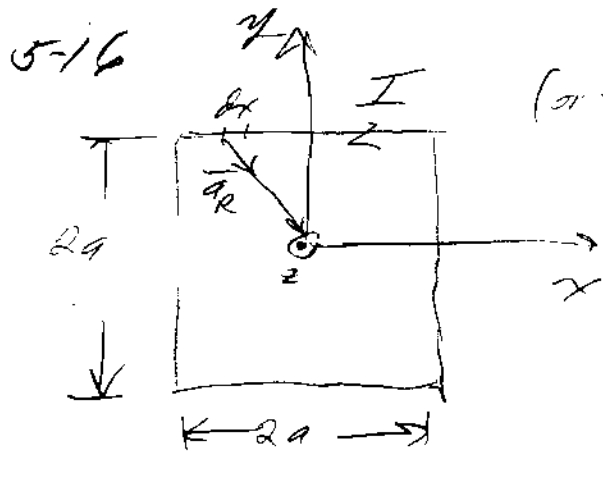


5-16



(or top)

$$\vec{dB} = \frac{\mu I dx \vec{a}_x \times \vec{a}_R}{4\pi (r^2 + a^2)}$$

$$\vec{a}_R = \frac{-x\vec{a}_x - a\vec{a}_y}{\sqrt{x^2 + a^2}}$$

$$\therefore \vec{dB} = \frac{\mu I dx (-a\vec{a}_z)}{4\pi (x^2 + a^2)^{3/2}}$$

$$B_{z, \text{top}} = \int_a^{-a} \frac{-\mu I a dx}{4\pi (x^2 + a^2)^{3/2}} = \frac{-\mu I a}{4\pi} \left\{ \frac{x}{a^2 \sqrt{x^2 + a^2}} \right\}_a^{-a}$$

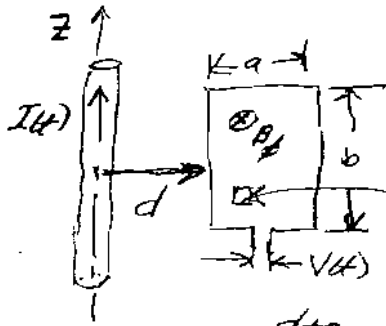
$$B_{z, \text{top}} = \frac{-\mu I}{4\pi} \left\{ \frac{-a}{a \cdot 2a} - \frac{a}{a \sqrt{2}a} \right\} = \frac{2\mu I}{4\pi \sqrt{2}a}$$

$$B_{z, \text{top}} = \frac{\mu I}{2\pi a \sqrt{2}} = \frac{\mu I \sqrt{2}}{4\pi a}$$

By symmetry other 3 sides contribute the same

$$\therefore B_z @ \text{center} = 4B_{z, \text{top}} = \frac{\mu I \sqrt{2}}{\pi a}$$

5.19



$$I(t) = I_m \sin \omega t$$

a) $H(t) = \frac{I_m \sin \omega t}{2\pi r}$ from $\oint \vec{H} \cdot d\vec{l} = I$

~~$$\vec{B} = \mu_0 \vec{H} \hat{\phi}$$~~

b) $\oint \vec{E} \cdot d\vec{l} = V(t) = -\frac{d}{dt} \int_{\rho=d}^{d+a} \int_{z=0}^b \frac{\mu_0 I_m \sin \omega t}{2\pi r} dz dp$

$$V(t) = -\frac{d}{dt} \left\{ \frac{\mu_0 I_m \sin \omega t}{2\pi} b \ln \left(\frac{d+a}{d} \right) \right\} = -\frac{\mu_0 I_m \omega b \cos \omega t}{2\pi} \ln \left(\frac{d+a}{d} \right)$$

(right hand terminal positive) see A page 882

or ... because \vec{F} on positive charges would be in the z direction on both long sides of the loop but of greater magnitude on the left hand side driving a net positive charge to the right hand terminal.

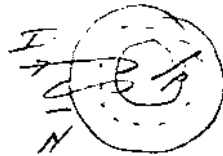
for $I_m = 10A$, $f = 80kHz$, $d = 4 \times 10^{-3}m$, $a = b = 0.1m$

$$V(t) = -\frac{4\pi \times 10^{-7} \times 10 \times 2\pi \times 2 \times 10^4 \times 0.1 \ln \left(1 + \frac{0.1}{4 \times 10^{-3}} \right) \cos(2\pi \times 8 \times 10^4 t)}{2\pi}$$

$$V(t) = -81.88 \times 10^{-3} \cos(4\pi \times 10^4 t) = \boxed{-81.9 \cos(4\pi \times 10^4 t) \text{ mV}}$$

c) 2 times above with opposite polarity

$$5.23 \quad U_m = \frac{1}{2} \int_V \mathbf{B} \cdot \mathbf{H} \, dv$$



$$\oint \mathbf{H} \cdot d\mathbf{l} = NI$$

$$H_{\phi} = \frac{NI}{2\pi r}$$

$$d) \quad \text{so } U_m = \frac{1}{2} \int_0^b \int_0^d \int_0^{2\pi} \frac{\mu_0 N^2 I^2}{4\pi r^2} r \, d\phi \, dr \, dz = \frac{\mu_0 N^2 I^2}{4\pi} \ln \frac{b}{a}$$

$$\text{or } U_m = \frac{\mu_0 N^2 I^2}{4\pi} \ln \frac{b}{a} = \frac{1}{2} L I^2$$

$$\therefore L = \frac{2U_m}{I^2} = \frac{\mu_0 N^2}{2\pi} \ln \frac{b}{a} \quad \text{same as Example 5-17}$$

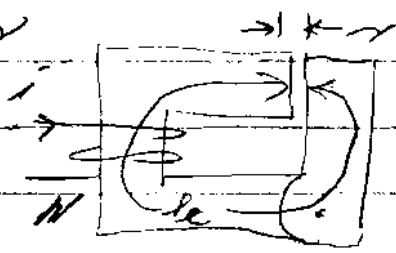
$$b) \quad I = 2, \mu_r = 4 \times 10^3, a = 10^{-2}, b = 3 \times 10^{-2}, d = 2 \times 10^{-2}, N = 150$$

$$U_m = \frac{4 \times 10^3 \times 4\pi \times 10^{-7} \times 2^2 \times 150^2}{4\pi} \ln 3 = 72 \times 10^{-2} \ln 3 = \boxed{79.1 \times 10^{-2} \text{ J}}$$

$$\text{so } L = \frac{2U_m}{I^2} = \frac{2 \times 79.1 \times 10^{-2}}{4} = \boxed{0.395 \text{ H}}$$

c) if $\mu_r = f(I)$ or $f(H)$ which would be true for ferromagnetic material?

