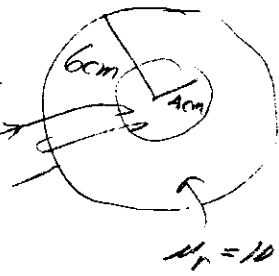


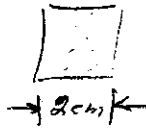
5-4

$I = 0.1$

$n = 100$



cross section



$R = \frac{2\pi \times 5 \times 10^{-2}}{10^3 \times 4\pi \times 10^{-7} \times 4 \times 10^{-4}}$

$R = \frac{10^{-1}}{16 \times 10^{-8}} = 0.0625 \times 10^7$

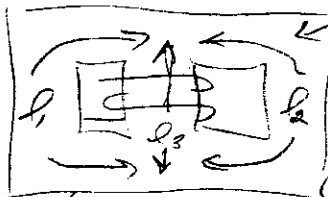
$\therefore \psi_m = \frac{nI}{R} = \text{Bav} A = \mu H_{\text{av}} A$

or  $H_{\text{av}} = \frac{nI}{R \mu A} = \frac{n I \times A}{\mu \times A} = \frac{nI}{\mu} = \frac{100}{2\pi \times 5 \times 10^{-2}} = 0.318 \times 10^2$

b)  $\oint H_{\text{eff}} = nI$  or  $H_{\text{eff}} = \frac{nI}{\mu}$  (the same as above)

with air gap don't have a path with constant  $H$  so cannot take  $H$  outside of the integral to find its value

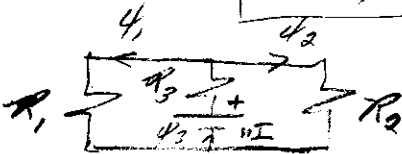
5-5



$H_f = 10^4, I = 0.1, n = 80$

$l_3 = 4 \text{ cm}, l_1 = l_2 = 12 \text{ cm}$

$A = 2 \text{ cm}^2 = 2 \times 10^{-4} \text{ m}^2$



$\psi_1 = \psi_2 = \psi_3$

$\psi_3 = \frac{nI}{R_3 + \frac{R_1}{2}}$

$\psi_3 = \frac{8}{\frac{4 \times 10^{-2}}{4\pi \times 10^{-7} \times 10^4} + \frac{6 \times 10^{-2}}{4\pi \times 10^{-7} \times 10^4} + \frac{2 \times 10^{-4}}{2 \times 10^{-4}}} = \frac{8 \times 4\pi \times 10^{-7} \times 10^4 \times 2 \times 10^4}{10^{-1}}$

$\psi_3 = 201.06 \times 10^{-6} = 0.201 \text{ mW} = 2\psi_{1,2}$

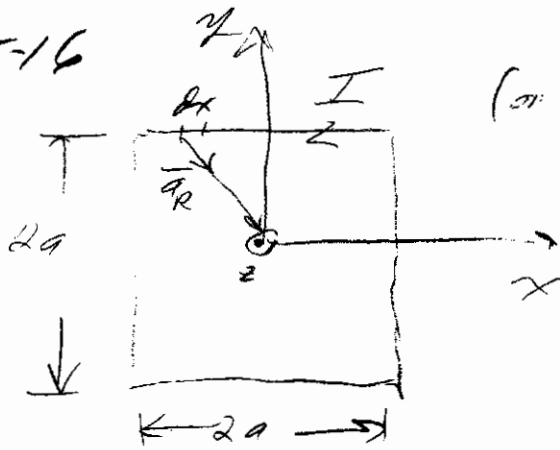
$B_{\text{av}3} = \frac{\psi_3}{A} = \frac{0.201 \times 10^{-3}}{2 \times 10^{-4}} = 0.1 \times 10 \approx 1 \text{ Weber/m}^2$

$B_{\text{av}1} = B_{\text{av}2} = \frac{\psi_1}{A} \approx 0.5 \text{ Weber/m}^2$

$H_{\text{av}3} = 2H_{\text{av}1} = 2H_{\text{av}2} = \frac{B_{\text{av}3}}{\mu_0 \mu_r} = \frac{1}{4\pi \times 10^{-7} \times 10^4} \approx 8 \times 10^4$

$[H_{\text{av}1} l_1 + H_{\text{av}3} l_3 = nI] ? \Rightarrow 40 \times 0.12 + 80 \times 0.04 = 8$   
 $4.8 + 3.2 = 8$  } QED

5-16



$$dB = \frac{\mu I dx \bar{a}_x \times \bar{a}_R}{4\pi (x^2 + a^2)}$$

$$\bar{a}_R = \frac{-x\bar{a}_x - a\bar{a}_z}{\sqrt{x^2 + a^2}}$$

$$\therefore dB = \frac{\mu I dx (-a\bar{a}_z)}{4\pi (x^2 + a^2)^{3/2}}$$

$$B_{z, \text{top}} = \int_a^{-a} \frac{-\mu I a dx}{4\pi (x^2 + a^2)^{3/2}} = \frac{-\mu I a}{4\pi} \left\{ \frac{x}{a^2 \sqrt{x^2 + a^2}} \right\}_a^{-a}$$

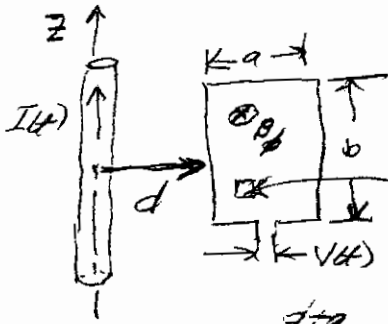
$$B_{z, \text{top}} = \frac{-\mu I}{4\pi} \left\{ \frac{-1}{a\sqrt{2}a} - \frac{1}{a\sqrt{2}a} \right\} = \frac{2\mu I}{4\pi \sqrt{2}a}$$

$$B_{z, \text{top}} = \frac{\mu I}{2\pi a\sqrt{2}} = \frac{\mu I \sqrt{2}}{4\pi a}$$

by symmetry other 3 sides contribute the same

$$\therefore B_z @ \text{center} = 4B_{z, \text{top}} = \frac{\mu I \sqrt{2}}{\pi a}$$

5.19



$$I(t) = I_m \sin \omega t$$

a)  $H_\phi = \frac{I_m \sin \omega t}{2\pi r}$  from  $\oint \vec{H} \cdot d\vec{l} = I$

$$\vec{B} = \mu_0 \mu_r \mu_0 \vec{H}$$

b)  $\oint \vec{E} \cdot d\vec{l} = V(t) = -\frac{d}{dt} \int_{\rho=d}^{d+a} \int_{z=0}^b \frac{\mu_0 I_m \sin \omega t}{2\pi r} dz dp$

$$V(t) = -\frac{d}{dt} \left\{ \frac{\mu_0 I_m \sin \omega t b}{2\pi} \ln\left(\frac{d+a}{d}\right) \right\} = -\frac{\mu_0 I_m \omega b \cos \omega t}{2\pi} \ln\left(\frac{d+a}{d}\right)$$

(right hand terminal positive) case A page 882

or  $\infty$ . because  $\vec{F}$  on positive charges would be in the  $z$  direction on both long sides of the loop but of greater magnitude on the left hand side driving a net positive charge to the right hand terminal.

