in}} = \frac{1}{2} |I_{\text{in}}|^2 R_{\text{in}} = \frac{1}{2} (2.828)^2 (20) = 79.98 \text{ Watts}$$

$$I = \hat{I}_m e^{-j\beta z} [1 - \Gamma(z)] \quad \therefore \hat{I}_m = \frac{I_{\text{in}}}{1 - \Gamma(0)}$$

$$\text{so } \hat{I}_{\text{load}} = \hat{I}_m e^{-j\frac{3\pi}{4}} [1 - \Gamma_{\text{load}}] = \hat{I}_{\text{in}} e^{-j\frac{3\pi}{4}} \frac{1 - \Gamma_{\text{load}}}{1 - \Gamma_{\text{in}}}$$

$$\text{or } \hat{I}_{\text{load}} = 2.828 \angle 8.13^\circ \frac{0.6 - j0.2}{1.4 + j0.2} = 1.2647 \angle 71.56^\circ$$

$$\therefore P_{\text{load}} = \frac{1}{2} (1.2647)^2 \times 100 = 79.97 \text{ Watts}$$

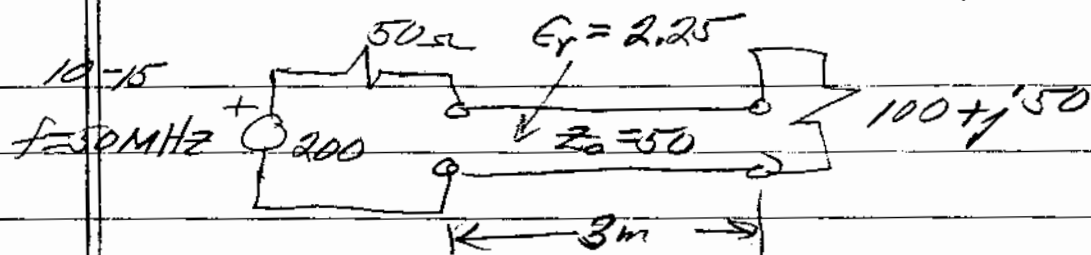
$$10.2 \quad P_{\text{ave}} = \frac{1}{2} \text{Re} \left\{ \hat{V}_m^+ e^{-j\beta z} [1 + \Gamma] \frac{\hat{V}_m^{+*}}{Z_0} e^{+j\beta z} [1 - \Gamma^*] \right\}$$

$$P_{\text{ave}} = \frac{1}{2} \text{Re} \left\{ \frac{|\hat{V}_m^+|^2}{Z_0} [1 - \Gamma^* + \Gamma - |\Gamma|^2] \right\}$$

$$\text{so } P_{\text{ave}} = \frac{|\hat{V}_m^+|^2}{2Z_0} [1 - |\Gamma|^2]$$

$$\Gamma = \frac{\hat{V}_m^-}{\hat{V}_m^+} e^{-j2\beta z} \quad \text{so } |\Gamma| = \frac{|\hat{V}_m^-|}{|\hat{V}_m^+|}$$

$$\text{so } P_{\text{ave}} = \frac{|\hat{V}_m^+|^2}{2Z_0} - \frac{|\hat{V}_m^-|^2}{2Z_0} = P_{\text{ave}}^+ - P_{\text{ave}}^-$$

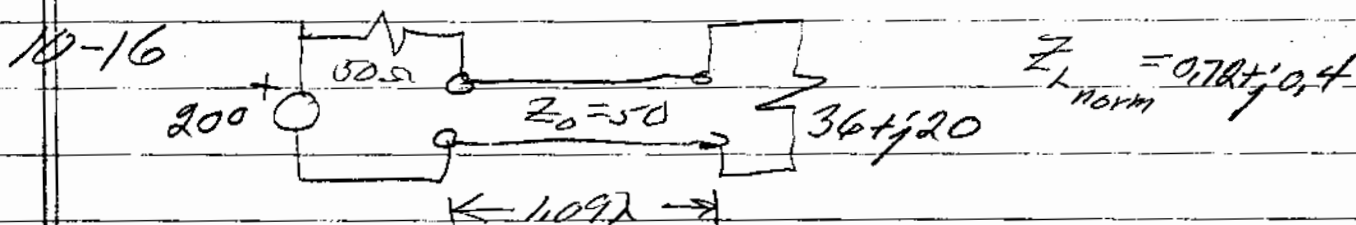


$$\lambda = \frac{3 \times 10^8}{5 \times 10^7 \times \sqrt{2.25}} = 4 \text{ m} \quad \therefore \text{line length} = \frac{3}{4} \lambda$$

$$Z_{L, \text{norm}} = 2 + j1 \quad ; \text{ from chart: } \Gamma_L = 0.46 \angle 26^\circ \leftarrow$$

$$[\text{chart scales } 0.214 + 0.25 = 0.464\lambda]$$

$$\text{from chart: } \left\{ \begin{array}{l} \Gamma_{in} = 0.46 \angle 154^\circ \\ Z_{in, \text{norm}} = 0.4 - j0.195 \text{ or } Z_{in} = 20 - j9.75 \end{array} \right\} \leftarrow$$



$$\text{from chart: } \Gamma_L = 0.29 \angle 112^\circ$$

$$\text{chart rotation} = 0.094 + 0.09 = 0.184\lambda$$

$$\text{from chart: } \Gamma_{in} = 0.29 \angle 48^\circ \text{ and } Z_{in, \text{norm}} = 1.32 + j0.58$$