5/14/8



$$a) \Phi_m = \frac{NI}{R_{\text{iron}} + R_{\text{gap}}} = \frac{NI}{R_{\text{total}}}$$

$$b) L = \frac{\lambda}{I} = \frac{N\Phi_m}{I} = \frac{N^2}{R_{\text{total}}}$$

$$\therefore U_m = \frac{1}{2} L I^2 = \frac{1}{2} \frac{N^2}{R} I^2$$

$$\text{found that } F_x = \frac{\partial U_m}{\partial x} = \frac{I^2}{2} \frac{\partial L}{\partial x} = \frac{I^2}{2} \frac{\partial}{\partial x} \left(\frac{N^2}{R} \right) = \frac{-N^2 I^2}{2R^2} \frac{\partial R}{\partial x}$$

$$\text{or } F_x = -\frac{1}{2} \frac{\partial}{\partial x} \left(\frac{N^2 I^2}{R} \right)$$

$$\text{so for } R_c = 0.12, A_c = 4 \times 10^{-4}, \mu = 1.5 \times 10^{-3}, I = 1.25 \text{ A}, N = 200$$

$$\text{and } \mu = 1.5 \times 10^{-3}$$

$$R_{\text{total}} = \frac{0.12}{10^5 \times 4\pi \times 10^{-7} \times 4 \times 10^{-4}} + \frac{\mu}{4\pi \times 10^{-7} \times 4 \times 10^{-4}} = 2.387 \times 10^3 + 0.0292 \times 10^9$$

$$\Phi_m = \frac{200 \times 1.25}{R_{\text{total}}} = \frac{2.5 \times 10^2}{2.98 \times 10^6} = 0.839 \times 10^{-4} \text{ webers}$$

$$\therefore F_x = -\frac{1}{2} (0.839 \times 10^{-4})^2 \times 1.99 \times 10^9 = -7 \text{ Newtons}$$

$$B_{\text{ave}} = \frac{\Phi_m}{A} = \frac{0.839 \times 10^{-4}}{4 \times 10^{-4}} = 0.21 \text{ W/m}^2$$

$$H_{\text{ave}} = \frac{B_{\text{ave}}}{\mu} = \frac{0.21}{4\pi \times 10^{-7}} = 1.67 \times 10^5$$

$$H_{\text{ave}} = \frac{0.21}{4\pi \times 10^{-7} \times 10^5} = 1.67$$

$$L = \frac{4 \times 10^4}{2.98 \times 10^6} = 1.31 \times 10^{-2} \approx 13 \text{ mH}$$

$$U_m = \frac{1}{2} L I^2 = \frac{1}{2} \times 1.31 \times 10^{-2} \times 1.25^2 = 1.02 \times 10^{-2} \text{ J}$$

$$\text{if } \mu = 0.75 \text{ an } R_{\text{new}} = \frac{R_{\text{total}}}{2} \text{ so } \Phi_m = 2\Phi_{\text{old}} \text{ and } F_{x,\text{new}} = 4F_{x,\text{old}}$$

5.48 $x=0$ $\frac{dP}{dx}$ is same as before but $R = R_{\text{film}} = 2.387 \times 10^{-3}$

$$\text{so } \frac{dP}{dx} = \frac{2.5 \times 10^{-2}}{2.387 \times 10^{-3}} = 1.047 \times 10^{-1}$$

$$\text{and } F_T = -\frac{1}{2} (1.047 \times 10^{-1})^2 \times 1.99 \times 10^9 = -1.09 \times 10^7 \text{ N} \leftarrow$$

6-5 air | $\epsilon = \epsilon_r \epsilon_0$



$$\frac{E_{m2}^+}{E_{m1}^+} = \frac{2\mu_2}{\mu_1 + \mu_2} = \frac{2 \times \frac{1}{\sqrt{\epsilon_r}}}{1 + \frac{1}{\sqrt{\epsilon_r}}}$$

so $\frac{E_{m2}^+}{E_{m1}^+} = \frac{2}{1 + \sqrt{\epsilon_r}}$

$$\frac{E_{m1}^-}{E_{m1}^+} = \frac{\frac{1}{2} - 1}{\frac{1}{2} + 1} = \frac{\frac{1}{\sqrt{\epsilon_r}} - 1}{\frac{1}{\sqrt{\epsilon_r}} + 1} = \frac{1 - \sqrt{\epsilon_r}}{1 + \sqrt{\epsilon_r}} \leftarrow$$

b) $E_{m1}^+ = 100$, $\epsilon_r = 2.25$, $\sqrt{\epsilon_r} = 1.5$

$$\frac{E_{m2}^+}{E_{m1}^+} = \frac{100 \times 2}{2.5} = 80$$

$$\frac{E_{m1}^-}{E_{m1}^+} = 100 \frac{1 - 1.5}{1 + 1.5} = -20 \leftarrow$$

c) $\epsilon_r = 81$; $\sqrt{81} = 9$

$$\text{so } \frac{E_{m2}^+}{E_{m1}^+} = \frac{100 \times 2}{10} = 20 \frac{\text{V}}{\text{m}} \leftarrow$$

$$\frac{E_{m1}^-}{E_{m1}^+} = 100 \frac{1 - 9}{1 + 9} = -80 \frac{\text{V}}{\text{m}} \leftarrow$$

$$6-6 \quad n_{\text{phase}} = \frac{\omega}{\beta} = \frac{\omega}{2\pi f} = \frac{c}{v_p} \leftarrow$$

$$\text{index of refraction } n = \sqrt{\epsilon_r} \quad \text{so } n = \frac{c}{v_p} \leftarrow$$

