

1-2 a) $\vec{A} + \vec{B} + \vec{C} = 5\vec{a}_x + 3\vec{a}_y - 9\vec{a}_z$ \leftarrow

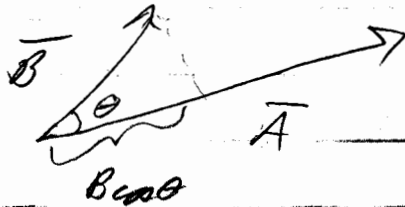
b) $|\vec{A}| = \sqrt{25+9+16} = 7.07$ \leftarrow

$|\vec{D}| = \sqrt{25+25+1} = 7.14$ \leftarrow

c) $2\vec{A} - \vec{C} = 10\vec{a}_x + 6\vec{a}_y + 14\vec{a}_z$ \leftarrow

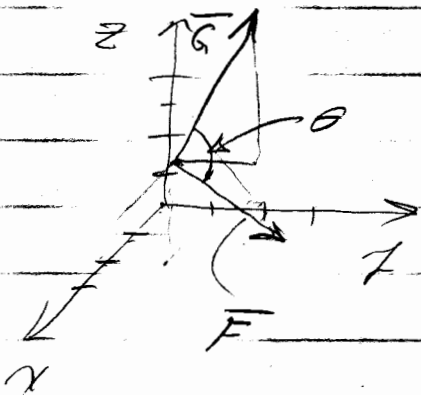
$|\vec{E}| = \sqrt{10^2 + 6^2 + 14^2} = 18.22$ \leftarrow

1-8



$$\vec{A} \cdot \vec{B} = AB \cos \theta$$

component of B
along A!



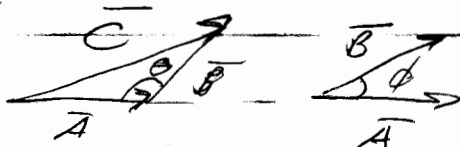
$$\vec{F} \cdot \vec{G} = |\vec{F}| |\vec{G}| \cos \theta = 800$$

$$\therefore \frac{F \cos \theta}{|\vec{G}|} = \frac{800}{53.85} = 14.85$$

$$\cos \theta = \frac{800}{|\vec{F}| |\vec{G}|} = \frac{800}{50 \times 53.85} = 0.2971$$

$$\therefore \theta = 72.71^\circ \leftarrow$$

1-11

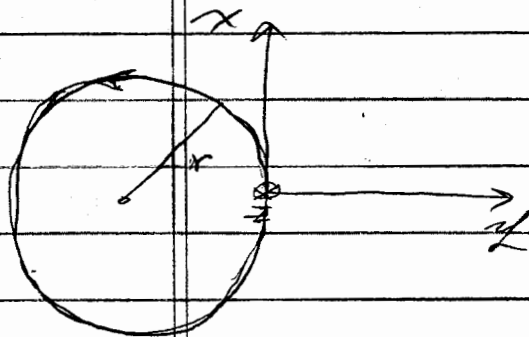


$$\vec{A} \cdot \vec{B} = AB \cos \phi \quad \theta = 180^\circ - \phi$$

$$C^2 = \vec{C} \cdot \vec{C} = (\vec{A} + \vec{B}) \cdot (\vec{A} + \vec{B}) = A^2 + B^2 + 2AB \cos \phi$$

$$\text{or } C^2 = A^2 + B^2 + 2AB \cos(180^\circ - \phi) = \boxed{A^2 + B^2 - 2AB \cos \phi} \leftarrow$$

1-25 $q = -e$, $\vec{u} = 10^5 \hat{a}_x$, $\vec{B} = 10^{-4} \hat{a}_z$



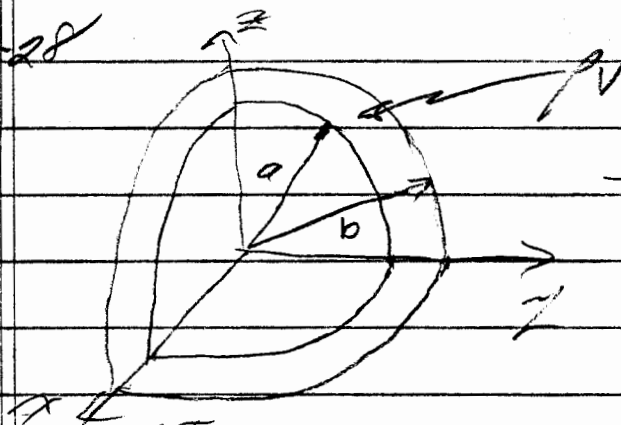
$$\vec{F} = q(\vec{E} + \vec{u} \times \vec{B})$$

Constant force normal to velocity will produce a circular trajectory with $r = \frac{mv^2}{F}$

$$\therefore r = \frac{9.1 \times 10^{-31} \times 10^{10}}{1.6 \times 10^{-19} \times 10^5 \times 10^{-4}} = 5.69 \times 10^{-3} \text{ m}$$

for no deflection $\vec{E} = -\vec{u} \times \vec{B} = -10^5 \hat{a}_x \times 10^{-4} \hat{a}_z = 10 \hat{a}_y$