$$\text{or } \boxed{Z_{in} = 66 + j29} \leftarrow$$

Problem
10-15

IMPEDANCE OR ADMITTANCE COORDINATES

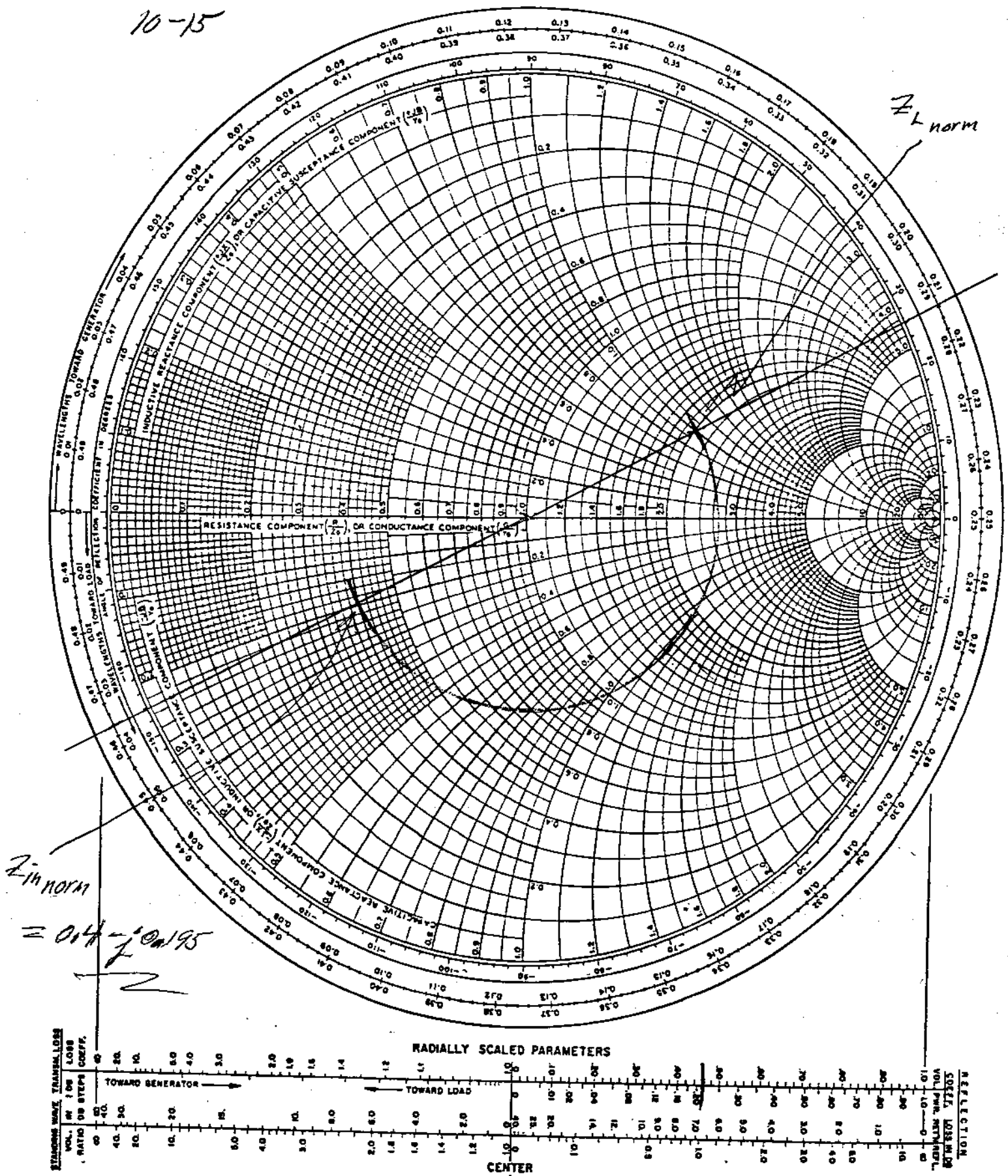


Fig. 9-3. A standard commercially available form of Smith chart graph paper. Copyrighted 1949 by Kay Electric Company, Pine Brook, N. J., and reprinted with their permission.