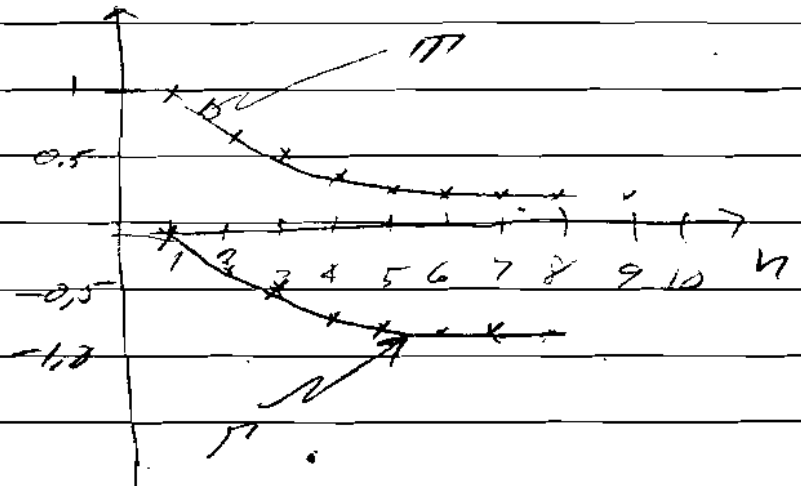
$$n_{\text{polyethylene}} = \sqrt{2.25} = 1.5 \leftarrow$$

$$n_{\text{water}} = \sqrt{81} = 9 \leftarrow$$

$$\Gamma = \frac{1-n}{1+n} \quad ; \quad T = \frac{2}{1+n}$$

$$|T - \Gamma| = \frac{2 - 1 + n}{1 + n} = 1 \leftarrow \left\{ \begin{array}{l} E \text{ field is continuous?} \\ \text{of boundary} \end{array} \right\}$$

n	T	Γ
1	1	0
2	0.67	-0.33
3	0.5	-0.5
4	0.4	-0.6
5	0.33	-0.67
6	0.29	-0.71
7	0.25	-0.75
8	0.22	-0.77
9	0.2	-0.8
10	0.18	-0.82



$$6-17 \hat{\eta}_1 \quad \hat{\eta}_2 \quad \hat{\eta}_3 \quad \delta_2 \rightarrow j\beta_2$$

$$\leftarrow \gamma/4 \rightarrow \quad e^{j\beta_2 d} \rightarrow e^{j \frac{2\pi}{\lambda} \cdot \frac{\lambda}{4}} = j$$

$$\text{Then } \hat{z}_1(0) = \eta_2 \frac{j(\hat{\eta}_3 + \eta_2) - j(\hat{\eta}_3 - \eta_2)}{j(\hat{\eta}_3 + \eta_2) + j(\hat{\eta}_3 - \eta_2)} = \frac{2j\eta_2 \eta_2}{2j\hat{\eta}_3} = \frac{\eta_2^2}{\hat{\eta}_3}$$

6-18 $\epsilon_{r3} = 2.56$ in above problem we need $\hat{z}_1(0) = \eta_1$

$$\therefore \eta_2 = \sqrt{\eta_1 \eta_3} \quad \text{or for all } \mu = 1$$

$$\text{we want } \frac{\eta_0}{\epsilon_r} = \sqrt{\frac{\eta_1 \eta_3}{\epsilon_r \epsilon_s}} \quad ; \quad \frac{1}{\epsilon_r} = \frac{1}{\sqrt{\epsilon_r \epsilon_s}}$$

$$\boxed{\epsilon_r = \sqrt{1 \times 2.56} = 1.6} \quad \leftarrow$$

reciprocal because got same value for η_2 if $\eta_1 + \eta_3$ are interchanged!

$$6-20 \hat{\eta}_1 \quad \eta_2 \quad \hat{\eta}_3 \quad e^{j\beta_2 d} \rightarrow e^{j\pi} = -1$$

$$\leftarrow \gamma/2 \rightarrow$$

$$\text{so } \hat{z}_1(0) = \eta_2 \frac{-(\hat{\eta}_3 + \eta_2) - (\hat{\eta}_3 - \eta_2)}{-(\hat{\eta}_3 + \eta_2) + (\hat{\eta}_3 - \eta_2)} = \eta_2 \frac{-2\hat{\eta}_3}{+2\eta_2} = \frac{\eta_2}{\hat{\eta}_3}$$

same result whenever $e^{j\frac{2\pi}{\lambda} \cdot d} = -1$

$$\text{or } d = n \frac{\lambda}{2} \quad ; \quad n = 1, 2, 3, 4, \dots$$

n odd

6-35 ①	②	$\theta_i = \tan^{-1} \sqrt{\frac{\epsilon_2}{\epsilon_1}}$
μ_0, ϵ_0	$\mu_0, 3\epsilon_0$	Brewster

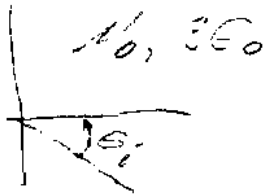
θ_{i0} from ① \rightarrow ② $\theta_{i0} = 60^\circ$
 ② \rightarrow ① $\theta_{i0} = 30^\circ$

must be // polarized \leftarrow

$$\frac{\sqrt{\epsilon_2}}{\sqrt{\epsilon_1}} \leftrightarrow \tan^{-1} \sqrt{\frac{\epsilon_2}{\epsilon_1}} = 90^\circ - \tan^{-1} \sqrt{\frac{\epsilon_2}{\epsilon_1}}$$

} so θ_i Brewster angles from opposite
 directions are always complements.

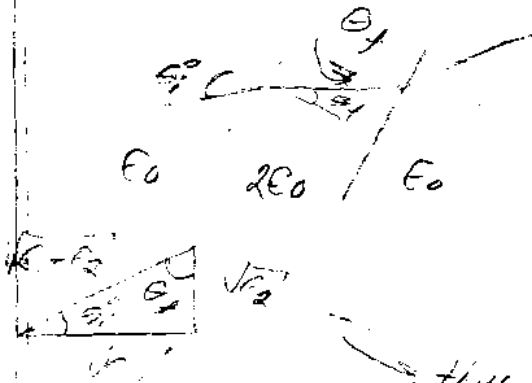
6.36 16, 50



$$\theta_{critical} = \sin^{-1} \sqrt{\frac{1}{5}} = \underline{35.26^\circ}$$

polarization not important

6.37 a)



$$\theta_i^\circ = \tan^{-1} \sqrt{\frac{\epsilon_2}{\epsilon_1}}$$

$$\frac{\sin \theta_t}{\sin \theta_i} = \sqrt{\frac{\epsilon_1}{\epsilon_2}}$$

$$\sin \theta_t = \frac{\sqrt{\epsilon_2}}{\sqrt{\epsilon_1 + \epsilon_2}} \cdot \sqrt{\frac{\epsilon_1}{\epsilon_2}} = \frac{\sqrt{\epsilon_1}}{\sqrt{\epsilon_1 + \epsilon_2}}$$

thus we see that $\theta_t = 90^\circ - \theta_i^\circ$

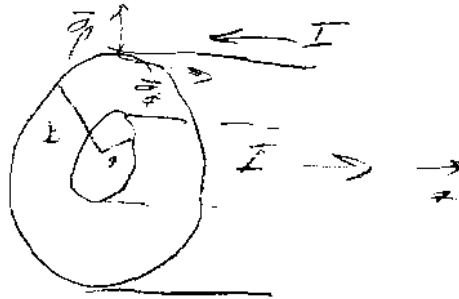
the stated in problem 6.35 that the Brewster angle for waves incident on the interface from either side are complementary angles. The angle of incidence at the second surface is θ_t so there will be no reflection at this surface because $\theta_t = 90^\circ - \theta_i^\circ$ as shown above