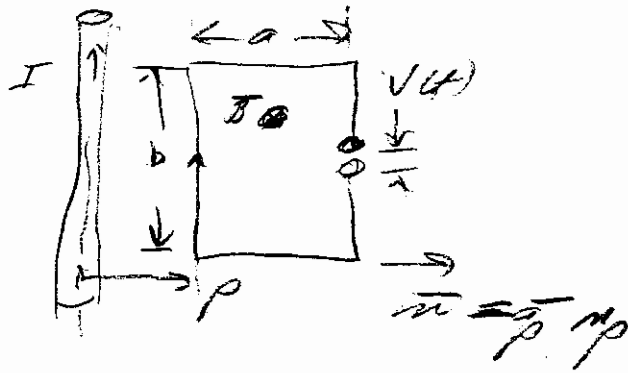
for  $I_m = 10A$ ,  $f = 20kHz$ ,  $d = 4 \times 10^{-3}m$ ,  $a = b = 0.1m$

$$V(t) = -\frac{4\pi \times 10^{-7} \times 10 \times 2\pi \times 20 \times 10^3 \times 0.1 \cos(2\pi \times 20 \times 10^3 t)}{2\pi} \ln\left(1 + \frac{0.1}{4 \times 10^{-3}}\right)$$

$$V(t) = -81.88 \times 10^{-3} \cos(4\pi \times 10^4 t) = \boxed{-81.9 \cos(4\pi \times 10^4 t) \text{ mV}}$$

c) 2 times above with opposite polarity

5.21



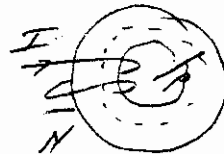
$$V(t) = \oint \mathbf{E} \cdot d\mathbf{l} = \int \nabla \times \mathbf{B} \cdot d\mathbf{l}$$

$$\mathbf{B} = \frac{\mu_0 I}{2\pi \rho} \hat{\phi}$$

$$\text{so } V(t) = \int_0^b \frac{\mu_0 I \rho}{2\pi} \frac{1}{z} dz + \int_b^0 \frac{\mu_0 I \rho}{2\pi (\rho + a)} dz = \frac{\mu_0 I a}{2\pi} \left\{ \frac{b}{\rho} - \frac{b}{\rho + a} \right\}$$

top terminal positive

5.23  $U_m = \frac{1}{2} \int_V \mathbf{B} \cdot \mathbf{H} dV$



$$\oint \mathbf{H} \cdot d\mathbf{l} = NI$$

$$H_d = \frac{NI}{2\pi}$$

a) so  $U_m = \frac{1}{2} \int_V \int_{\rho=a}^b \int_{z=0}^d \frac{\mu N^2 I^2}{4\pi \rho^2} dz \rho d\rho = \frac{\mu N^2 I^2 d}{4\pi} \ln \frac{b}{a}$

or  $U_m = \frac{\mu d N^2 I^2}{4\pi} \ln \frac{b}{a} = \frac{1}{2} L I^2$

$$L = \frac{2U_m}{I^2} = \frac{\mu d N^2}{2\pi} \ln \frac{b}{a}$$

same as Example 5-17

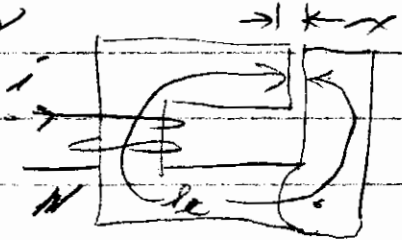
b)  $I = 2, \mu_r = 4 \times 10^3, a = 10^{-2}, b = 3 \times 10^{-2}, d = 2 \times 10^{-2}, N = 150$

$$U_m = \frac{4 \times 10^3 \times 150^2 \times 2 \times 10^{-2} \times 4 \times 10^{-4}}{2\pi} \ln 3 = 7.91 \times 10^{-2} \text{ J}$$

so  $L = \frac{2U_m}{I^2} = \frac{2 \times 7.91 \times 10^{-2}}{4} = 0.395 \text{ H}$

c) if  $\mu_r = f(I)$  or  $f(H)$  which would be true for ferromagnetic materials?

5.48



a)  $\oint \vec{B} \cdot d\vec{l} = \frac{\mu_0 N I}{R_{int} + R_{ext}} = \frac{\mu_0 N I}{R_{total}}$

b)  $L = \frac{\Phi}{I} = \frac{N \oint \vec{B} \cdot d\vec{l}}{I} = \frac{N^2}{R_{total}}$

so  $U_m = \frac{1}{2} L I^2 = \frac{1}{2} \frac{N^2}{R} I^2$

found that  $F_x = \frac{\partial U_m}{\partial x} = \frac{I^2}{2} \frac{\partial L}{\partial x} = \frac{I^2}{2} \frac{\partial}{\partial x} \left( \frac{N^2}{R} \right) = \frac{-N^2 I^2}{2 R^2} \frac{\partial R}{\partial x}$

or  $F_x = -\frac{1}{2} \frac{\partial}{\partial x} \left( \frac{N^2 I^2}{R} \right)$

so for  $\mu_0 = 4\pi \times 10^{-7}$ ,  $A_c = 4 \times 10^{-4}$ ,  $r = 1.5 \times 10^{-3}$ ,  $I = 1.25$  A,  $N = 200$

and  $\mu = 10^5 \mu_0$

$R_{total} = \frac{0.12}{10^5 \times 4\pi \times 10^{-7} \times 4 \times 10^{-4}} + \frac{r}{4\pi \times 10^{-7} \times 4 \times 10^{-4}} = 2.387 \times 10^3 + 0.0298 \times 10^3$

$\mu_m = \frac{200 \times 1.25}{R_{total}} = \frac{2.5 \times 10^2}{2.98 \times 10^6} = 0.839 \times 10^{-4}$  Webers

so  $F_x = -\frac{1}{2} (0.839 \times 10^{-4})^2 \times 1.99 \times 10^9 = -7$  Newtons

$B_{ave} = \frac{\mu_m}{A} = \frac{0.839 \times 10^{-4}}{4 \times 10^{-4}} = 0.21$  W/m<sup>2</sup>

$H_{ave} = \frac{B_{ave}}{\mu} = \frac{0.21}{4\pi \times 10^{-7}} = 1.67 \times 10^5$

$H_{ext} = \frac{0.21}{4\pi \times 10^{-7} \times 10^5} = 1.67$

$L = \frac{4\pi \times 10^{-4}}{2.98 \times 10^6} = 1.31 \times 10^{-2} \approx 13$  mH

$U_m = \frac{1}{2} L I^2 = \frac{1}{2} 1.31 \times 10^{-2} \times 1.25^2 = 1.02 \times 10^{-2}$

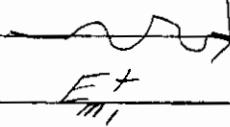
If  $r = 0.75$  mm  $R_{total} = \frac{R_{old}}{2}$  so  $\mu_m = 2\mu_{m, old}$  and  $F_x_{new} = 4 F_x_{old}$

5.48  $x=0$   $\frac{dR}{dx}$  is same as before but  $R = R_{\text{min}} = 2.387 \times 10^3$

$$\text{so } \mu = \frac{2.5 \times 10^2}{2.387 \times 10^3} = 1.047 \times 10^{-1}$$

$$\text{and } F_x = -\frac{1}{2} (1.047 \times 10^{-1})^2 \times 1.99 \times 10^9 = \boxed{-1.09 \times 10^7 \text{ N}}$$

6-5 air |  $\epsilon = \epsilon_0$



$$\frac{E_{m2}^+}{E_{m1}^+} = \frac{n_2}{n_1 + n_2} = \frac{2 + \frac{1}{\sqrt{\epsilon_r}}}{10 + \frac{1}{\sqrt{\epsilon_r}}}$$

so  $\boxed{\frac{E_{m2}^+}{E_{m1}^+} = \frac{2}{1 + \sqrt{\epsilon_r}}}$

$$\boxed{\frac{E_{m1}^-}{E_{m1}^+} = \frac{n_2 - n_1}{n_2 + n_1} = \frac{\frac{1}{\sqrt{\epsilon_r}} - 1}{\frac{1}{\sqrt{\epsilon_r}} + 1} = \frac{1 - \sqrt{\epsilon_r}}{1 + \sqrt{\epsilon_r}}}$$

b)  $E_{m1}^+ = 100$ ,  $\epsilon_r = 2.25$ ,  $\sqrt{\epsilon_r} = 1.5$

$$\frac{E_{m2}^+}{E_{m1}^+} = \frac{100 \times 2}{2.5} = \boxed{80}$$

$$E_{m1}^- = 100 \frac{1 - 1.5}{1 + 1.5} = \boxed{-20}$$

c)  $\epsilon_r = 81$ ;  $\sqrt{\epsilon_r} = 9$

$$\text{so } \frac{E_{m2}^+}{E_{m1}^+} = \frac{100 \times 2}{10} = \boxed{20 \frac{\text{V}}{\text{m}}}$$

$$E_{m1}^- = 100 \frac{1 - 9}{1 + 9} = \boxed{-80 \frac{\text{V}}{\text{m}}}$$

$$6-6 \quad n_{\text{phase}} = \frac{\omega}{\beta} = \frac{\omega}{2\pi f \beta} = \frac{c}{v_{\text{eff}}} \leftarrow$$

$$\text{index of refraction } n = \sqrt{\epsilon_r} \quad \text{so } n = \frac{c}{v_{\text{ph}}} \leftarrow$$