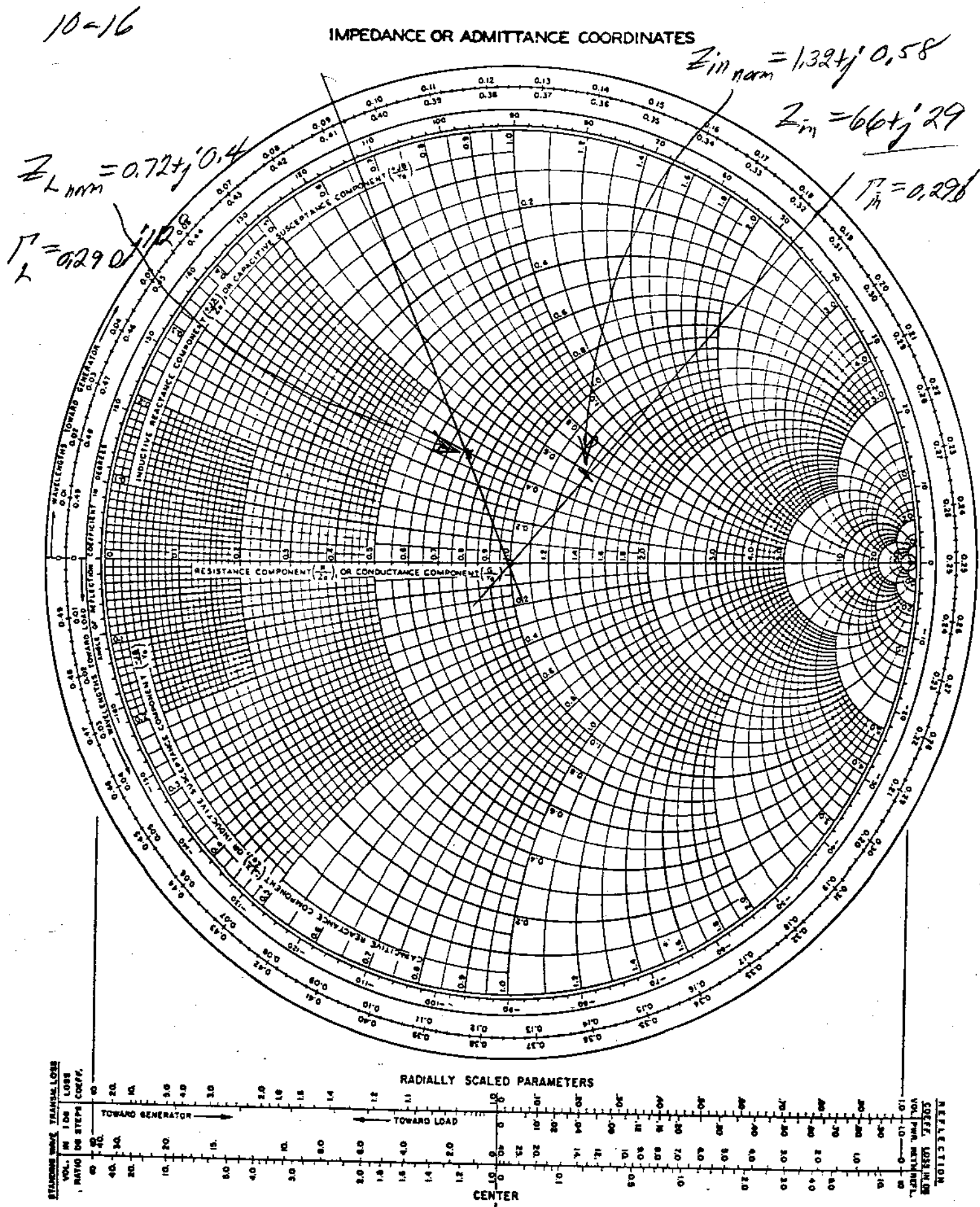


Fig. 9-3. A standard commercially available form of Smith chart graph paper. Copyrighted 1949 by Kay Electric Company, Pine Brook, N. J., and reprinted with their permission.

$$10-21 \quad Z_L = 36 + j20 \quad ; \quad Z_0 = 50$$

$$\therefore Z_{L_{\text{norm}}} = 0.72 + j0.4$$

from chart (next page)

$$\boxed{Y_{L_{\text{norm}}} = 1.07 - j0.59} \quad \leftarrow$$

$$\frac{1}{Z_{L_{\text{norm}}}} = \frac{1}{0.72 + j0.4} = \frac{1}{0.8237 \angle 29.05^\circ} = 1.214 \angle -29.05^\circ$$

$$\boxed{\text{or } \frac{1}{Z_{L_{\text{norm}}}} = 1.06 - j0.59} \quad \leftarrow$$