$$b) \Gamma_{||} = 0 \quad ; \quad \theta_i^\circ = \tan^{-1} \sqrt{2} = 54.73^\circ$$

$$\Gamma_{\perp} = \frac{\cos \theta_i - \sqrt{\frac{\epsilon_2}{\epsilon_1}} \cos \theta_t}{\cos \theta_i + \sqrt{\frac{\epsilon_2}{\epsilon_1}} \cos \theta_t} \quad ; \quad \theta_t = \sin^{-1} \left(\sqrt{\frac{\epsilon_1}{\epsilon_2}} \sin \theta_i \right) = 35.26^\circ$$

$$\Gamma_{\perp} = \frac{0.5774 - 1.155}{0.5774 + 1.155} = \frac{-0.577}{1.732} = \boxed{-0.333} \leftarrow$$

7.2



$$E_z = \frac{-J_z}{\sigma}; J_z = \frac{I}{\pi a^2 - \pi b^2}$$

$$H_\phi = \frac{I}{2\pi r}$$

$$\vec{E} \times \vec{H} = \frac{J_z I}{\sigma 2\pi b} \frac{1}{r} = \frac{I^2}{2\pi^2 \sigma (a^2 - b^2)} \frac{1}{r}$$

$P_{\text{into wire volume}} = \int_{z=0}^L \int_{\phi=0}^{2\pi} \frac{I^2}{2\pi^2 \sigma (a^2 - b^2)} r b dr d\phi dz$

$$P = \frac{2\pi L I^2}{2\pi^2 \sigma (a^2 - b^2)} = I^2 \frac{L}{\sigma \pi (a^2 - b^2)} = I^2 R$$

$$7-13 \quad \hat{E}_x = \hat{E}_m^+ e^{-\alpha z} e^{j\beta z} [1 + \Gamma] \quad \hat{H}_y = \frac{\hat{E}_m^+}{\eta} e^{-\alpha z} e^{j\beta z} [1 - \Gamma]$$

$$P_{ave} = \frac{1}{2} \text{Re} \{ \hat{E} \times \hat{H}^* \} = \frac{1}{2} \text{Re} \left\{ \frac{|\hat{E}_m^+|^2}{\eta} (1 + \Gamma)(1 - \Gamma^*) \right\} \hat{a}_z$$

$$\bar{P}_{ave} = \frac{|\hat{E}_m^+|^2}{2\eta} \text{Re} \{ (1 + \Gamma)(1 - \Gamma^*) - \Gamma + \Gamma^* - |\Gamma|^2 \} \hat{a}_z$$

$$\bar{P}_{ave} = \frac{|\hat{E}_m^+|^2}{2\eta} [1 - |\Gamma|^2] \hat{a}_z = \bar{P}_{ave}^+ - \bar{P}_{ave}^- \quad \leftarrow$$

$$\therefore \frac{|\bar{P}_{ave}^-|}{|\bar{P}_{ave}^+|} = |\Gamma|^2 \quad \leftarrow$$

$$7-17 \quad P_{ave} = \frac{1}{2} \text{Re} \left\{ \frac{|\hat{E}_m^+|^2 e^{-2\alpha z}}{\eta} e^{j\beta z} [1 + \Gamma] [1 - \Gamma^*] \right\}$$

$$P_{ave} = \frac{|\hat{E}_m^+|^2 e^{-2\alpha z}}{2\eta} \text{Re} \left\{ [\cos \theta + j \sin \theta] [1 + \Gamma + \Gamma^* - \Gamma \Gamma^* - |\Gamma|^2] \right\}$$

$$P_{ave} = \frac{|\hat{E}_m^+|^2 e^{-2\alpha z}}{2\eta} \left\{ \cos \theta [1 - |\Gamma|^2] - \sin \theta [2\Gamma_i] \right\} \quad \leftarrow (1)$$

for $\Gamma = 0$ this becomes $\boxed{P_{ave} = \frac{|\hat{E}_m^+|^2 e^{-2\alpha z}}{2\eta} \cos \theta}$

b) lossless case $\eta \rightarrow \eta$, $\alpha \rightarrow 0$ and $x \rightarrow 0$

giving: $\boxed{P_{ave} = \frac{|\hat{E}_m^+|^2}{2\eta} [1 - |\Gamma|^2]}$ as in 7-13

$$P_{ave} = \frac{1}{2} \text{Re} \left\{ \frac{\hat{E}_m^+ e^{-\alpha z} e^{j\beta z} + j\theta}{\eta} \frac{\hat{E}_m^+ e^{-\alpha z} e^{j\beta z}}{e^{j\theta}} \right\} = \frac{|\hat{E}_m^+|^2 e^{-2\alpha z} \cos \theta}{2\eta}$$

positive wave

$$P_{ave} = \frac{1}{2} \text{Re} \left\{ \frac{\hat{E}_m^+ e^{-\alpha z} e^{j\beta z} + j\theta}{\eta} \frac{\hat{E}_m^+ e^{-\alpha z} e^{j\beta z} (-\Gamma^*)}{e^{j\theta}} \right\} = \frac{|\hat{E}_m^+|^2 e^{-2\alpha z} \sin \theta}{2\eta}$$

negative wave

summing these two terms would miss the $-\sin \theta [2\Gamma_i]$ term in the above expression!

$$7-21 \quad P_{\text{out}} \text{ of sun} = 1340 \text{ W/m}^2$$

@ earth

assuming single frequency wave we have:

$$P_{\text{ave}} = \frac{|\hat{E}_m|^2}{2\eta}; \quad \text{or } |\hat{E}_m| = \sqrt{2 \times 377 \times 1340} = 1.005 \times 10^3 \text{ V/m}$$

$$|\hat{H}_m| = \frac{|\hat{E}_m|}{\eta} = 2.66 \text{ A/m}$$

$$P_{\text{total}} \text{ from sun} = 4\pi (1.48 \times 10^{11})^2 \cdot 1340 = 36.88 \times 10^{25} \text{ Watts}$$

$$11-11 \quad \Delta z = 0.01 \lambda; \quad \hat{I} = 5 \text{ A}; \quad f = 300 \text{ MHz}$$

$$a) \quad \lambda = \frac{3 \times 10^8}{3 \times 10^8} = 1 \text{ m} \quad \therefore \boxed{\Delta z = 0.01 \text{ m}} \quad \leftarrow$$