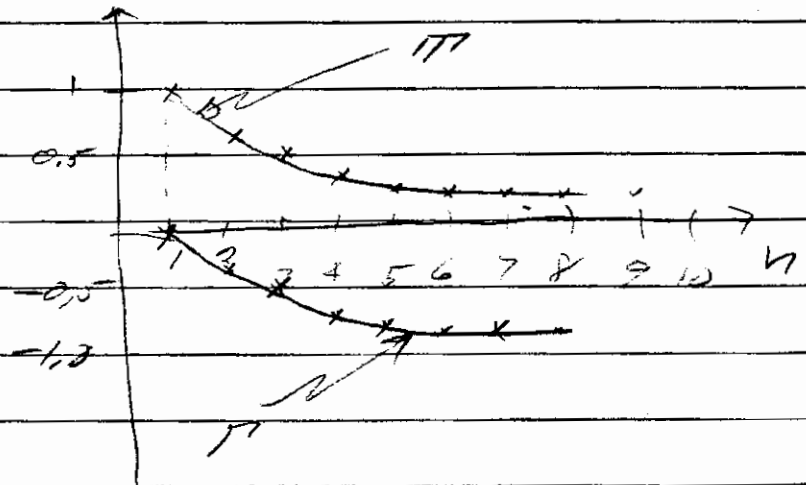
$$n_{\text{polyethylene}} = \sqrt{2.25} = 1.5 \leftarrow$$

$$n_{\text{water}} = \sqrt{81} = 9 \leftarrow$$

$$\Gamma = \frac{1-n}{1+n} \quad ; \quad T = \frac{2}{1+n}$$

$$\Gamma - \Gamma = \frac{2 - 1 + n}{1 + n} = 1 \quad \leftarrow \left\{ \begin{array}{l} E \text{ field is continuous} \\ \text{at boundary} \end{array} \right.$$

$n$	$\Gamma$	$T$
1	1	0
2	0.67	-0.33
3	0.5	-0.5
4	0.4	-0.6
5	0.33	-0.67
6	0.29	-0.71
7	0.25	-0.75
8	0.22	-0.77
9	0.2	-0.8
10	0.18	-0.82



EE #34

Homework 4

$$6-17 \quad \eta_1 \quad | \quad \eta_2 \quad | \quad \eta_3 \quad \delta_2 \rightarrow j\beta_2$$

$$\leftarrow \lambda/4 \rightarrow \quad e^{j\beta_2 d} \rightarrow e^{j \frac{2\pi}{\lambda} \cdot \frac{\lambda}{4}} = j$$

$$\text{Then } \hat{Z}_1(0) = \eta_2 \frac{j(\eta_3 + \eta_2) - j(\eta_3 - \eta_2)}{j(\eta_3 + \eta_2) + j(\eta_3 - \eta_2)} = \frac{2j\eta_2\eta_3}{2j\eta_3} = \frac{\eta_2}{\eta_3} \leftarrow$$

6-18  $\epsilon_{r3} = 2.56$  in above problem we need  $\hat{Z}_1(0) = \eta_1$

$$\infty \quad \eta_2 = \sqrt{\eta_1 \eta_3} \quad \text{or for all } \mu = \mu_0$$

$$\text{we want } \frac{\mu_0}{\epsilon_r} = \sqrt{\frac{\mu_0^2}{\epsilon_1 \epsilon_3}} \quad ; \quad \epsilon_{r2} = \frac{1}{\sqrt{\epsilon_{r1} \epsilon_{r3}}}$$

$$\boxed{\epsilon_{r2} = \sqrt{1 \times 2.56} = 1.6} \quad \leftarrow$$

reciprocal because get same value for  $\eta_2$  if  $\eta_1$  +  $\eta_3$  are interchanged?

$$6-20 \quad \eta_1 \quad | \quad \eta_2 \quad | \quad \eta_3 \quad e^{j\beta_2 d} \rightarrow e^{j\pi} = -1$$

$$\leftarrow \lambda/2 \rightarrow$$

$$\text{so } \hat{Z}_1(0) = \eta_2 \frac{-(\eta_3 + \eta_2) - (\eta_3 - \eta_2)}{-(\eta_3 + \eta_2) + (\eta_3 - \eta_2)} = \frac{\eta_2 (-2\eta_3)}{-2\eta_2} = \frac{\eta_2}{\eta_3}$$

same result whenever  $e^{j \frac{2\pi}{\lambda} \cdot d} = -1$

$$\text{or } d = n \frac{\lambda}{2} \quad ; \quad n = 1, 2, 3, \dots$$



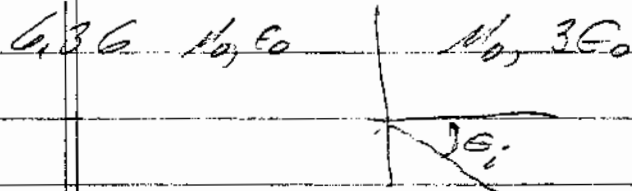
$$6-35 \quad \textcircled{1} \quad \left| \quad \textcircled{2} \quad \theta_i = \tan^{-1} \sqrt{\frac{\epsilon_2}{\epsilon_1}} \right. \\ n_0, \epsilon_0 \quad \left| \quad n_0, 3\epsilon_0 \quad \text{Brewster}$$

$$\begin{aligned} \text{is from } \textcircled{1} \rightarrow \textcircled{2} \quad \theta_{iB} = 60^\circ \\ \textcircled{2} \rightarrow \textcircled{1} \quad \theta_{iB} = 30^\circ \end{aligned} \quad \left. \vphantom{\begin{aligned} \text{is from } \textcircled{1} \rightarrow \textcircled{2} \\ \textcircled{2} \rightarrow \textcircled{1} \end{aligned}} \right\} \text{so}$$

must be // polarized  $\leftarrow$

$$\frac{\sqrt{\epsilon_2}}{\sqrt{\epsilon_1}} \leftrightarrow \tan^{-1} \sqrt{\frac{\epsilon_2}{\epsilon_1}} = 90^\circ - \tan^{-1} \sqrt{\frac{\epsilon_1}{\epsilon_2}}$$

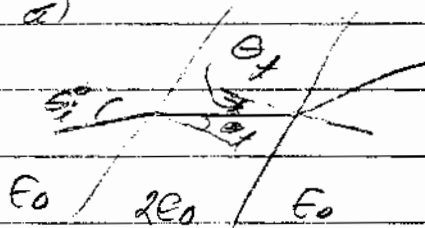
so  $\theta_{iB}$  angle from opposite directions are always compliments!



$$\theta_{\text{critical}} = \sin^{-1} \sqrt{\frac{1}{3}} = \underline{\underline{35.26^\circ}}$$