Problem
10-21

IMPEDANCE OR ADMITTANCE COORDINATES

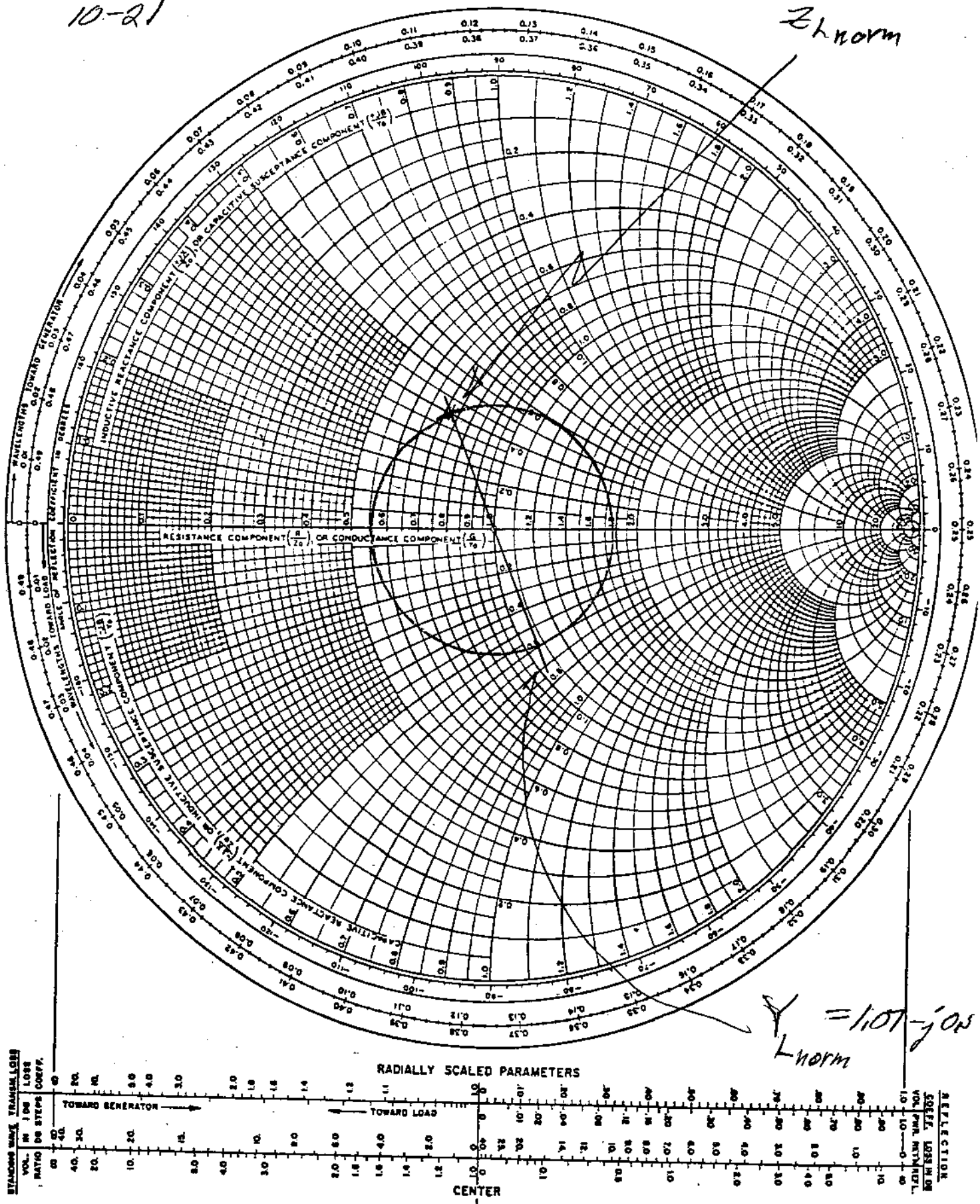
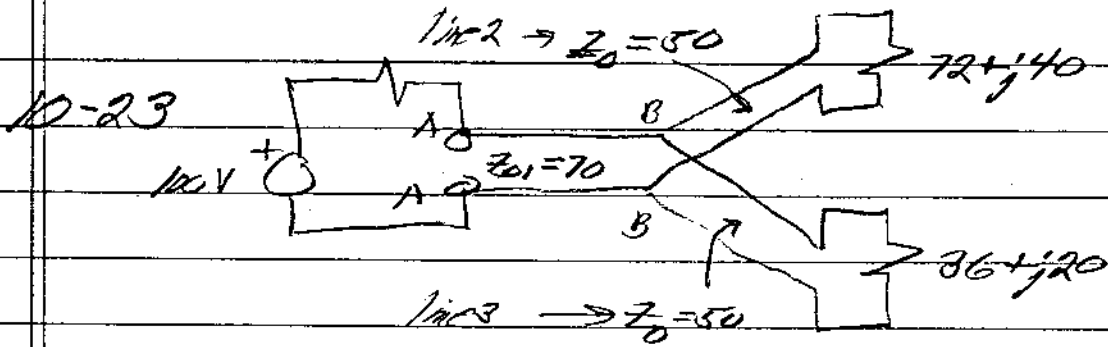


Fig. 9-3. A standard commercially available form of Smith chart graph paper. Copyrighted 1949 by Kay Electric Company, Pine Brook, N. J., and reprinted with their permission.



from example 10-6 $P_{ave \text{ into A-A}} = 8.5 \text{ Watts}$

$$Y_{in @ BB} = G_2 + jB_2 \quad ; \quad Y_{in @ BB} = G_3 + jB_3$$

$$P_{ave} = \frac{1}{2} R_0 \{ \tilde{V} \tilde{I}^* \} = \frac{1}{2} R_0 \{ \tilde{V} \tilde{V}^* Y^* \} = \frac{1}{2} |\tilde{V}|^2 G$$

$$\therefore \boxed{\frac{P_{ave2}}{P_{ave1}} = \frac{G_2}{G_3}} \quad \leftarrow$$

$$\frac{1}{2} |\tilde{V}|^2 (G_2 + G_3) = 8.5 = \frac{1}{2} |\tilde{V}|^2 G_2 \left(1 + \frac{G_3}{G_2} \right)$$

$$= P_{ave2} \left(1 + \frac{G_3}{G_2} \right)$$

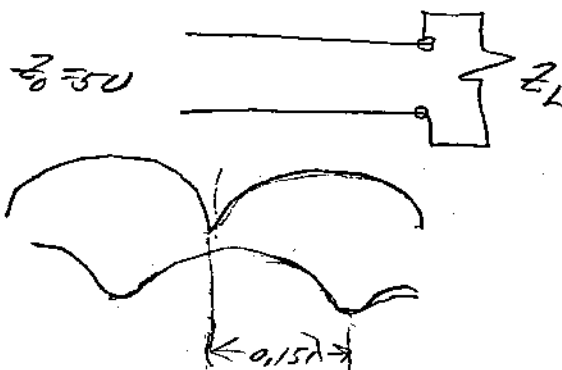
but from example: $G_2 = 0.0366 + G_3 = 0.012$

$$\text{so } P_{ave2} = \frac{8.5}{1 + \frac{0.012}{0.0366}} = \boxed{6.4 \text{ Watts}} \quad \leftarrow$$