(for zone if $\beta r \gg 1$ from (11-30)
 so $\beta r = 30$ is reasonably in the far zone

$$\text{this is } [r = \frac{30}{\beta} = \frac{30}{2\pi} \lambda = 3.18 \text{ m}] \quad \leftarrow$$

$$b) \quad \hat{E}_\theta = \eta \hat{H}_\phi = \frac{j\omega\mu I \Delta z e^{-j\beta r}}{4\pi r} \sin\theta \quad \leftarrow$$

$\sin\theta = 1 \quad \theta = 90^\circ$

$$c) \quad \bar{P} = \frac{1}{2} \rho_0 \int \hat{E}_\theta \hat{H}_\phi^* \times \hat{a}_r \cdot \hat{a}_r \, d\Omega = \frac{1}{2} \cdot \frac{\omega^2 \mu^2 I^2 \Delta z^2}{4\pi r^2} \int \sin^2\theta \, d\Omega$$

$$\bar{P} = \frac{\eta I^2 \Delta z^2 \int \sin^2\theta \, d\Omega}{8\pi r^2} = \frac{\eta I^2 \Delta z^2}{8\pi r^2} \int_0^\pi \sin^2\theta \, 2\pi \sin\theta \, d\theta$$

$$\boxed{\bar{P} = \frac{\eta I^2}{8\pi r^2} \left(\frac{\Delta z}{\lambda}\right)^2} = \frac{377 \times 25 \times 10^{-4}}{8 \times 3.18^2} = \boxed{0.0117 \text{ Watts/m}^2}$$

$$11-14 \quad P_{\text{rad}} = \int_0^{2\pi} \int_0^\pi \frac{\eta I^2}{8\pi r^2} \left(\frac{\Delta z}{\lambda}\right)^2 \sin^3\theta \, d\theta \, d\phi$$

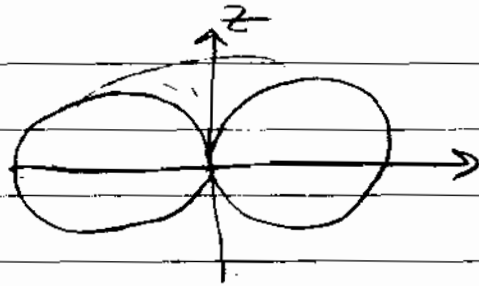
$$\left[P_{\text{rad}} = \frac{\eta I^2}{8\pi r^2} \left(\frac{\Delta z}{\lambda}\right)^2 \int_0^{2\pi} \int_0^\pi \sin^3\theta \, d\theta \, d\phi = \frac{\eta I^2}{3} \left(\frac{\Delta z}{\lambda}\right)^2 \right]$$

$$a) \quad \text{so } P_{\text{rad}} = \frac{\eta \times 377 \times 25 \times 10^{-4}}{3} = \boxed{0.99 \text{ Watts}} \quad \leftarrow$$

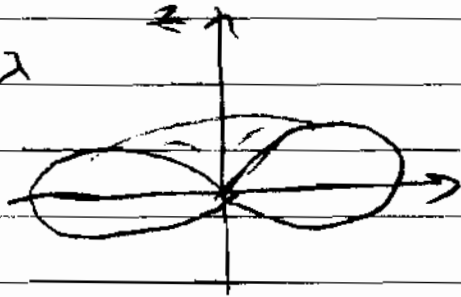
$$b) \quad \text{if } \Delta z \rightarrow 0.02 \text{ m} \quad P_{\text{rad}} = 4 \times 0.99 = 3.95 \text{ Watts} \quad \leftarrow$$

$$\text{if } \Delta z = 0.005 \text{ m} \quad P_{\text{rad}} = \frac{0.99}{4} = 0.25 \text{ Watts} \quad \leftarrow$$

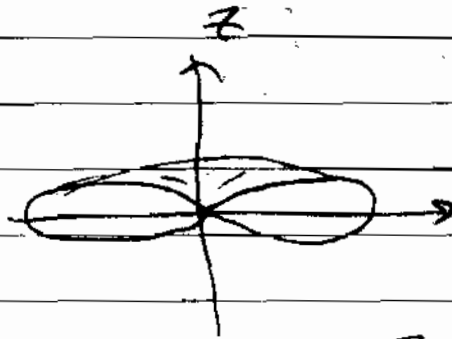
11-19 a) $L = \frac{3}{2}\lambda$



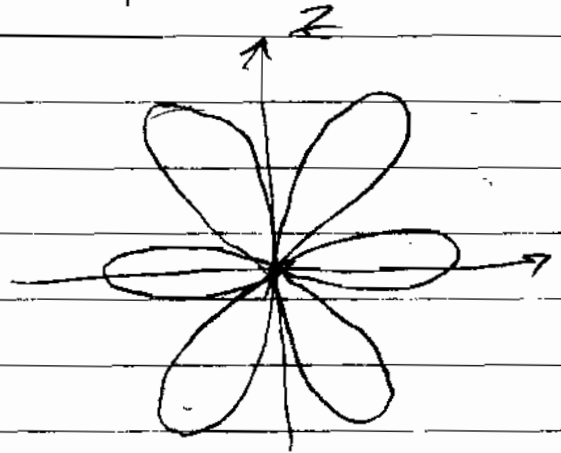
b) $L = \frac{5}{4}\lambda$



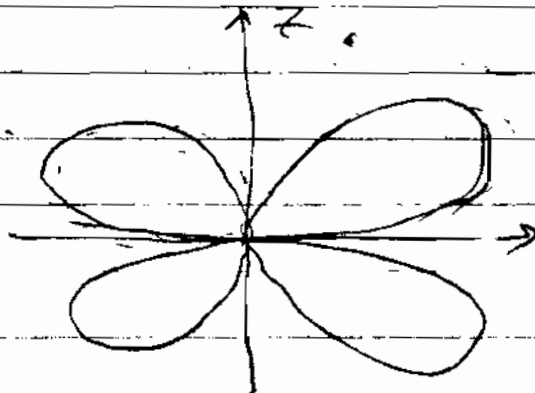
c) $L = \lambda$



11-20 a) $L = 1.5\lambda$



b) $L = 2\lambda$



9.1 \vec{d}_e dipole ; $I = 10A$; $d_e = \frac{\lambda}{50}$; $r = 10^3 m$

$$P_{max} = \frac{1}{2} \epsilon_0 \left\{ \frac{\mu I^2 d_e^2 \omega^4}{16\pi^2 r^2} \right\} = \frac{2\pi I^2 d_e^2 \omega^4}{2 \times 16\pi^2 r^2}$$

but $\left[\omega = \frac{2\pi f \times \sqrt{\mu \epsilon}}{v} = \frac{2\pi f}{\lambda} \right]$

$$\therefore P_{max} = \frac{I^2 d_e^2 \times 2\pi \times \left(\frac{2\pi f}{\lambda}\right)^4}{\lambda^2 \times 16 \times \pi^2 r^2} = \frac{10^2 \times 120\pi^2}{(50)^2 \times 8 \times 10^6} = 1.89 \times 10^{-6} \frac{W}{m^2}$$