1-28



$$\oint \epsilon_0 \vec{E} \cdot d\vec{s} = \int \rho_v dV$$

$\vec{E} = E_r(r) \hat{a}_r$ from symmetry

for $r < a$ $\int \rho_v dV = 0 \therefore E = 0$

$$a \leq r \leq b \quad \int_{\phi=0}^{2\pi} \int_{\theta=0}^{\pi} \epsilon_0 E_r \hat{a}_r \cdot r^2 \sin\theta d\theta d\phi = \int_{r=a}^r \int_{\phi=0}^{2\pi} \int_{\theta=0}^{\pi} \rho_v r^2 \sin\theta d\theta d\phi dr$$

$$\therefore \epsilon_0 E_r 4\pi r^2 = \rho_v 4\pi \frac{r^3 - a^3}{3} \quad \therefore E_r = \frac{\rho_v}{\epsilon_0 r^2} \left[\frac{r^3 - a^3}{3} \right]$$

for $r > b$ right hand side becomes $\int_{r=a}^b$ so:

$$E_r = \frac{\rho_v}{\epsilon_0 r^2} \left[\frac{b^3 - a^3}{3} \right]$$

1.29 For $r < a$ $\rho_v = \rho_0(1+kr)$

$$Q = \int_0^a \int_0^{2\pi} \int_0^\pi \rho_0(1+kr) r^2 \sin\theta d\theta d\phi dr = 4\pi\rho_0 \left\{ \frac{a^3}{3} + k \frac{a^4}{4} \right\}$$

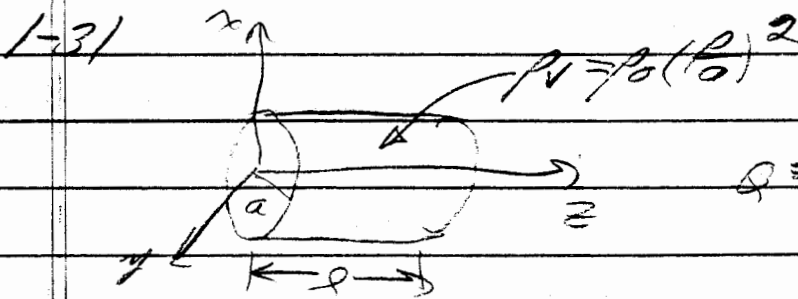
$$Q=0 \text{ if } k = -\frac{a^3}{3} \cdot \frac{4}{a^4} = -\frac{4}{3a}$$

For a spherically symmetric charge distribution
 $\vec{E} = E_r(r) \vec{a}_r$ $\oint \epsilon_0 \vec{E} \cdot d\vec{s}$ over a spherical surface for $r > a$ $\epsilon_0 E_r 4\pi r^2 = Q = 0 \therefore E = 0$

For $r < a$ $\epsilon_0 E_r 4\pi r^2 = \int_0^r \int_0^{2\pi} \int_0^\pi \rho_0(1 - \frac{4r}{3a}) r^2 \sin\theta d\theta d\phi dr$

$$= 4\pi\rho_0 \left[\frac{r^3}{3} - \frac{4r^4}{3a} \right]$$

$$\therefore E_r = \frac{\rho_0}{\epsilon_0} \left[\frac{r}{3} - \frac{4r^2}{3a} \right]$$



$$Q = \int_{z=0}^L \int_{\phi=0}^{2\pi} \int_{\rho=0}^a \rho_0 \left(\frac{\rho}{a}\right)^2 d\rho d\phi dz$$

a) or $Q = 2\pi L \frac{\rho_0}{a^2} \cdot \frac{a^4}{4} = \frac{\pi \rho_0 a^2 L}{2}$

b) For $\rho > a$ $\epsilon_0 E_p 2\pi \rho L = \frac{\pi \rho_0 a^2 L}{2}$

$$\text{or } E_p = \frac{\rho_0 a^2}{4\epsilon_0 \rho} = \frac{\rho_0 a^2}{2\pi \epsilon_0 \rho}$$