$$P_{ave3} = 8.5 - 6.4 = \boxed{2.1 \text{ Watts}} \quad \leftarrow$$

$\nearrow$
losses lines

10-27

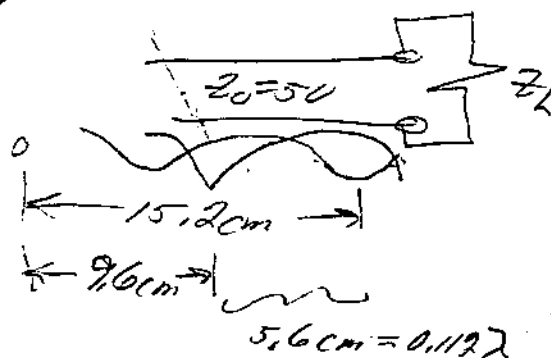


$$SWR = 4.0$$

$$\text{from chart } Z_{L, \text{norm}} = 0.67 + j1.14$$

$$\therefore Z_L = 33.5 + j57$$

10.28



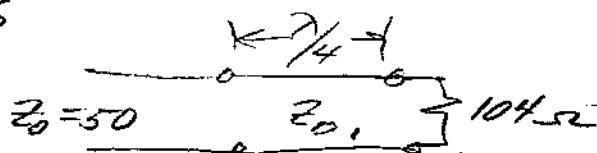
$$f = 600 \text{ MHz} ; SWR = 3.5$$

$$\lambda = \frac{3 \times 10^8}{6 \times 10^8} = 0.5 \text{ m}$$

$$\text{from chart } Z_{L, \text{norm}} = 0.475 + j0.73$$

$$\text{or } Z_L = 23.75 + j36.5$$

10.36



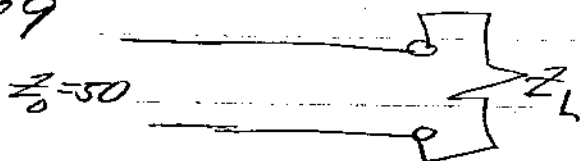
$$f = 500 \text{ MHz} , \epsilon_r = 2.26$$

$$Z_{01} = \sqrt{50 \times 104} = 72.1 \Omega$$

$$\lambda = \frac{3 \times 10^8}{\sqrt{2.26} \times 5 \times 10^8} = \frac{0.6}{1.5} = 0.4 \text{ m}$$

$$\therefore \lambda/4 = 0.1 \text{ m}$$

10.39



$$f = 500 \text{ MHz} ; \lambda = 60 \text{ cm}$$

$$SWR = 3.5$$

(see chart)

place stub $(0.25 - 0.171)\lambda = 0.08\lambda = 4.8 \text{ cm}$ either direction from V_{min}

a) For stub toward the load $Y_{\text{norm, stub}} = -j1.3$; stub length = $0.355 - 0.25 = 0.10$

or stub length = 6.3 cm

SWR from generator to stub = 1

b) SWR from stub to load = 3.5

c) For stub toward the generator $Y_{\text{norm, stub}} = +j1.3$; stub length = $(0.145 + 0.25)\lambda = 23.7 \text{ cm}$