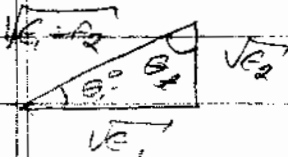
polarization not important

6.37 a)



$$\theta_i^\circ = \tan^{-1} \sqrt{\frac{\epsilon_2}{\epsilon_1}}$$

$$\frac{\sin \theta_t}{\sin \theta_i} = \sqrt{\frac{\epsilon_1}{\epsilon_2}}$$



$$\sin \theta_t = \frac{\sqrt{\epsilon_2}}{\sqrt{\epsilon_1 + \epsilon_2}} \cdot \sqrt{\frac{\epsilon_1}{\epsilon_2}} = \frac{\sqrt{\epsilon_1}}{\sqrt{\epsilon_1 + \epsilon_2}}$$

thus we see that  $\theta_t = 90^\circ - \theta_i^\circ$

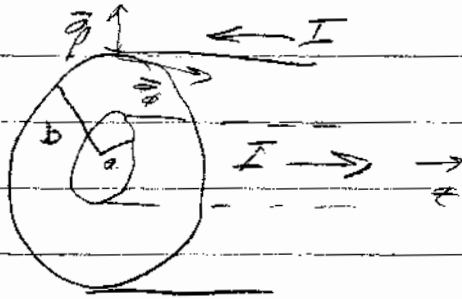
We showed in problem 6.35 that the Brewster angle for waves incident on the interface from either side are complementary angles. The angle of incidence at the second surface is  $\theta_t$ , so there will be no reflection at this surface because  $\theta_t = 90^\circ - \theta_i^\circ$  as shown above.

$$b) \Gamma_{\parallel} = 0 \quad ; \quad \theta_i^\circ = \tan^{-1} \sqrt{2} = 54.73^\circ$$

$$\Gamma_{\perp} = \frac{\cos \theta_i - \sqrt{\frac{\epsilon_2}{\epsilon_1}} \cos \theta_t}{\cos \theta_i + \sqrt{\frac{\epsilon_2}{\epsilon_1}} \cos \theta_t} \quad ; \quad \theta_t = \sin^{-1} \left( \sqrt{\frac{\epsilon_1}{\epsilon_2}} \sin \theta_i \right) = 35.26^\circ$$

$$\Gamma_{\perp} = \frac{0.5774 - 1.155}{0.5774 + 1.155} = \frac{-0.577}{1.732} = \underline{\underline{-0.333}}$$

7.2



$$E_z = \frac{-J_z}{\sigma} ; J_z = \frac{I}{\pi(c^2 - b^2)}$$

$$H_\phi = \frac{I}{2\pi r}$$

$$\overline{E \times H} = \frac{J_z I}{\sigma 2\pi b} \frac{a}{r} = \frac{I^2}{2\pi \sigma (c^2 - b^2)} \frac{a}{r}$$

$$P_{\text{into outer conductor}} = \int_{z=0}^L \int_{\phi=0}^{2\pi} \frac{I^2 a}{2\pi \sigma b (c^2 - b^2)} \cdot b db d\phi dz$$

$$P = \frac{2\pi L I^2}{2\pi \sigma (c^2 - b^2)} = I^2 \frac{L}{\sigma \pi (c^2 - b^2)} = I^2 R \quad \checkmark$$

7-13  $\hat{E}_x = \hat{E}_m^+ e^{j\beta z} [1 + \Gamma]$   $\hat{H}_y = \frac{\hat{E}_m^+}{\eta} e^{-j\beta z} [1 - \Gamma]$

$P_{ave} = \frac{1}{2} \text{Re} \{ \hat{E} \times \hat{H}^* \} = \frac{1}{2} \text{Re} \left\{ \frac{|\hat{E}_m^+|^2}{\eta} (1 + \Gamma)(1 - \Gamma^*) \right\} \hat{a}_z$

$\bar{P}_{ave} = \frac{|\hat{E}_m^+|^2}{2\eta} \text{Re} \{ 1 + \Gamma + \Gamma^* + \Gamma\Gamma^* - \Gamma - \Gamma^* - |\Gamma|^2 \} \hat{a}_z$

$\bar{P}_{ave} = \frac{|\hat{E}_m^+|^2}{2\eta} [1 - |\Gamma|^2] \hat{a}_z = \bar{P}_{ave}^+ - \bar{P}_{ave}^- \leftarrow$

$\therefore \frac{|\bar{P}_{ave}^-|}{|\bar{P}_{ave}^+|} = |\Gamma|^2 \leftarrow$

7-17  $P_{ave} = \frac{1}{2} \text{Re} \left\{ \frac{|\hat{E}_m^+|^2}{\eta} e^{-2\alpha z} e^{j\theta} [1 + \Gamma] [1 - \Gamma^*] \right\}$

$P_{ave} = \frac{|\hat{E}_m^+|^2}{2\eta} e^{-2\alpha z} \text{Re} \left\{ [ \cos\theta + j \sin\theta ] [ 1 + \Gamma + \Gamma^* + \Gamma\Gamma^* - \Gamma - \Gamma^* - |\Gamma|^2 ] \right\}$

$P_{ave} = \frac{|\hat{E}_m^+|^2}{2\eta} e^{-2\alpha z} \left\{ \cos\theta [1 - |\Gamma|^2] - \sin\theta [2\Gamma_i] \right\} \leftarrow (1)$

for  $\Gamma = 0$  this becomes  $P_{ave} = \frac{|\hat{E}_m^+|^2}{2\eta} e^{-2\alpha z} \cos\theta \leftarrow$

b) lossless case  $\eta \rightarrow \eta$  i.e.  $\theta \rightarrow 0$  and  $\alpha \rightarrow 0$

giving:  $P_{ave} = \frac{|\hat{E}_m^+|^2}{2\eta} [1 - |\Gamma|^2]$  as in 7-13

$P_{ave} = \frac{1}{2} \text{Re} \left\{ \frac{\hat{E}_m^+}{\eta} e^{-\alpha z} e^{j\beta z + j\theta} \frac{\hat{E}_m^{*+}}{\eta} e^{-\alpha z} e^{-j\beta z + j\theta^*} \right\} = \frac{|\hat{E}_m^+|^2}{2\eta} e^{-2\alpha z} \cos\theta$   
 positive wave

$P_{ave} = \frac{1}{2} \text{Re} \left\{ \frac{\hat{E}_m^+}{\eta} e^{-\alpha z} e^{j\beta z} \frac{\hat{E}_m^{*+}}{\eta} e^{-\alpha z} e^{-j\beta z} (-\Gamma^*) \right\} = \frac{|\hat{E}_m^+|^2}{2\eta} e^{-2\alpha z} |\Gamma|^2 \cos\theta$   
 negative wave

summing these two terms would miss the  $-\sin\theta [2\Gamma_i]$  term in the above expression?

$$7-21 \quad P_{\text{avg}} \text{ of sun} = 1340 \text{ W/m}^2 \\ \text{@ earth}$$

assuming single frequency wave we have:

$$P_{\text{avg}} = \frac{|\hat{E}_m|^2}{2\eta} ; \text{ or } |\hat{E}_m| = \sqrt{2 \times 377 \times 1340} = 1.005 \times 10^3 \text{ V/m}$$

$$|\hat{H}_m| = \frac{|\hat{E}_m|}{\eta} = 2.66 \text{ A/m}$$

$$P_{\text{total}} \text{ from sun} = 4\pi (1.48 \times 10^{11})^2 \cdot 1340 \text{ W/m}^2 = 36.88 \times 10^{25} \text{ Watts}$$

A. 1" radius @ wavelength

$$f_c = \frac{c}{2\pi r} = \frac{3 \times 10^8 \times 1.8 \times 10^{-2}}{2\pi \times 2.54} = 3.46 \times 10^9 \text{ Hz}$$