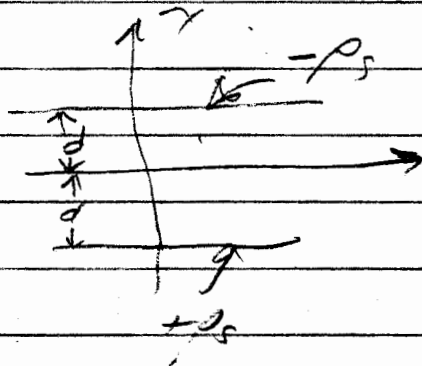
1-31 c) $\rho < a$

$$\int_{z=0}^{\infty} \int_{\phi=0}^{2\pi} \int_{\rho=0}^{\rho} \epsilon_0 E_{\rho} \rho d\phi dz = \int_{z=0}^{\rho} \int_{\phi=0}^{2\pi} \int_{\rho=0}^{\rho} \rho_0 \left(\frac{\rho}{a}\right)^2 \rho \rho d\phi dz$$

$$\epsilon_0 E_{\rho} \rho = \frac{\rho_0 \rho^3}{4a^2}$$

$$E_{\rho} = \frac{\rho_0 \rho}{4\epsilon_0 a^2} \quad \leftarrow$$

1-32



a) between the plates
both charges produce an E_x in the positive x direction so $E_x = \frac{\rho_s}{\epsilon_0}$

for $x > d$ or $x < -d$ the fields cancel
i.e. $E_x = 0$

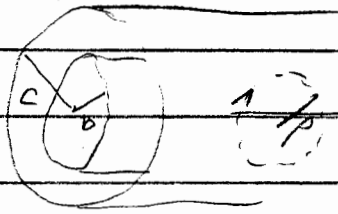
b) both plates have positive charge then

$$\text{for } x > d \quad E_x = \frac{\rho_s}{\epsilon_0}$$

$$x < -d \quad E_x = -\frac{\rho_s}{\epsilon_0}$$

$$-d < x < d \quad E_x = 0$$

1.33



$\vec{J} = \frac{I}{\text{cross sectional area}}$

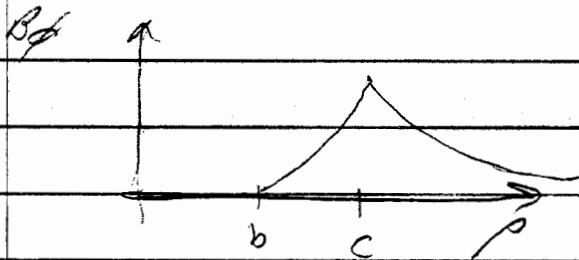
a) $\therefore \vec{J} = \frac{I}{\pi(c^2 - b^2)} \hat{z}$

for $\rho < b$ $\int \frac{b}{\mu_0} \vec{J} \cdot d\vec{l} = 0 = B_\phi \frac{2\pi\rho}{\mu_0} \Rightarrow B_\phi = 0$

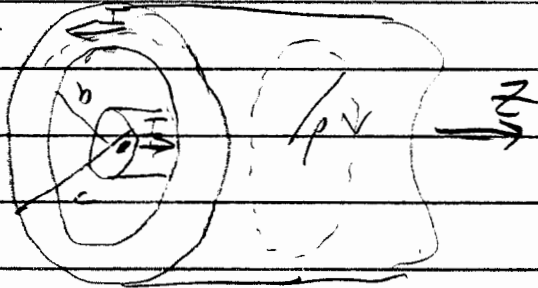
for $b < \rho < c$ $\frac{2\pi\rho B_\phi}{\mu_0} = \int_{\phi=0}^{2\pi} \int_{p=b}^{\rho} \frac{I}{\pi(c^2 - b^2)} \rho db dp = \frac{I 2\pi}{2\pi(c^2 - b^2)} (\rho^2 - b^2)$

$\therefore B_\phi = \frac{\mu_0 I}{2\pi} \cdot \frac{(\rho^2 - b^2)}{(c^2 - b^2)}$

for $\rho > c$ $B_\phi = \frac{\mu_0 I}{2\pi}$ same as line current along z axis



1.34



a) for $\rho < a$; $\vec{J} = \frac{I}{\pi a^2} \hat{z}$

for $b < \rho < c$ $\vec{J} = \frac{-I}{\pi(c^2 - b^2)} \hat{z}$

from $\vec{J} = \frac{I}{\text{area}}$

b) for $\rho < a$ $\frac{2\pi\rho B_\phi}{\mu_0} = \int_{\phi=0}^{2\pi} \int_{p=0}^{\rho} \frac{I}{\pi a^2} p db dp = \frac{2\pi I}{2\pi a^2} \rho^2$

or $B_\phi = \frac{\mu_0 I \rho}{2\pi a^2}$

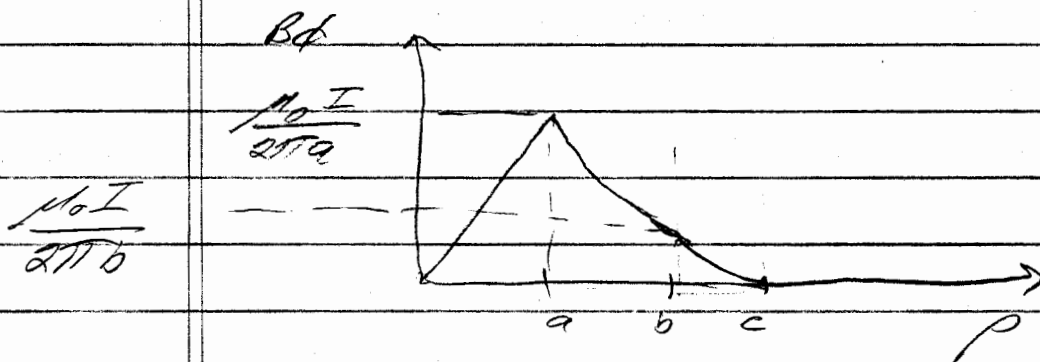
for $a < \rho < b$ $\frac{2\pi\rho B_\phi}{\mu_0} = I$ or $B_\phi = \frac{\mu_0 I}{2\pi\rho}$