$$Z_{1 @ V_{min}} = 0.25$$

$$Z_n = 0.67 + j1.14$$

Problem 10.27

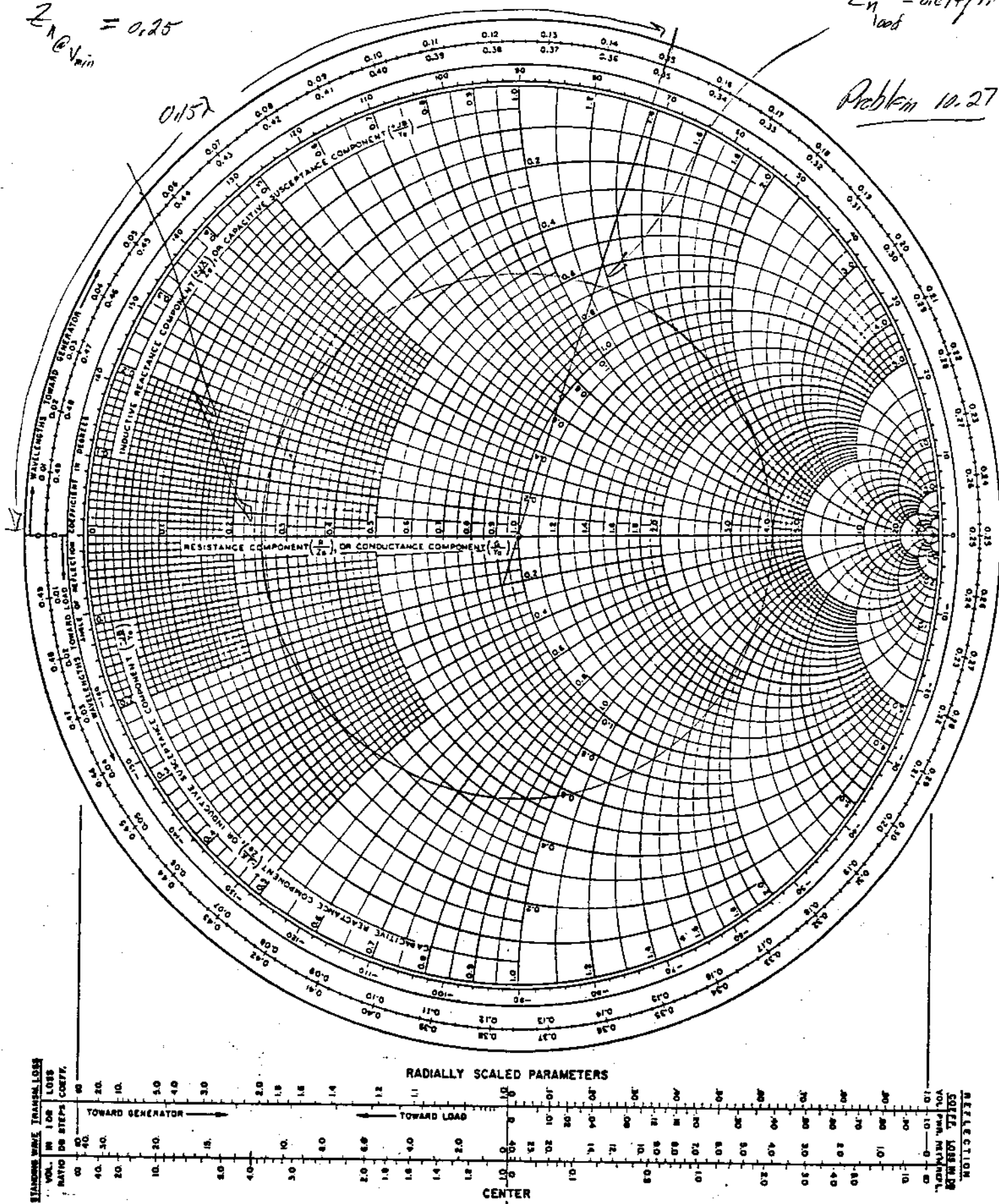
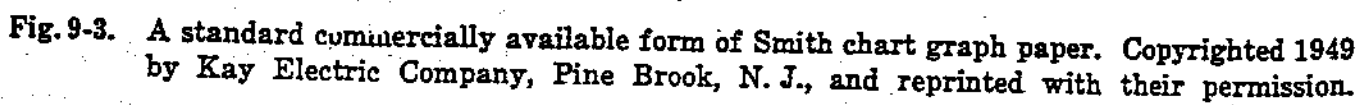
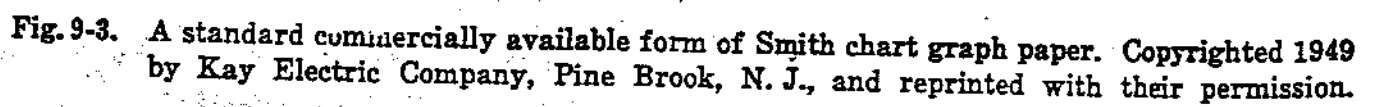
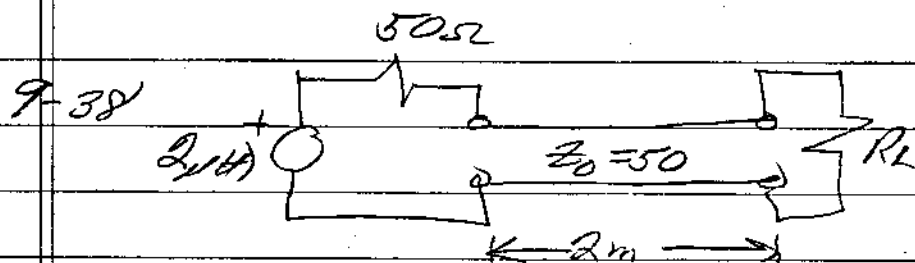


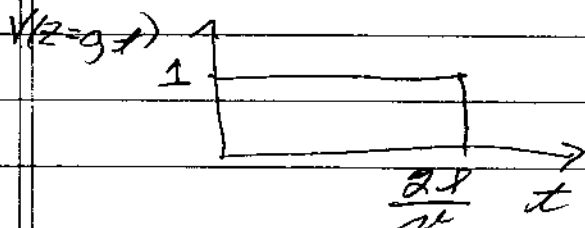
Fig. 9-3. A standard commercially available form of Smith chart graph paper. Copyrighted 1949 by Kay Electric Company, Pine Brook, N. J., and reprinted with their permission.





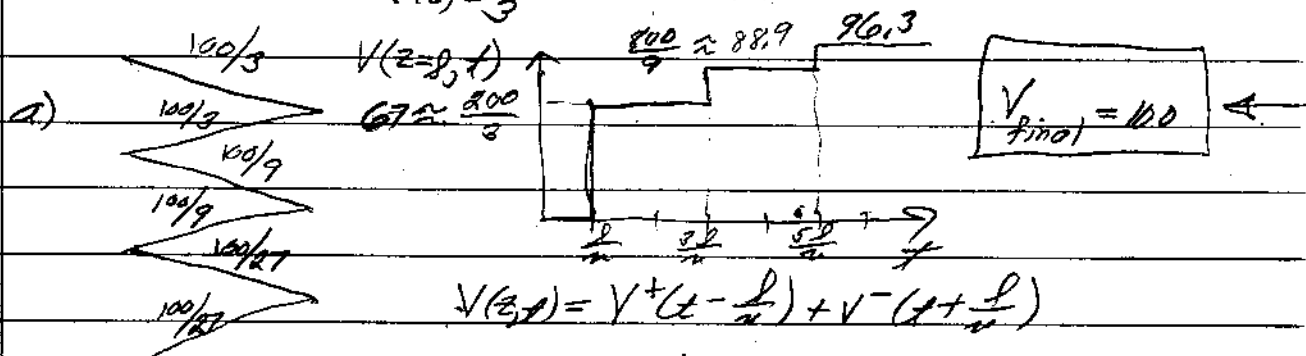
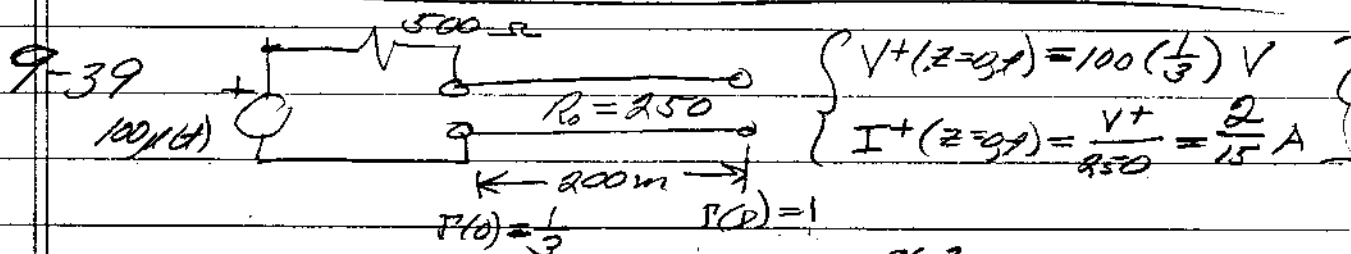
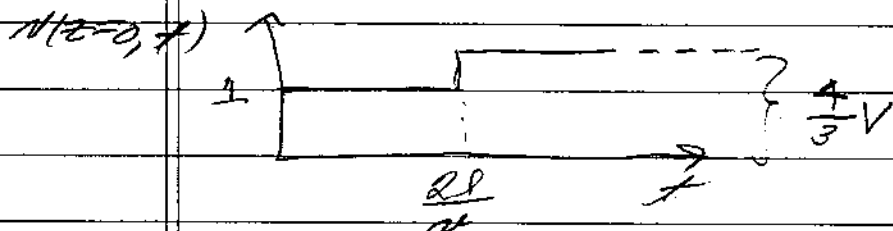