9.2 $L = 1m$; $f = 10^6$ $\therefore \lambda = \frac{3 \times 10^8}{10^6} = 300m$ (short dipole)

$I = 12A$, $r = 5 \times 10^3$

$$P(\theta = 30^\circ) = \frac{I^2 \pi}{8 \times 2} \left(\frac{d_e}{\lambda}\right)^2 \sin^2 30^\circ = \frac{12^2 \times 377}{8 \times 2 \times 5 \times 10^6} \left(\frac{1}{300}\right)^2 \sin^2 30^\circ = 7.57 \times 10^{-10} \frac{W}{m^2}$$

9.5 $L = 2m$, $f = 10^6$ $\therefore \lambda = \frac{3 \times 10^8}{10^6} = 300m$ (short dipole)

Cu antenna $\therefore \sigma = 5.8 \times 10^7$ wire radius = $1mm$

a) $P_{rad} = \frac{2\pi I^2 \left(\frac{d_e}{\lambda}\right)^2}{3} = \frac{2\pi \times 32^2}{3} \left(\frac{2}{300}\right)^2 = \boxed{0.0351 \text{ a}}$

$$R_{loss} = \frac{L}{2a} \sqrt{\frac{f \mu}{\pi \sigma}} = \frac{2}{2 \times 10^{-3}} \sqrt{\frac{10^6 \times 4\pi \times 10^{-7}}{\pi \times 5.8 \times 10^7}} = \boxed{0.083 \text{ a}}$$

so $\xi = \frac{0.0351}{0.0351 + 0.083} = 0.297$ or $\boxed{29.7\%}$

b) $G = \xi \times 0 = 0.297 \times 1.5 = 0.446$ or $\boxed{-3.5/dB}$

c) $20 = \frac{I^2 \pi \pi \left(\frac{d_e}{\lambda}\right)^2}{3}$ or $I = \sqrt{\frac{60}{\pi \pi}} \left(\frac{\lambda}{d_e}\right)$

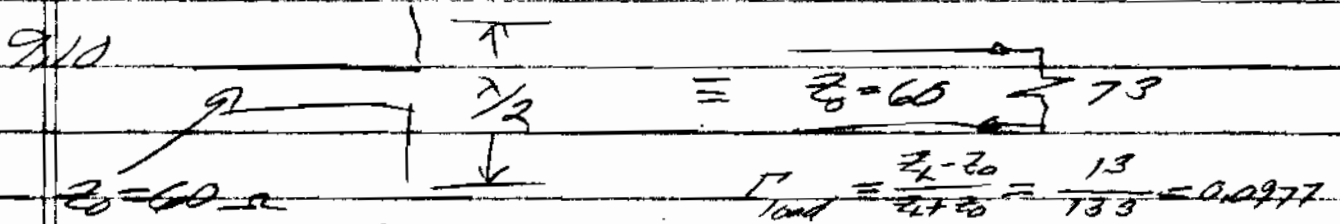
or $I = \sqrt{\frac{60}{120\pi}} \left(\frac{\lambda}{d_e}\right) = \frac{1}{\sqrt{2\pi}} (150) = \boxed{33.76A}$

$P_{transmitter} = \frac{P_{rad}}{\xi} = \frac{20}{0.297} = \boxed{67.34 \text{ Watts}}$

9.8 $\xi = 90\%$; $D_{dB} = 6.7 dB$; $G = ?$

$D_{dB} = 10 \log_{10} D$; $D = 10^{\frac{6.7}{10}} = 4.677$; $G = 50 = 4.2$

or $G_{dB} = 6.24 dB$



$SWR = \frac{|V_{max}|}{|V_{min}|} = \frac{1 + |\Gamma|}{1 - |\Gamma|} = \frac{1 + 0.0977}{1 - 0.0977} = 1.217$

9.15 36 GHz ; 1m dishes ; $P_T = 10^{-9} W$; $r = 4 \times 10^4$

$\lambda = \frac{3 \times 10^8}{3.6 \times 10^{10}} = 0.1 m$

$P_r = 10^{-9} (r \lambda)^2 \left(\frac{1}{A_r A_t} \right) = \frac{10^{-9} \times 16 \times 10^8 \times 10^{-2}}{\pi^2} = 25.97 \times 10^{-3} W$

9.16 $\lambda/2$ dipole ; $P_t = 10^3$; $f = 50 \text{ MHz}$; $G_r = 13 \text{ dB}$
 $R = 3 \times 10^4$; $D_r = 19.95$; $\lambda = \frac{3 \times 10^8}{5 \times 10^7} = 6 \text{ m}$

9.16 $P_r = P_t D_r D_r \left(\frac{\lambda}{4\pi R} \right)^2 = 10^3 \times 19.95 \times 19.95 \left(\frac{6}{4\pi \times 3 \times 10^4} \right)^2 = 8.28 \times 10^{-6} \text{ W}$

9.21 946 Hz ; antenna $1 \text{ m} \times 0.1 \text{ m}$; $\lambda = \frac{3 \times 10^8}{94 \times 10^3} = 3.19 \times 10^{-3} \text{ m}$

a) $BW_{\text{elevation}} \approx \frac{3.19 \times 10^{-3}}{0.1} = 3.19 \times 10^{-2} \text{ radians} = 1.8^\circ$

$BW_{\text{azimuth}} \approx 3.19 \times 10^{-2} \text{ radians} = 0.18^\circ$

b) $d = 300 \times 3.19 \times 10^{-3} = 0.957 \text{ m}$

9.23 $\phi = 0$ $\phi = \delta$

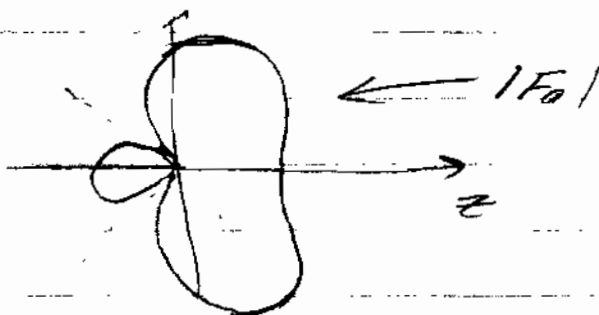
a) $a_0 = a_1 = 1$; $\delta = \frac{\pi}{4}$; $d = \frac{\lambda}{2}$

uniform array : $|F_0| = \frac{\sin(\frac{N\psi}{2})}{\sin \frac{\psi}{2}}$ where $\psi = \frac{2\pi}{\lambda} d \cos \theta - \delta$

so $\psi = \pi \cos \theta - \frac{\pi}{4}$ and $|F_0| = \frac{\sin \psi}{\sin \frac{\psi}{2}}$

maximum of array pattern @ $\psi = 0$ so $\theta_{\text{max}} = \cos^{-1} \frac{1}{4} = 75.52^\circ$