$$\text{For } b \leq \rho < c; \quad \frac{2\pi\rho B_\phi}{\mu_0} = -\int_0^{2\pi} \int_b^\rho \frac{I}{\pi(c^2 - b^2)} \rho d\phi d\rho + I$$

$$B_\phi = \frac{\mu_0}{2\pi\rho} \left\{ I - \frac{2\pi I}{2\pi(c^2 - b^2)} (\rho^2 - b^2) \right\} = \frac{\mu_0 I}{2\pi\rho} \left\{ \frac{c^2 - \rho^2}{c^2 - b^2} \right\} \quad \leftarrow$$

For $\rho > c$ $B_\phi = 0$ (no current through circular contour) \leftarrow

c) $a = 3\text{mm}$, $b = 6\text{mm}$, $c = 8\text{mm}$, $I = 100\text{ Amperes}$



$$B_\phi(\rho=a) = \frac{2 \times 10^{-7} \times 10^2}{2\pi \times 3 \times 10^{-3}} = 0.667 \times 10^{-2} \quad \leftarrow$$

$$B_\phi(\rho=b) = \frac{1}{2} \text{ of above } = 0.333 \times 10^{-2} \quad \leftarrow$$

$$\frac{|J|}{\rho < a} = \frac{100}{\pi \times 9 \times 10^{-6}} = 3.53 \times 10^6 \text{ A/m}^2 \quad \leftarrow$$

$$\frac{|J|}{b < \rho < c} = \frac{+100}{\pi(64 \times 10^{-6} - 36 \times 10^{-6})} = \frac{10^2}{\pi \times 28 \times 10^{-6}} = 1.13 \times 10^6 \frac{\text{A}}{\text{m}^2} \quad \leftarrow$$

1-35 for $p < b$ B_{ϕ} only due to current in center conductor which is Example 1-15

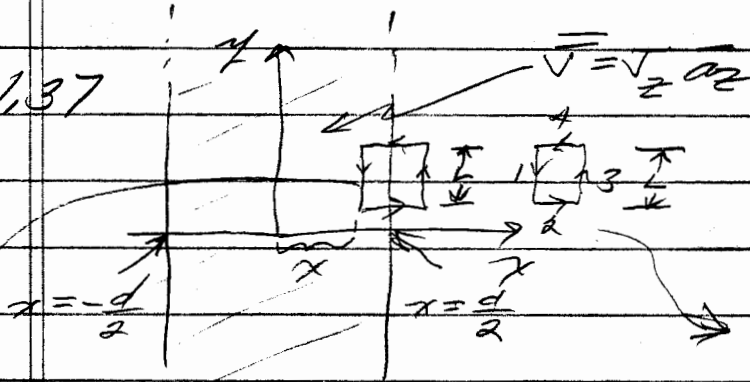
for $b < p < c$ superposition gives

$$B_{\phi} = \frac{\mu_0 I}{2\pi p} - \frac{\mu_0 I}{2\pi p} \cdot \frac{p^2 - b^2}{c^2 - b^2} = \frac{\mu_0 I}{2\pi p} \left\{ \frac{c^2 - p^2}{c^2 - b^2} \right\} \quad \text{QED}$$

for $p > c$

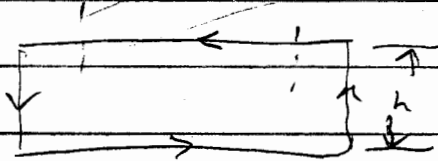
$$B_{\phi} = \frac{\mu_0 I}{2\pi p} - \frac{\mu_0 I}{2\pi p} = 0 \quad \text{! } \sigma$$

1.37



Relating back to line currents we see that there is only a B_y component

$$\oint \frac{\vec{B}}{\mu_0} \cdot d\vec{l} = 0 = (-B_y L + B_y L) \frac{1}{\mu_0}$$