a) $R_L = 0$, $\Gamma_L = -1$

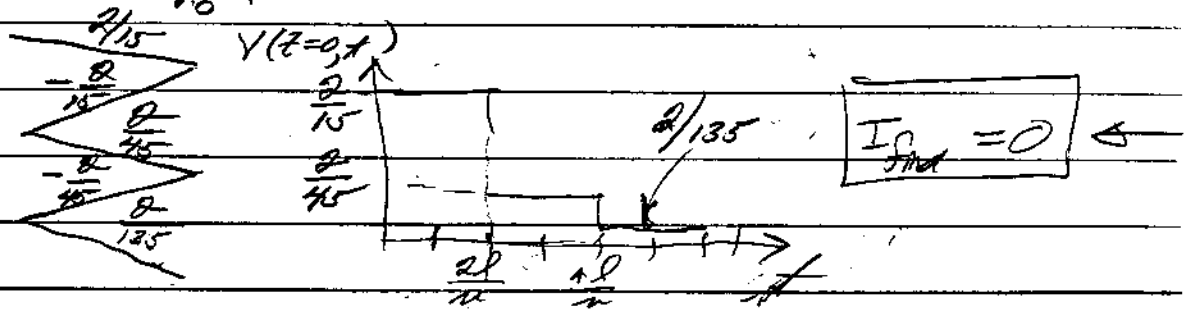


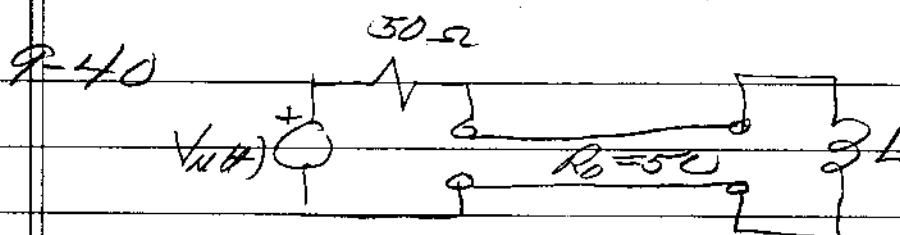
where $\frac{L}{v} = \frac{2}{3 \times 10^8} = \frac{2}{3} \times 10^{-8}$

b) $R_L = 100$, $\Gamma_L = \frac{100-50}{100+50} = \frac{1}{3}$



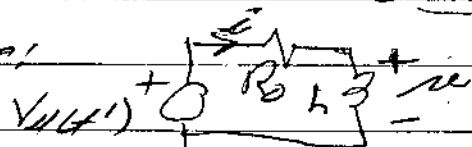
b) $I(z, t) = \frac{1}{R_0} \{ V^+ - V^- \} = \frac{V^+}{R_0} \{ 1 - \Gamma \}$





@ load $V^+(t - \frac{L}{u}) = \frac{V}{2} u(t - \frac{L}{u}) = \frac{V}{2} u(t')$; $t' = t - \frac{L}{u}$

so at load we have:



$$V = iR_0 + L \frac{di}{dt'}$$

$$i_{\text{hom}} = A e^{st'}; s = -\frac{R_0}{L} \quad \text{so } i_h = A e^{-\frac{R_0}{L} t'}$$

$$i_{\text{particular}} = K = \frac{V}{R_0} \quad \text{so } i' = A e^{-\frac{R_0}{L} t'} + \frac{V}{R_0}$$