1st zero when $\psi = -\pi = \pi \cos \theta - \frac{\pi}{4}$ or $\cos \theta = -\frac{3}{4}$; $\theta_{\text{zero}} = 138.6^\circ$



9.23 b) $a_0=1, a_1=2, \delta=0, d=\lambda$

$$F_0 = 1 + 2e^{j\psi} ; \psi = \frac{2\pi}{\lambda} d \cos\theta - \phi = 2\pi \cos\theta$$

$$\therefore F_0 = 1 + 2e^{j2\pi \cos\theta} = 1 + 2\cos(2\pi \cos\theta) + j2\sin(2\pi \cos\theta)$$

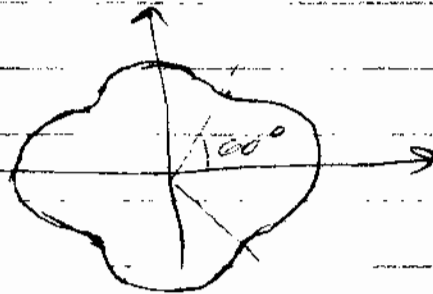
$$\text{so } |F_0| = [1 + 2\cos(2\pi \cos\theta)]^2 + 4\sin^2(2\pi \cos\theta)$$

$$|F_0| = 1 + 4\cos(2\pi \cos\theta) + 4 = 5 + 4\cos(2\pi \cos\theta)$$

computer plot gives:

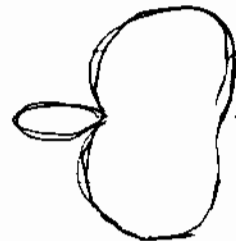
@ $\theta = 0 + 90^\circ$ $|F_0| = 9$

@ $\theta = 60^\circ$ $|F_0| = 1$



9-24 from 9.23a)

$$F_0 =$$

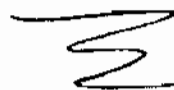
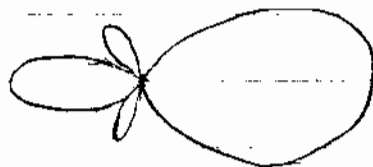


$$F_{element} =$$



$$\text{total pattern} = F_{element} \times F_0$$

so total pattern is



Broadcast Antenna Array $[F_a = (z - z_1)(z - z_2)]$
 where $z = e^{j\theta} = e^{j\beta d \cos \theta}$

$\theta = 0$ (fed in phase) will provide maximum @ $\theta = 90^\circ$
 next zeroes when $\theta = 26^\circ$ and 154°

$$z_1 = \frac{2\pi d}{\lambda} \cos 26^\circ = \frac{\pi}{2} \cos 26^\circ = 0.449\pi$$

$$z_2 = \frac{\pi}{2} \cos 154^\circ = -0.449\pi$$

$$\text{so } F_a = (z - e^{j0.449\pi})(z - e^{-j0.449\pi}) = z^2 - z(e^{j0.449\pi} + e^{-j0.449\pi}) + 1$$

$$\text{or } F_a = z^2 - 0.39z + 1 \quad z = e^{j\frac{\pi}{8} \cos \theta}$$

(see attached plot)

9.18 a) $P_t = 10\text{W}$, $f = 6\text{GHz}$, $G_t = 20\text{dB}$, $G_r = 23\text{dB}$, $N = 2 \times 10^8$

$$D(\theta, \phi) = \frac{P_{\text{W/m}^2} 4\pi R^2}{P_t}; \quad \lambda = \frac{3 \times 10^8}{6 \times 10^9} = 0.05\text{m}$$

$$\text{a) } P_{\text{@ receiver}} = \frac{G_t P_t}{4\pi R^2} = \frac{10^9 \times 10}{4\pi \times 4 \times 10^8} = 0.0199 \times 10^{-5} = 1.99 \times 10^{-7} \text{ W/m}^2$$

$$\text{b) } P_{\text{RECEIVER}} = P_t G_t G_r \left(\frac{\lambda}{4\pi R}\right)^2 = 1.99 \times 10^{-7} \times 25 \times 10^{-4} \times 199.53 \left(\frac{1}{4\pi}\right) = 7.999 \times 10^{-9} \text{ W}$$

$$\text{c) } N = kTB = 1.38 \times 10^{-23} \times 10^3 \times 10^7 = 1.38 \times 10^{-13} \text{ W} \quad \therefore \frac{P}{N} = 5.72 \times 10^4 \text{ or } 47.6 \text{ dB}$$

9.20 Beamwidth = 1.5° @ 20GHz $1.5^\circ \times \frac{\pi}{180} = \frac{1.5 \times 10^{-2}}{d/\lambda}$; $d/\lambda = 0.573$
 $\lambda = \frac{3 \times 10^8}{20 \times 10^9} = 1.5 \times 10^{-2} \text{ m}$; $D = \frac{4\pi}{\lambda^2} A_{\text{eff}} = \frac{4\pi (0.573)^2}{2.25 \times 10^{-4} \times 4} = 1.44 \times 10^4$