\therefore outside of current $B_y = \text{constant}$

for this contour $\frac{2 B_y x}{\mu_0} = dx J_2$; $B_y = \frac{\mu_0 J_2}{2} x \quad x > \frac{d}{2}$

$$\frac{\mu_0 J_2 x}{\mu_0 2} - \frac{B_y(x) x}{\mu_0} = J_2 \left(\frac{d}{2} - x\right) x$$

$$B_y = -\mu_0 J_2 \left(\frac{d}{2} - x\right) + \frac{d J_2 \mu_0}{2} = \mu_0 J_2 x \quad 0 < x < \frac{d}{2}$$

negative of these answers for $x < 0$

Q.17 $E_r = \frac{\rho_0}{\epsilon_0} \left(\frac{r}{3} - \frac{r^2}{3a} \right)$

$$\nabla \cdot E_r = \frac{1}{r^2} \frac{d}{dr} \left[\frac{\rho_0}{\epsilon_0} \left(\frac{r^3}{3} - \frac{r^4}{3a} \right) \right] = \frac{\rho_0}{r^2 \epsilon_0} \left(r - \frac{4r^3}{3a} \right)$$

$$\nabla \cdot E_r = \frac{\rho_0}{\epsilon_0} \left(1 - \frac{4r}{3a} \right) = \frac{\rho_0}{\epsilon_0}$$

2.41 $\hat{E}_x^+ = 1885 e^{-j\beta_0 z}$; $f = 100 \text{ MHz}$

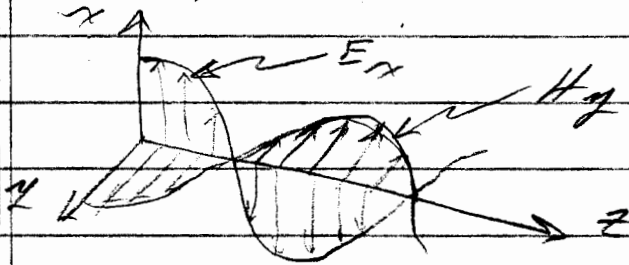
- a) Magnitude = 1885 V/m
 Traveling in $+\hat{a}_z$ direction
 Linear \hat{a}_x polarization

b) $E_x^+(z,t) = \Re\{E_x^+ e^{j2\pi \times 10^8 t}\} = 1885 \cos(2\pi \times 10^8 t - \beta_0 z)$
 where $\beta_0 = \omega \sqrt{\mu_0 \epsilon_0}$; $\lambda = \frac{2\pi}{\beta_0} = \frac{3 \times 10^8}{10^8} = 3 \text{ m}$

c) $\hat{H}_y^+ = \frac{1885}{377} e^{-j\beta_0 z} = 5 e^{-j\beta_0 z}$

$B_y^+ = \mu_0 H_y^+ = 20\pi \times 10^{-7} e^{-j\beta_0 z}$

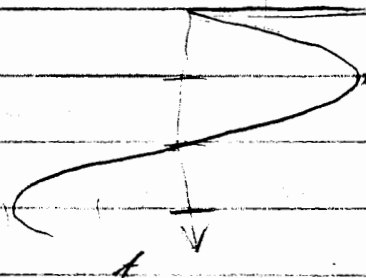
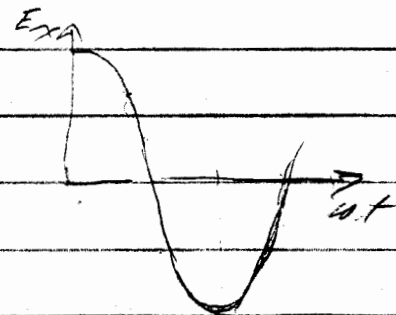
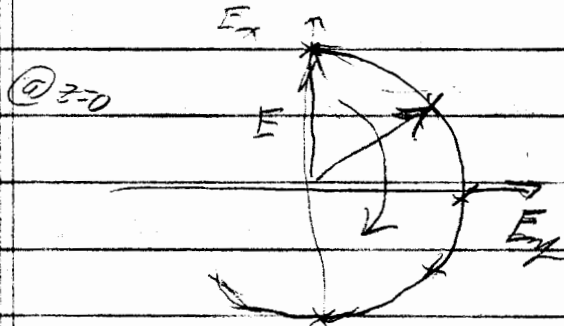
$H_y^+(z,t) = 5 \cos(2\pi \times 10^8 t - \beta_0 z)$



2.46 $\hat{E}(z) = 500 e^{-j\beta_0 z} (\hat{a}_x - j\hat{a}_y)$

$E(z,t) = 500 \cos(\omega t - \beta_0 z) \hat{a}_x + 500 \sin(\omega t - \beta_0 z) \hat{a}_y$

or @ $z=0$ $E(z,t) = 500 \cos(\omega t) \hat{a}_x + 500 \sin(\omega t) \hat{a}_y$



GW circular

$\hat{H}_z(z) = \frac{500}{\mu_0} e^{-j\beta_0 z} (\hat{a}_y + j\hat{a}_x)$

$$3.1 \quad n = 10^{29} \text{ electrons/m}^3 \quad ; \quad v = 5.8 \times 10^7 \text{ m/s/m}$$