B.  $P_{\text{max}}$  for  $0.4 \times 0.9'$  waveguide @  $10 \text{ GHz}$

$$E_y = -jK \frac{\omega \mu_0}{\pi} \sin \frac{\pi}{a} x = E_{y\text{max}} \sin \frac{\pi}{a} x$$

$$H_x = K_j \frac{\beta_{z0} a}{\pi} \sin \frac{\pi}{a} x = -E_{y\text{max}} \sqrt{\frac{\epsilon}{\mu}} \sqrt{1 - \left(\frac{f_c}{f}\right)^2} \sin \frac{\pi}{a} x$$

$$P_{\text{ave}} = \frac{1}{2} \int_0^a \int_0^b \vec{E} \times \vec{H} \cdot \hat{z} \, dx \, dy = \frac{1}{2} \int_0^a E_{y\text{max}}^2 \sin^2 \frac{\pi}{a} x \sqrt{\frac{\epsilon}{\mu}} \sqrt{1 - \left(\frac{f_c}{f}\right)^2} \, dx \int_0^b dy$$

$$P_{\text{ave}} = \frac{1}{2} E_{y\text{max}}^2 \sqrt{\frac{\epsilon}{\mu}} \sqrt{1 - \left(\frac{f_c}{f}\right)^2} \int_0^a \sin^2 \frac{\pi}{a} x \, dx \int_0^b dy$$

$\frac{1}{2} [1 - \cos \frac{2\pi x}{a}]$

so  $P_{\text{ave}} = \frac{1}{2} E_{y\text{max}}^2 \sqrt{\frac{\epsilon}{\mu}} \sqrt{1 - \left(\frac{f_c}{f}\right)^2} \frac{ba}{2}$  (Equation 8-90)

$$P_{\text{ave}} = 1.16 \times 10^{-7} E_{y\text{max}}^2$$

but  $E_{y\text{max}} \approx 3 \times 10^6 \text{ V/m}$  so  $P_{\text{ave}} = 1.16 \times 10^{-7} \times 9 \times 10^{12} \approx 1.04 \times 10^6 \text{ W}$

P.23  $f_c = \frac{1}{2\sqrt{\mu\epsilon} a}$  TE<sub>10</sub> mode

a)  $5 \text{ GHz}$ ;  $a_{\text{min}} = \frac{1}{2\sqrt{\mu\epsilon} f} = \frac{3 \times 10^8}{10 \times 10^9} = 3 \times 10^{-2} \text{ m}$  ←

b)  $5 \text{ MHz}$ ;  $a_{\text{min}} = \frac{3 \times 10^8}{10 \times 10^6} = 30 \text{ m}$  ←

c)  $5 \text{ KHz}$ ;  $a_{\text{min}} = \frac{3 \times 10^8}{10 \times 10^3} = 3 \times 10^4 \text{ m}$  ←

9.27

TE<sub>10</sub> mode

$$f_c = \frac{1}{2\sqrt{\mu_0 \epsilon_0}} \frac{1}{15} = \frac{3 \times 10^8}{30} = 10 \text{ MHz}$$

Vertical polarization

AM will not propagate } 535 → 1605 KHz  
 FM will propagate } 88 → 108 MHz

$$11-11 \quad \Delta z = 0.01 \lambda; \quad \hat{I} = 5 \text{ A}; \quad f = 300 \text{ MHz}$$

$$a) \quad \lambda = \frac{3 \times 10^8}{3 \times 10^8} = 1 \text{ m} \quad \therefore \Delta z = 0.01 \text{ m}$$

(far zone if  $\beta_0 r \gg 1$  from (11-30)  
 so  $\beta_0 r = 80$  is reasonably in the far zone)

$$\text{this is } [r = \frac{80}{\beta_0} = \frac{80}{2\pi} \lambda = 3.18 \text{ m}]$$

$$b) \quad \hat{E}_\theta = \eta \hat{H}_\phi = \frac{j\omega\mu I \Delta z e^{-j\beta r}}{4\pi r} \sin\theta$$

$\sin\theta = 1 @ \theta = 90^\circ$

$$c) \quad \bar{P} = \frac{1}{2} \text{Re} \{ \hat{E}_\theta \hat{H}_\phi^* \} = \frac{1}{2} \cdot \frac{\omega^2 \mu^2 I^2 \Delta z^2}{4\pi^2 r^2} \hat{a}_r$$

$$\bar{P} = \frac{\omega^2 \mu^2 I^2 \Delta z^2 \sqrt{\epsilon} \sqrt{\mu}}{8\pi^2 r^2} = \frac{\eta I^2 \Delta z^2}{8\pi^2 \lambda^2 r^2}$$

$$\bar{P} = \frac{\eta I^2}{8\pi^2 r^2} \left(\frac{\Delta z}{\lambda}\right)^2 = \frac{377 \times 25 \times 10^{-4}}{8 \times 3.18^2} = 0.0117 \text{ Watts/m}^2$$

$$11-14 \quad P_{\text{rad}} = \int_{\phi=0}^{2\pi} \int_{\theta=0}^{\pi} \frac{\eta I^2}{8\pi^2} \left(\frac{\Delta z}{\lambda}\right)^2 \sin\theta \, d\theta \, d\phi$$

$$P_{\text{rad}} = \frac{\eta \pi I^2}{8} \left(\frac{\Delta z}{\lambda}\right)^2 \int_0^{\pi} \sin\theta \, d\theta = \frac{\eta \pi I^2}{3} \left(\frac{\Delta z}{\lambda}\right)^2$$

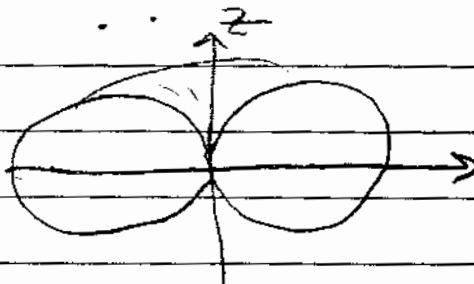
$$a) \quad \text{so } P_{\text{rad}} = \frac{\pi \times 377 \times 25 \times 10^{-4}}{3} = 0.99 \text{ Watts}$$

$$b) \quad \text{if } \Delta z \rightarrow 0.02 \text{ m} \quad P_{\text{rad}} = 4 \times 0.99 = 3.95 \text{ Watts}$$

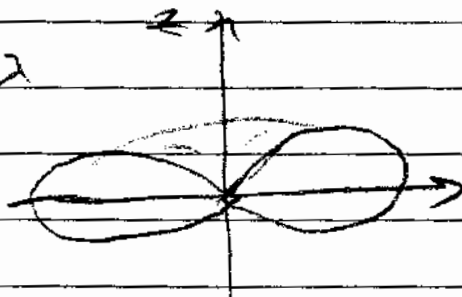
$$\text{if } \Delta z = 0.005 \text{ m} \quad P_{\text{rad}} = \frac{0.99}{4} = 0.25 \text{ Watts}$$