$$\text{a) } \therefore D = 1.44 \times 10^4 \text{ or } 41.6 \text{ dB}$$

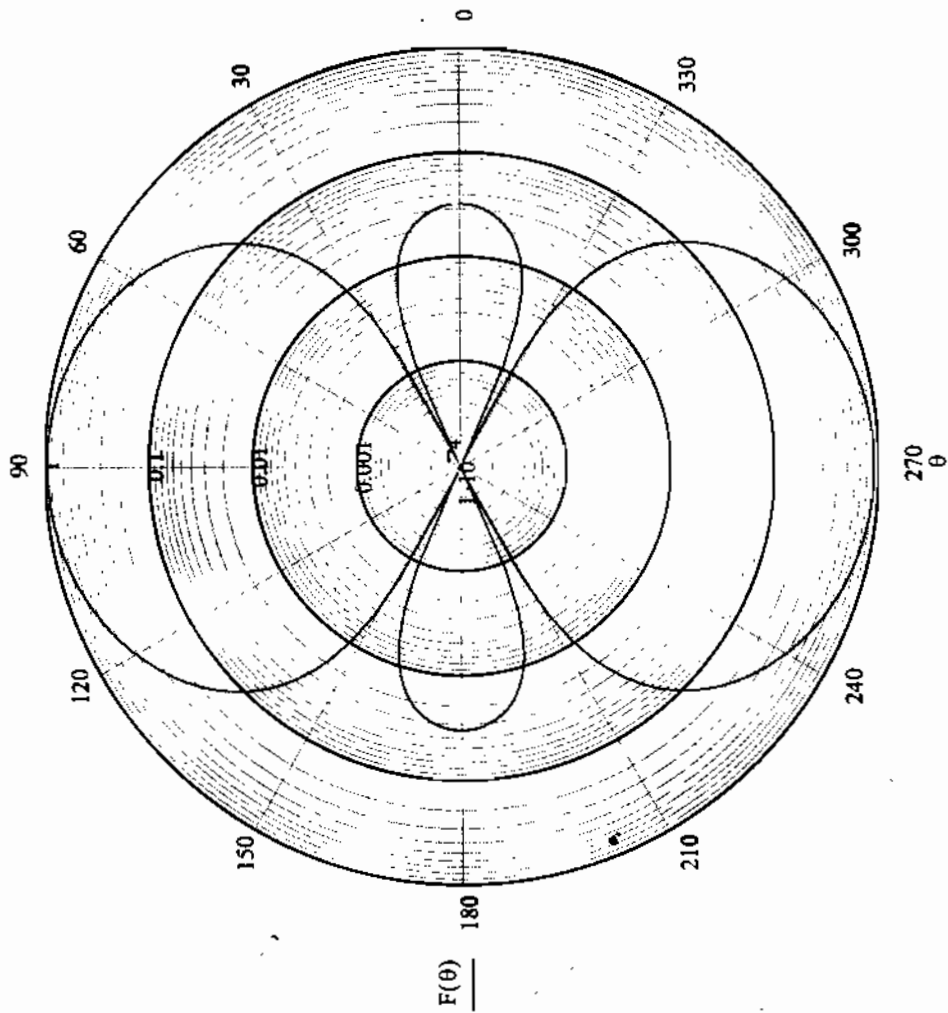
b) For twice the area D will be multiplied by 2 and beamwidth $\div \sqrt{2}$

c) for twice the frequency $\text{beamwidth} \div 2$ and D multiplied by 4

Broadcast Array Special Problem

$$j := \sqrt{-1}; \quad \theta := 0, \frac{\pi}{100} \dots 2 \cdot \pi \quad z(\theta) := e^{j \frac{\pi}{2} \cos(\theta)} \quad z_1 := e^{j \frac{\pi}{2} \cos\left(26 \frac{\pi}{180}\right)} \quad z_2 := e^{j \frac{\pi}{2} \cos\left(154 \frac{\pi}{180}\right)}$$

$$F(\theta) := \left[\left[\frac{1}{\sqrt{3}} (z(\theta) - z_1) (z(\theta) - z_2) \right] \right]^2$$



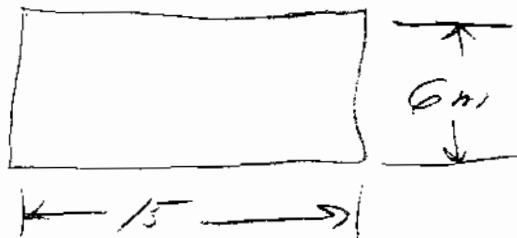
$$8-23 \quad f_c = \frac{1}{2\sqrt{\epsilon} a} \quad \text{for } TE_{10} \text{ mode}$$

$$a) \quad 5 \text{ GHz} \quad a_{\min} = \frac{1}{2\sqrt{\epsilon} f} = \frac{3 \times 10^8}{10 \times 10^9} = \boxed{3 \times 10^{-2} \text{ m}} \leftarrow$$

$$b) \quad 5 \text{ MHz} \quad a_{\min} = \frac{3 \times 10^8}{10 \times 10^6} = \boxed{30 \text{ m}} \leftarrow$$

$$c) \quad 5 \text{ kHz} \quad a_{\min} = \frac{3 \times 10^8}{10^4} = \boxed{3 \times 10^4 \text{ m}} \leftarrow$$

7-27

TE₁₀ mode

$$f_c = \frac{3 \times 10^8}{2 \times 15} = 10 \text{ MHz}$$

→ Vertical polarization

AM will not propagate

535-1605 kHz

FM will propagate

88-108 MHz

2

EE 434 Homework 12

P_{max} for $0.4" \times 0.9"$ waveguide @ 10 GHz

$$\hat{E}_y = E_{y,max} \sin \frac{\pi}{a} x$$

$$\hat{H}_x = -E_{y,max} \sqrt{\frac{\epsilon}{\mu}} \sqrt{1 - \left(\frac{f_c}{f}\right)^2} \sin \frac{\pi}{a} x$$

$$\overline{P_{ave}} = \frac{1}{2} \text{Re} \{ \hat{E} \times \hat{H}^* \} = \frac{1}{2} \text{Re} \left\{ \hat{a}_z E_{y,max}^2 \sin^2 \left(\frac{\pi}{a} x \right) \sqrt{\frac{\epsilon}{\mu}} \sqrt{1 - \left(\frac{f_c}{f}\right)^2} \right\}$$

$$P_{ave} = \frac{1}{2} E_{y,max}^2 \sqrt{\frac{\epsilon}{\mu}} \sqrt{1 - \left(\frac{f_c}{f}\right)^2} \int_{y=0}^b \int_{x=0}^a \sin^2 \left(\frac{\pi}{a} x \right) dx dy$$

$\frac{1}{2} \left[1 - \cos \left(\frac{2\pi x}{a} \right) \right]$

$$P_{ave} = \frac{1}{2} E_{y,max}^2 \sqrt{\frac{\epsilon}{\mu}} \sqrt{1 - \left(\frac{f_c}{f}\right)^2} \frac{ba}{2} \quad (\text{Equation 8-90})$$

$$\text{or } P_{ave} = 1.16 \times 10^{-7} E_{y,max}^2$$

but $E_{y,max} \cong 3 \times 10^6 \text{ V/m}$ in air

$$\text{so } P_{ave,max} = 1.16 \times 10^{-7} \times 9 \times 10^{12} = 1.04 \times 10^6 \text{ W}$$