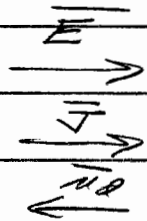
$$a) \quad \mu_e = \frac{q \tau_e}{m} \quad ; \quad \sigma = \frac{n q^2}{m} \tau_e$$

$$\text{so } \mu_e = \sigma \left(\frac{1}{n q} \right) = \frac{5.8 \times 10^7}{10^{29} \times 1.6 \times 10^{-19}} = \boxed{3.625 \times 10^{-3}}$$

$$b) \quad \text{charge density} = -10^{29} \frac{\text{elec}}{\text{m}^3} \times \frac{1.6 \times 10^{-19} \text{ C}}{\text{elec}} \times \frac{1 \text{ m}^3}{10^9 \text{ mm}^3} = \boxed{-16 \frac{\text{C}}{\text{mm}^3}}$$

$$c) \quad \vec{E} = 1 \vec{a}_x \quad ; \quad \vec{v}_d = -\mu_e \vec{E} = -3.625 \times 10^{-3} \times 1 \vec{a}_x = \boxed{-3.625 \times 10^{-3} \frac{\text{m}}{\text{sec}}}$$

$$\vec{J} = \sigma \vec{E} = 5.8 \times 10^7 \vec{a}_x \text{ A/m}^2$$



} negative charge on electrons so $\vec{v}_d + \vec{J}$ in opposite directions

3-3 He 10^{25} atoms/m³, $\chi_e = 1.5 \times 10^{-4}$, $E = 10^3$

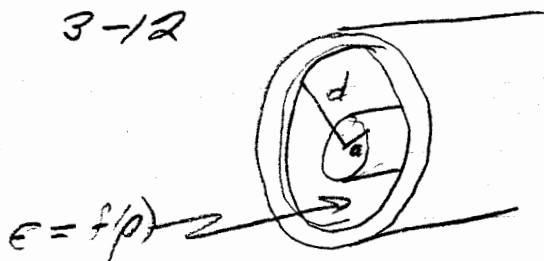
$$\vec{D} = \epsilon_0 \vec{E} + \vec{P} \quad \vec{P} = \epsilon_0 \chi_e \vec{E} \quad \therefore \vec{D} = \epsilon_0 (1 + \chi_e) \vec{E}$$

a) $P = \epsilon_0 \chi_e E = \frac{10^{-9}}{360} \times 1.5 \times 10^{-4} \times 10^3 = 0.0133 \times 10^{-10} = \underline{\underline{1.33 \times 10^{-12}}}$

b) $\rho_+ = 2 \times 10^{25} \times 1.6 \times 10^{-19} = 3.2 \times 10^6 \text{ C/m}^3$; $P = \rho_+ d_{\text{ave}}$
 $\therefore d_{\text{ave}} = \frac{1.33 \times 10^{-12}}{3.2 \times 10^6} = \underline{\underline{0.41 \times 10^{-18} \text{ m}}}$

c) $\epsilon_r = 1 + \chi_e = \underline{\underline{1.00015}}$

3-12



a) $\oint \vec{D} \cdot d\vec{s} = \int \rho_v dV$ use circular cylindrical con
 $a < \rho < d$

$$\int_{\phi=0}^{2\pi} \int_{z=0}^l \rho_p \rho d\phi dz = Q$$

$$2\pi \rho \rho_p l = Q$$

so $E_p = \frac{Q}{2\pi \epsilon \rho l}$ constant if $\epsilon = \frac{K}{\rho}$
 problem ask for $\epsilon = \epsilon_r @ \rho = d \quad \therefore \boxed{\epsilon = \frac{\epsilon_r d}{\rho}}$

so $E_p = \frac{Q \rho}{2\pi \epsilon_r \epsilon_0 d l \rho} = \boxed{\frac{Q}{2\pi \epsilon_r \epsilon_0 d l}}$

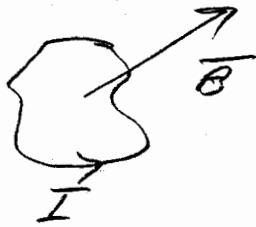
b) $D_p = \epsilon_0 E_p + P_p$ so $P_p = D_p - \epsilon_0 E_p = \frac{Q}{2\pi \rho l} - \frac{Q \epsilon_0}{2\pi \epsilon_r d l}$

$\boxed{P_p = \frac{Q}{2\pi l} \left(\frac{1}{\rho} - \frac{\epsilon_0}{\epsilon_r d} \right)}$

$\rho_p = -\nabla \cdot \vec{P} = + \frac{1}{\rho} \frac{\partial}{\partial \rho} \left(\frac{\rho Q \epsilon_0}{2\pi \epsilon_r d} \right) = \boxed{\frac{Q \epsilon_0}{2\pi \epsilon_r d \rho}}$

c) use layers that approximate the $\frac{\epsilon_r d}{\rho}$ variation in ϵ_r .