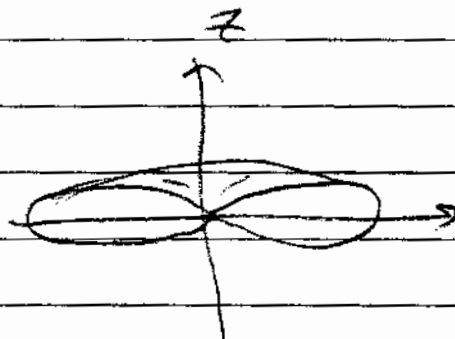
11-19 a)  $L = \frac{\lambda}{2}$



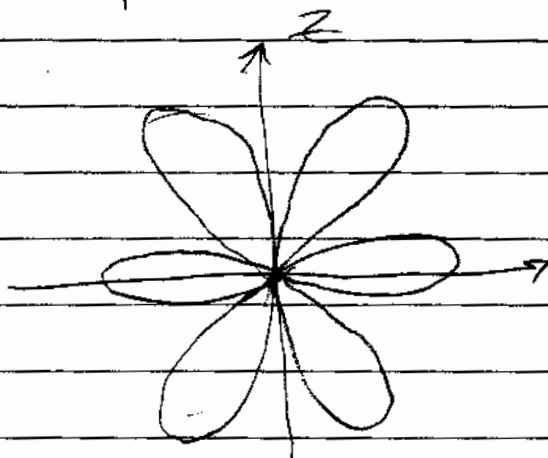
b)  $L = \frac{5}{4} \lambda$



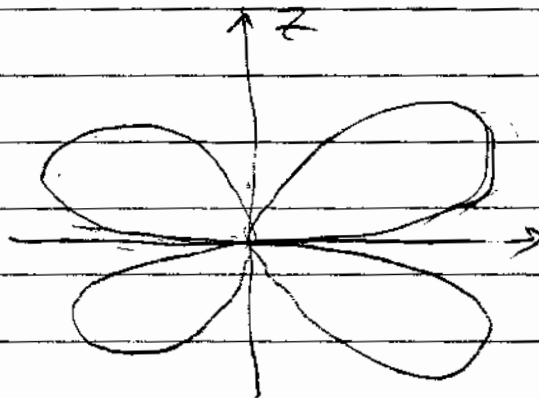
c)  $L = \lambda$



11-20 a)  $L = 1.5 \lambda$



b)  $L = 2 \lambda$



9.1 "dz" dipole ;  $I = 10A$  ;  $dz = \frac{\lambda}{50}$  ;  $r = 10^3 m$

$$P_{max} = \frac{1}{2} \eta_0 \left\{ \frac{\beta I^2 dz^2 \sin^2 \theta}{16\pi^2 r^2} \right\} = \frac{2\pi I^2 dz^2 \sin^2 \theta}{2\lambda 16\pi^2 r^2}$$

but  $\left[ \eta_0 = \frac{2\pi f \sqrt{\mu_0} \sqrt{\epsilon_0}}{c^2} = \frac{2\pi f \mu_0}{c} \right]$

$$\therefore P_{max} = \frac{I^2 dz^2 2\pi \eta_0}{\lambda^2 16\pi^2 r^2} = \frac{10^2 \times 120\pi}{(50)^2 \times 8 \times 10^6} = 1.88 \times 10^{-6} \frac{W}{m^2}$$

9.2  $L = 1m$  ;  $f = 10^6$   $\therefore \lambda = \frac{3 \times 10^8}{10^6} = 300m$  (short dipole)

$I = 12A$  ,  $r = 5 \times 10^3$

$$P(\theta = 30^\circ) = \frac{I^2 \eta_0}{8\pi^2} \left( \frac{dz}{\lambda} \right)^2 \sin^2 30^\circ = \frac{12^2 \times 377}{8 \times 25 \times 10^6} \left( \frac{1}{300} \right)^2 \sin^2 30^\circ = 7.57 \times 10^{-10} \frac{W}{m^2}$$

9.5  $L = 2a$  ,  $f = 10^6$   $\therefore \lambda = \frac{3 \times 10^8}{10^6} = 300m$  (short dipole)

Cu antenna  $\therefore \sigma = 5.8 \times 10^7$  wire radius =  $1mm$

a)  $R_{rad} = \frac{2\pi \eta_0}{3} \left( \frac{dz}{\lambda} \right)^2 = \frac{2\pi \times 377}{3} \left( \frac{2}{300} \right)^2 = 0.0351 \Omega$

$$R_{loss} = \frac{L}{2a} \sqrt{\frac{1}{\pi \sigma}} = \frac{2}{2 \times 10^{-3}} \sqrt{\frac{10^6 \times 4\pi \times 10^{-7}}{\pi \times 5.8 \times 10^7}} = 0.083 \Omega$$

so  $\epsilon = \frac{0.0351}{0.0351 + 0.083} = 0.297$  or  $29.7\%$

b)  $G = \epsilon \cdot D = 0.297 \times 1.5 = 0.446$  or  $-3.5/dB$

c)  $20 = \frac{I^2 \eta_0}{3} \left( \frac{dz}{\lambda} \right)^2$  or  $I = \sqrt{\frac{60}{\eta_0}} \left( \frac{\lambda}{dz} \right)$

or  $I = \sqrt{\frac{60}{120\pi^2} \left( \frac{\lambda}{dz} \right)^2} = \frac{1}{\sqrt{2\pi}} (150) = 33.76A$

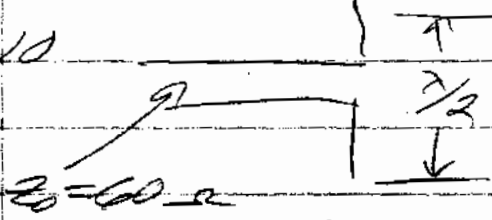
$P_{transmitter} = \frac{P_{rad}}{\epsilon} = \frac{20}{0.297} = 67.34 W$

$$9.8 \quad \xi = 90\% ; D_{dB} = 6.74 \text{ dB} ; G = ?$$

$$D_{dB} = 10 \log_{10} D \quad \therefore D = 10^{\frac{D_{dB}}{10}} = 4.677 ; G = \xi D = 4.2$$

$$\text{or } G_{dB} = 6.24 \text{ dB}$$

9.10



$$\equiv Z_L = 73$$

$$\Gamma_{\text{load}} = \frac{Z_L - Z_0}{Z_L + Z_0} = \frac{13}{133} = 0.0977$$

$$SWR = \frac{|V_{\text{max}}|}{|V_{\text{min}}|} = \frac{1 + |\Gamma|}{1 - |\Gamma|} = \frac{1 + 0.0977}{1 - 0.0977} = 1.217$$

$$9.15 \quad 3 \text{ GHz} ; 1 \text{ m dishes} ; P_T = 10^{-9} \text{ W} ; \gamma = 4 \times 10^{-4}$$

$$\lambda = \frac{3 \times 10^8}{3 \times 10^9} = 0.1 \text{ m}$$

$$P_r = 10^{-9} (\gamma \lambda)^2 \left( \frac{1}{A_r A_t} \right) = \frac{10^{-9} \times 16 \times 10^8 \times 10^{-2} \times 16}{\pi^2} = 25.94 \times 10^{-3} \text{ W}$$

9.16  $\lambda/2$  dipole ;  $P_t = 10^5$  ;  $f = 50 \text{ MHz}$  ;  $G_r = 13 \text{ dB}$   
 $R = 3 \times 10^4$  ;  $D_r = 19.95$  ;  $\lambda = \frac{3 \times 10^8}{5 \times 10^7} = 6 \text{ m}$

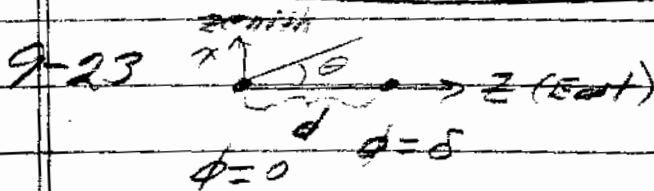
$$P_r = P_t D_r D_f \left( \frac{\lambda}{4\pi R} \right)^2 = 10^5 \times 19.95 \times 1.64 \left( \frac{6}{4\pi \times 3 \times 10^4} \right)^2 = 8.28 \times 10^{-6} \text{ W}$$

9.21 94 GHz ; antenna  $1 \text{ m} \times 0.1 \text{ m}$  ;  $\lambda = \frac{3 \times 10^8}{94 \times 10^9} = 3.19 \times 10^{-3} \text{ m}$

a) BW elevation  $\approx \frac{3.19 \times 10^{-3}}{0.1} = 3.19 \times 10^{-2} \text{ radians} = 1.8^\circ$

BW azimuth  $\approx 3.19 \times 10^{-3} \text{ radians} = 0.18^\circ$

b)  $d = 300 \times 3.19 \times 10^{-3} = 0.957 \text{ m}$



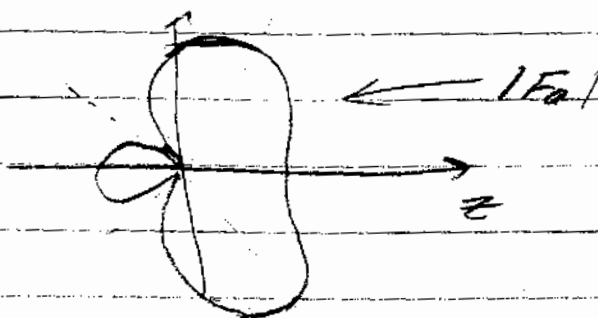
a)  $a_0 = a_1 = 1$  ;  $\delta = \frac{\pi}{4}$  ;  $d = \frac{\lambda}{2}$

uniform array :  $|F_a| = \frac{\sin(N\psi)}{\sin\psi}$  where  $\psi = \frac{2\pi}{\lambda} d \cos\theta - \delta$

so  $\psi = \pi \cos\theta - \frac{\pi}{4}$  and  $|F_a| = \frac{\sin\psi}{\sin\frac{\psi}{2}}$

maximum of array pattern @  $\psi = 0$  so  $\theta_{\max} = \cos^{-1} \frac{1}{4} = 78.52^\circ$