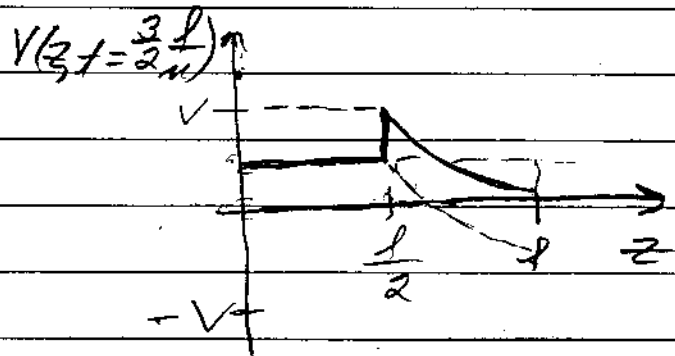
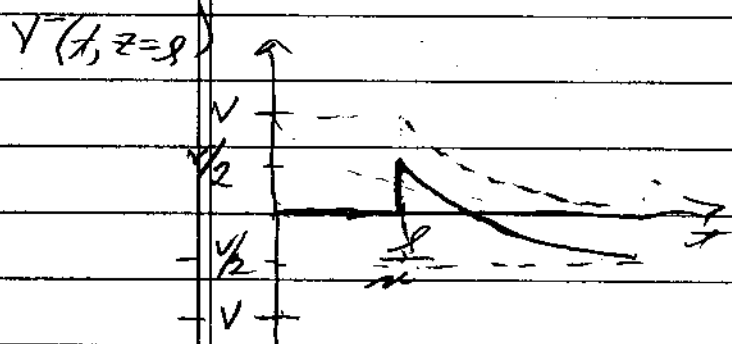
Assuming no initial energy storage [$i(0) = 0$]

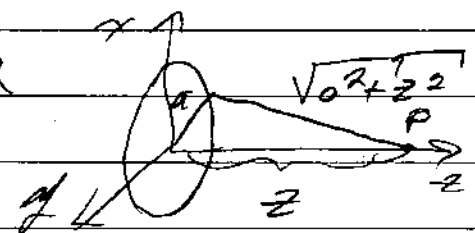
$$i = \frac{V}{R_0} (1 - e^{-\frac{R_0}{L} t'}) = \left[V^+(t - \frac{L}{u}) - V^-(t + \frac{L}{u}) \right] \frac{1}{R_0}$$

giving $V^-(t + \frac{L}{u}) = V^+(t - \frac{L}{u}) - V(1 - e^{-\frac{R_0}{L} (t - \frac{L}{u})})$

$$\text{or } V^-(t + \frac{L}{u}) = \frac{V}{2} u(t - \frac{L}{u}) - V(1 - e^{-\frac{R_0}{L} (t - \frac{L}{u})}) u(t - \frac{L}{u})$$

$$V^-(t + \frac{L}{u}) = \left[-\frac{V}{2} + V e^{-\frac{R_0}{L} (t - \frac{L}{u})} \right] u(t - \frac{L}{u})$$



4-12  a) $\Phi_P = \int_{\phi=0}^{2\pi} \frac{q \rho \, d\phi}{4\pi\epsilon (a^2 + z^2)^{1/2}}$

$\Phi_P = \frac{q \rho \, 2\pi}{4\pi\epsilon (a^2 + z^2)^{1/2}}$

$\vec{E} = -\nabla\Phi = -\frac{\partial\Phi}{\partial z} \hat{z} = \frac{q \rho \, 2\pi}{4\pi\epsilon (a^2 + z^2)^{3/2}} \hat{z}$ on z axis

b) $\Phi(z) = -\int_{-\infty}^z \frac{q \rho \, z' \, dz'}{4\pi\epsilon (a^2 + z'^2)^{3/2}} = -\int_{-\infty}^z \frac{q \rho \, du}{4\pi\epsilon u^{3/2}}$

let $u = a^2 + z^2$
 $du = 2z \, dz$

$\Phi(z) = + \frac{q \rho \, 2}{4\pi\epsilon u^{1/2}} \Big|_{-\infty}^{a^2 + z^2}$

so $\Phi(z) = \frac{q \rho}{2\pi\epsilon (a^2 + z^2)^{1/2}}$

4-16 for coax $C/m = \frac{2\pi\epsilon}{\ln(b/a)} = 96.8 \times 10^{-12}$

$\epsilon = 8.26$

so $\ln(b/a) = \frac{2\pi \times 10^{-9} \times 8.26}{36\pi \times 96.8 \times 10^{-12}} = 1.297$

so $\frac{b}{a} = 3.6585$; so $b = 0.713 \text{ in or } 1.81 \text{ cm}$

4-29 $U_e = \iiint \vec{D} \cdot \vec{E} \, dV = \frac{1}{2} \int_0^\pi \int_0^b \int_0^a \frac{\epsilon_1 V^2}{\rho^2 [\ln(b/a)]^2} \rho \, d\rho \, dz \, d\phi$

[using (4-71)]

$+ \frac{1}{2} \int_{\phi=\pi}^{2\pi} \int_{\rho=a}^b \int_{z=0}^l \frac{\epsilon_2 V^2}{\rho^2 [\ln(b/a)]^2} \rho \, d\rho \, dz \, d\phi$

$U_e = \frac{\pi V^2 l}{2 (\ln(b/a))^2} (\epsilon_1 + \epsilon_2) = \frac{1}{2} C V^2$

so $C = \frac{\pi l}{\ln(b/a)} (\epsilon_1 + \epsilon_2)$

4-61

 $30 \rightarrow 500 \text{ pF}$ in 0 to 260°

$$V = 5000 \text{ V}$$

$$T = \frac{\partial U_e}{\partial \theta} = \frac{\Delta U_e}{\Delta \theta}$$

$$\text{and } U_e = \frac{1}{2} CV^2$$

$$\text{so } \Delta U_e = \frac{1}{2} V^2 (30 - 500) \times 10^{-12} = -V^2 \frac{470}{2} \times 10^{-12}$$

$$T = - \frac{25 \times 10^6 \times 470 \times 10^{-12}}{2 \times 0.60 \times \pi / 180} = 1.294 \times 10^{-3} \text{ N-m}$$