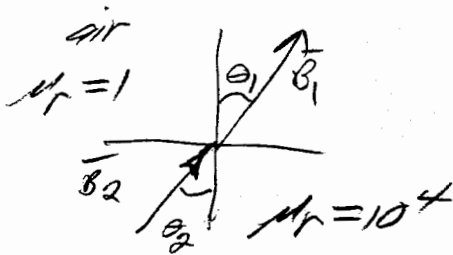
3.16



$$\vec{F} = \oint d\vec{q} \vec{r} \times \vec{B}$$

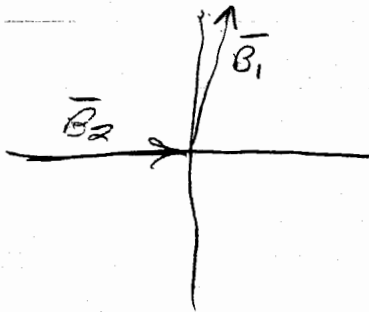
$$\vec{F} = \oint I \vec{dl} \times \vec{B} = -I \oint \vec{B} \times d\vec{l}$$

$$\vec{F} = -I \vec{B} \times \oint d\vec{l} \equiv 0 \quad \leftarrow$$

3.25 $H_1 = H_2$ and $B_1 = B_2$ 

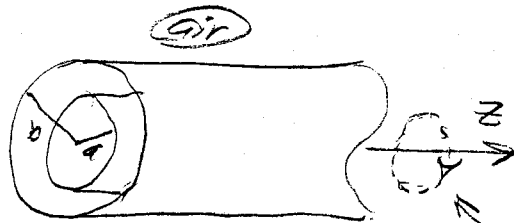
$$\tan \theta_2 = \frac{\mu_2}{\mu_1} \tan \theta_1 \quad (3.76)$$

$$\text{or } \theta_1 = \tan^{-1} [10^{-4} \tan \theta_2]$$



θ_2	θ_1
0	0
45°	$5.7 \times 10^{-3}^\circ$
89°	0.328°
89.9°	3.27°
89.9675	10°

3-28



I carried in conductor of radius a ($\mu = \mu_0$)
for $a < \rho < b$ $\mu = \mu_r$

$\oint \vec{H} \cdot d\vec{l} = \int \vec{J} \cdot d\vec{s}$ integrate around circular contour of radius ρ .

a) for $\rho < a$ $H_\phi 2\pi\rho = \frac{I}{\pi a^2} \pi \rho^2$ or $H_\phi = \frac{I\rho}{2\pi a^2}$
 $B_\phi = \frac{\mu_0 I\rho}{2\pi a^2}$

for $a < \rho < b$ $H_\phi 2\pi\rho = I$
 $H_\phi = \frac{I}{2\pi\rho}$
 $B_\phi = \frac{\mu_r I}{2\pi\rho} = \frac{\mu_r \mu_0 I}{2\pi\rho}$

for $\rho > b$
 $H_\phi = \frac{I}{2\pi\rho}$
 $B_\phi = \frac{\mu_0 I}{2\pi\rho}$

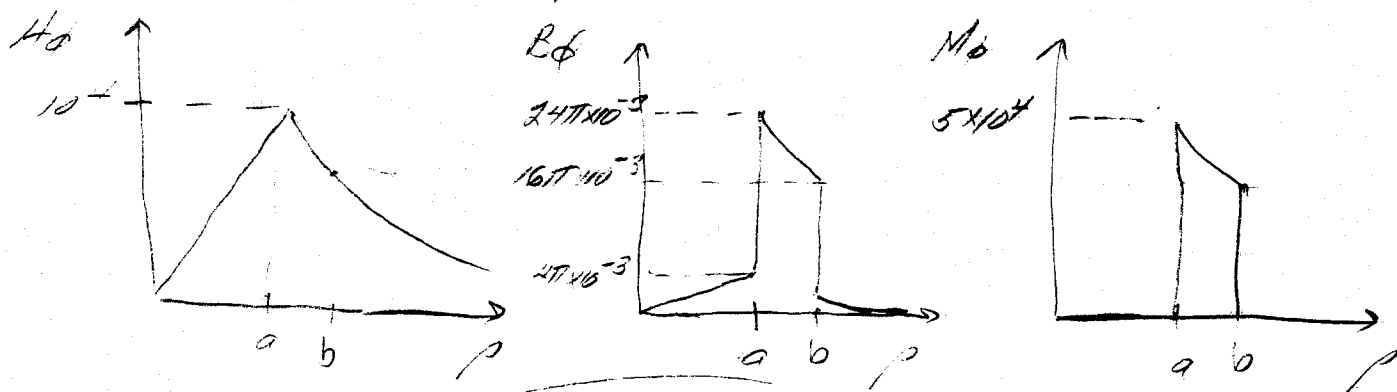
b) $\vec{M} = \frac{\vec{B}}{\mu_0} - \vec{H} = \left(\frac{\mu_r I}{2\pi\rho} - \frac{I}{2\pi\rho} \right) \hat{\phi} = \frac{I}{2\pi\rho} (\mu_r - 1) \hat{\phi}$

$\left\{ \begin{array}{l} H_\phi \text{ is continuous across each boundary (} H_{\text{tang}} \text{ is continuous)} \\ B_\phi \text{ is discontinuous} \end{array} \right.$