1<sup>st</sup> zero when  $\psi = -\pi = \pi \cos\theta - \frac{\pi}{4}$  or  $\cos\theta = -\frac{3}{4}$  ;  $\theta_{\text{zero}} = 132.6^\circ$



9.23 b)  $a_0=1, a_1=2, \delta=0, d=2$

$$F_a = 1 + 2e^{j\psi} ; \psi = \frac{2\pi}{\lambda} d \cos \theta - \phi = 2\pi \cos \theta$$

$$\therefore F_a = 1 + 2e^{j2\pi \cos \theta} = 1 + 2 \cos(2\pi \cos \theta) + j 2 \sin(2\pi \cos \theta)$$

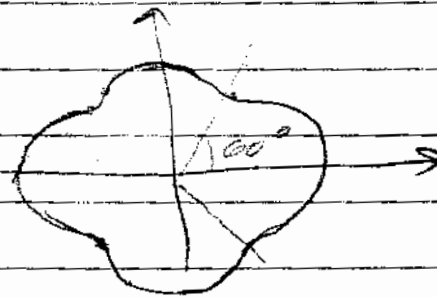
$$\text{so } |F_a| = [1 + 2 \cos(2\pi \cos \theta)]^2 + 4 \sin^2(2\pi \cos \theta)$$

$$|F_a| = 1 + 4 \cos(4\pi \cos \theta) + 4 = 5 + 4 \cos(4\pi \cos \theta)$$

computer plot gives:

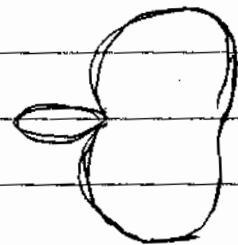
@  $\theta = 0 + 90^\circ$   $|F_a| = 9$

@  $\theta = 60^\circ$   $|F_a| = 1$



9.24 from 9.23a)

$$F_a =$$

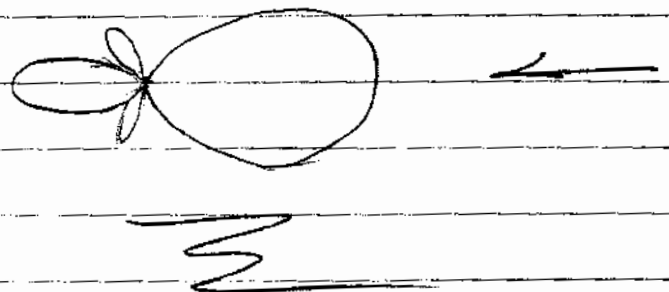


$$F_{\text{element}} =$$



$$\text{total pattern} = F_{\text{element}} \times F_a$$

$\therefore$  total pattern is



Broadcast Antenna Array  $[F_a = (z - z_1)(z - z_2)]$   
 where  $z = e^{j\psi} = e^{j\beta d \cos \theta}$

$\psi = 0$  (fed in phase) will provide maximum @  $\theta = 90^\circ$   
 next zeroes when  $\theta = 26^\circ$  and  $154^\circ$

$$e^{j\psi_1} = \frac{2\pi d}{\lambda} \cos 26^\circ = \frac{\pi}{2} \cos 26^\circ = 0.449\pi$$

$$e^{j\psi_2} = \frac{\pi}{2} \cos 154^\circ = -0.449\pi$$

$$\text{so } F_a = (z - e^{j0.449\pi})(z - e^{-j0.449\pi}) = z^2 - z(e^{j0.449\pi} + e^{-j0.449\pi}) + 1$$

$$\text{or } F_a = z^2 - 0.319z + 1$$

$$z = e^{j\frac{\pi}{2} \cos \theta}$$

(see attached plot)

9.18 a)  $P_t = 10\text{W}$ ,  $f = 6\text{GHz}$ ,  $G_t = 20\text{dB}$ ,  $G_r = 23\text{dB}$ ,  $R = 3 \times 10^8$

$$D(\theta, \phi) = \frac{P_{\text{W/m}^2} 4\pi R^2}{P_t}; \quad \lambda = \frac{3 \times 10^8}{6 \times 10^9} = 0.05\text{m}$$

$$\text{a) } P_{\text{@ receiver}} = \frac{G_t P_t}{4\pi R^2} = \frac{10 \times 10}{4\pi \times (3 \times 10^8)^2} = 0.0199 \times 10^{-7} = 1.99 \times 10^{-7} \text{ W/m}^2$$

$$\text{b) } P_{\text{receiver}} = P_t G_t G_r \left(\frac{\lambda}{4\pi R}\right)^2 = 1.99 \times 10^{-7} \times 25 \times 10^4 \times 199.53 \left(\frac{0.05}{4\pi \times 3 \times 10^8}\right)^2 = 7.999 \times 10^{-9} \text{ W}$$

$$\text{c) } N = \beta TB = 1.38 \times 10^{-23} \times 10^3 \times 10^7 = 1.38 \times 10^{-13} \text{ W/Hz} \quad \frac{S}{N} = 5.72 \times 10^4 \text{ or } 47.6\text{dB}$$

9.20 Beamwidth  $\theta = 1.5^\circ$  @  $20\text{GHz}$   $1.5^\circ \times \frac{\pi}{180} = \frac{15 \times 10^{-2}}{\text{dia}}$ ;  $\text{dia} = 0.573\text{m}$

$$\lambda = \frac{3 \times 10^8}{20 \times 10^9} = 15 \times 10^{-2} \text{ m}; \quad D = \frac{4\pi}{\lambda^2} A_{\text{eff}} = \frac{4\pi \times (0.573)^2}{2.25 \times 10^{-4} \times 4} = 1.44 \times 10^4$$

$$\text{a) } D = 1.44 \times 10^4 \text{ or } 41.6\text{dB}$$

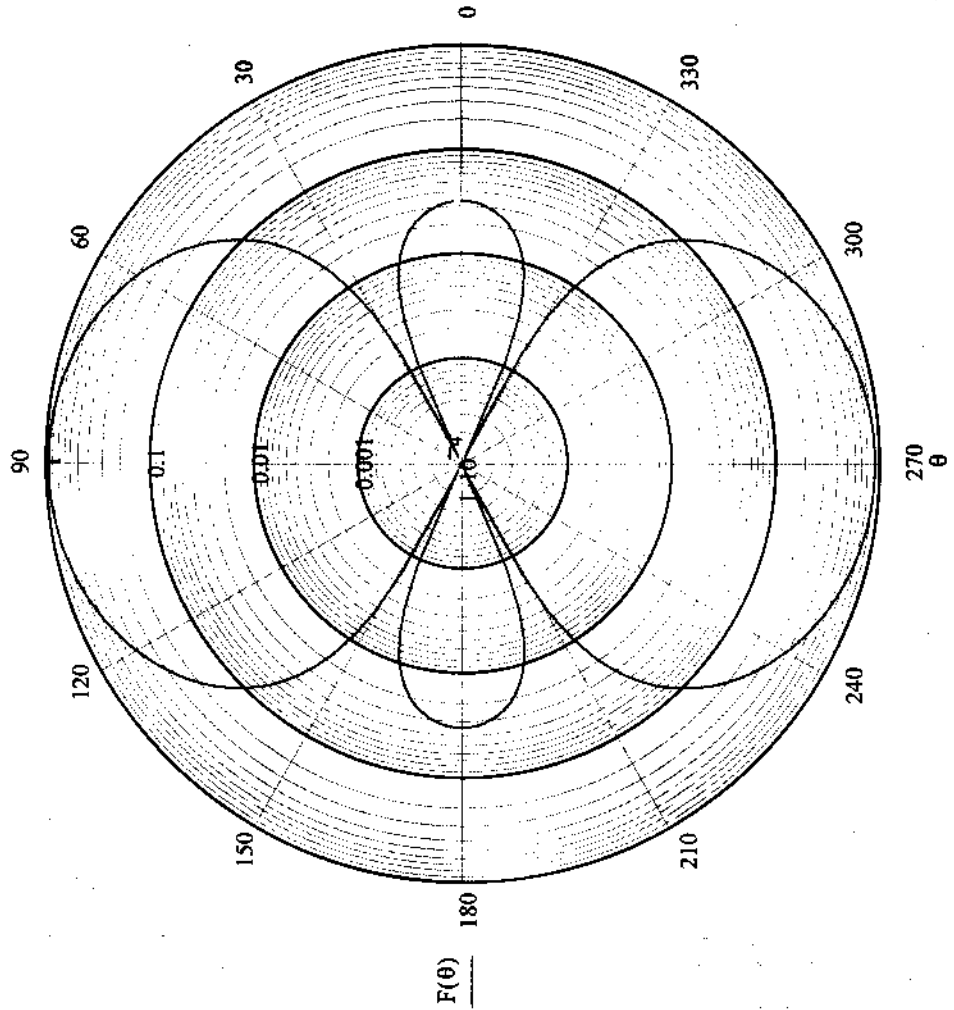
b) For twice the area  $D$  will be multiplied by 2 and beamwidth  $\div \sqrt{2}$

c) for twice the frequency  $D$  will be multiplied by 2 and  $\sqrt{2}$  multiplied by 4

### Broadcast Array Special Problem

$$j := \sqrt{-1}; \quad \theta := 0, \frac{\pi}{100}, \dots, 2\pi \quad z(\theta) := e^{j \frac{\pi}{2} \cos(\theta)} \quad z_1 := e^{j \frac{\pi}{2} \cos\left(26 \frac{\pi}{180}\right)} \quad z_2 := e^{j \frac{\pi}{2} \cos\left(154 \frac{\pi}{180}\right)}$$

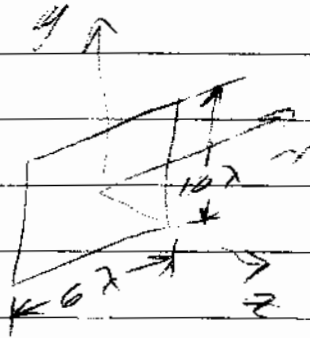
$$F(\theta) := \left[ \frac{1}{\sqrt{3}} \cdot (z(\theta) - z_1) \cdot (z(\theta) - z_2) \right]^2$$



Problems

Homework 12

11-26

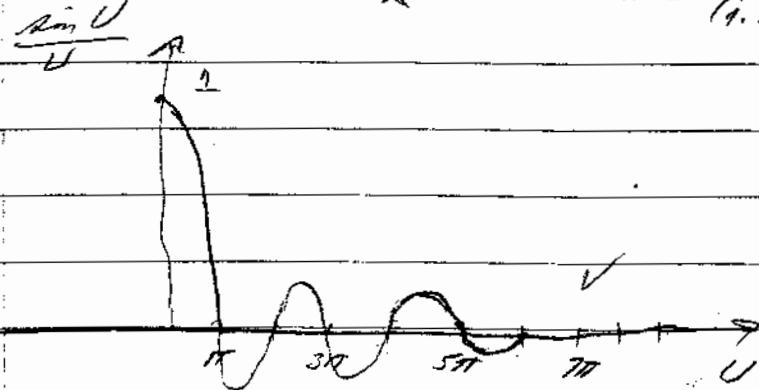


$\phi = 0$  pattern ( $xz$  plane)

$$\vec{E} = \frac{j\beta E_m}{4\pi r} ab (1 + \cos\theta) e^{j\beta r} \frac{\sin(\frac{\beta a \sin\theta}{2})}{\frac{\beta a \sin\theta}{2}}$$

(aperture is  $6\lambda$  wide in this plane)

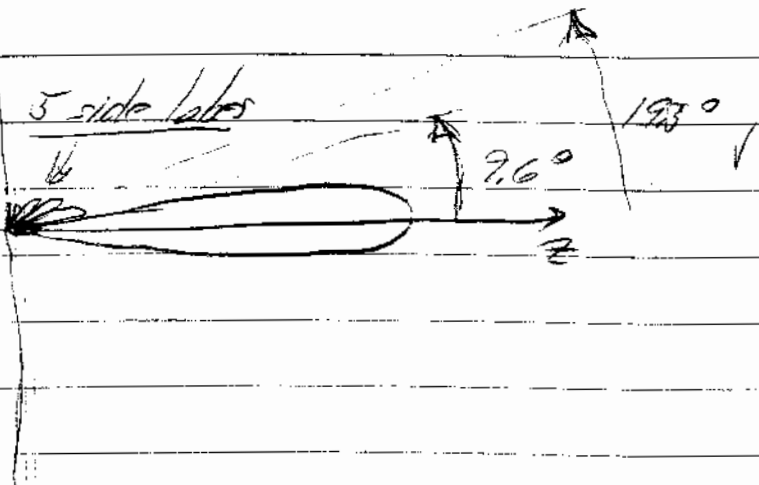
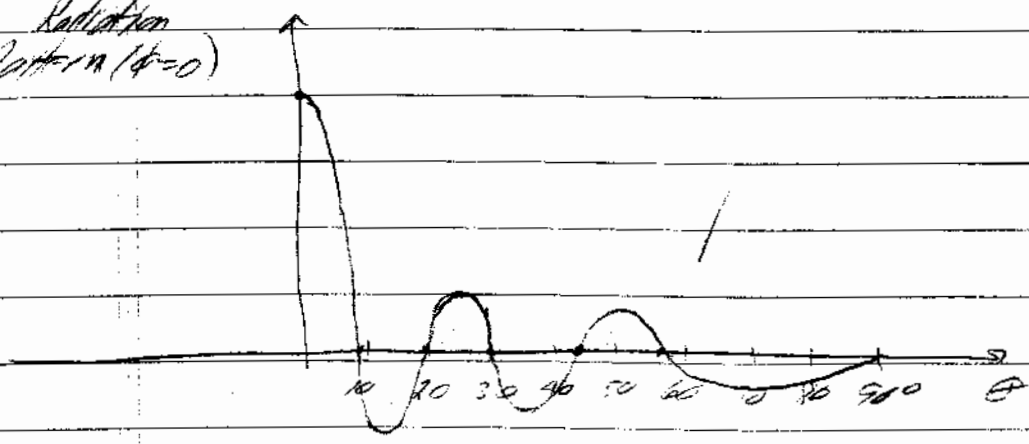
so  $\frac{\beta a}{r} = \frac{2\pi}{\lambda} \cdot \frac{6\lambda}{r} = 6\pi$  which is the visible range of  $U$   
 (i.e.  $0 < U < 6\pi$  for  $0 < \theta < \frac{\pi}{2}$ )



Zeros ( $\sin\theta = 0$ )

U	$\theta$
$\pi$	$9.6^\circ$
$2\pi$	$19.5^\circ$
$3\pi$	$30^\circ$
$4\pi$	$42^\circ$
$5\pi$	$56^\circ$
$6\pi$	$90^\circ$

Radiation Pattern ( $\phi = 0$ )





Homework 12 (page 2)

11-26 (continued) beam width

From table 11-1

$$\theta_{\text{half-power}} \approx \frac{50^\circ}{6} = \underline{\underline{8.33^\circ}}$$

First sidelobe level down 13.2 dB

11-29

5

11-30

4