@ $\rho = a$ $H_\phi = \frac{628}{2\pi \times 10^{-2}} = 10^4$; $B_\phi = 24\pi \times 10^{-3}$ ($\rho = a^+$)
 $B_\phi = 4\pi \times 10^{-3}$ ($\rho = a^-$)

$\rho = b$ $H_\phi = \frac{628}{2\pi \times 15 \times 10^{-2}} = \frac{2}{3} \times 10^4$; $B_\phi(\rho = b^-) = 4\pi \times 10^{-7} \times 6 \times \frac{2}{3} \times 10^4 = 16\pi \times 10^{-3}$
 $B_\phi(\rho = b^+) = 4\pi \times 10^{-7} \times \frac{2}{3} \times 10^4 = \frac{8}{3}\pi \times 10^{-3}$

$M = 0$ for $\rho < a$ and $\rho > b$ $M = 5H$ for $a < \rho < b$



3-28 continued

$$\bar{n} \times (\bar{M}_1 - \bar{M}_2) = \bar{J}_{sm}$$

$$\bar{J}_{sm} = \nabla \times \bar{M}$$

$$\bar{J}_{sm} = \bar{a}_\rho \left(-\frac{\partial M_\phi}{\partial z} \right) + \bar{a}_z \left(\frac{1}{\rho} \frac{\partial}{\partial \rho} (\rho M_\theta) \right) = 0$$

$$\bar{J}_{sm}(\rho=a) = \bar{a}_\rho \times \bar{M} = 5 \times 10^4 \bar{a}_z$$

$$\bar{J}_{sm}(\rho=b) = -\bar{a}_\rho \times \bar{M} = -\frac{10}{3} \times 10^4 \bar{a}_z$$

3.29

Region 1 $\epsilon = \epsilon_0$ 

$$\bar{E}_1 = -15\bar{a}_x + 20\bar{a}_y + 30\bar{a}_z$$

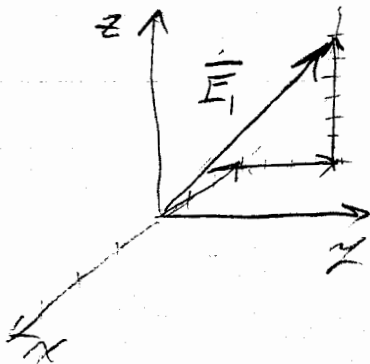
$$\left\{ \begin{array}{l} E_{tng1} = E_{tng2} \\ D_{norm1} = D_{norm2} \end{array} \right.$$

Region 2 $\epsilon = 4\epsilon_0$

$$a) \bar{E}_2 = -15\bar{a}_x + 20\bar{a}_y + \frac{15}{2}\bar{a}_z \leftarrow$$

$$\bar{D}_1 = \epsilon_0 \bar{E}_1$$

$$\bar{D}_2 = 4\epsilon_0 \bar{E}_2$$



$$b) \bar{n} \cdot \bar{E}_1 = |\bar{E}_1| \cos \theta_1 = 30$$

$$\therefore \theta_1 = \cos^{-1} \frac{30}{\sqrt{15^2 + 20^2 + 30^2}} = \boxed{39.8^\circ} \leftarrow$$

$$\theta_2 = \cos^{-1} \frac{15/2}{\sqrt{15^2 + 20^2 + 7.5^2}} = \boxed{73.3^\circ} \leftarrow$$

$$\text{ck: } \tan \theta_2 = \frac{\epsilon_2}{\epsilon_1} \tan \theta_1$$

$$3.333 = 4 \times 0.833 = 3.33 \quad !$$

$$3.33 \quad \alpha = \frac{\omega \sqrt{\mu \epsilon}}{\sqrt{2}} \left[\sqrt{1 + \left(\frac{\sigma}{\omega \epsilon}\right)^2} - 1 \right]^{1/2}$$

$$\beta = \frac{\omega \sqrt{\mu \epsilon}}{\sqrt{2}} \left[\sqrt{1 + \left(\frac{\sigma}{\omega \epsilon}\right)^2} + 1 \right]^{1/2}$$

$$\eta = \sqrt{\frac{\mu}{\epsilon - j\frac{\sigma}{\omega}}}$$

For $\sigma = 0$, $\mu = \mu_0$, & $\epsilon = \epsilon_0$ this gives:

$$\alpha = 0 \quad ; \quad \beta = \omega \sqrt{\mu_0 \epsilon_0} \quad ; \quad \eta = \sqrt{\frac{\mu_0}{\epsilon_0}} \quad \leftarrow$$

3.38 $E_m^+ = 1$ @ $z = 0$ sea water $\epsilon_r = 81$, $\sigma = 4$
 $f = 10^4$
 $\frac{\sigma}{\omega \epsilon} = \frac{4 \times 36\pi}{2\pi \times 10^4 \times 10^{-9}} = 72 \times 10^5 \quad \therefore \text{good conductor}$

$$\alpha = \beta = \frac{\omega \sqrt{\mu \epsilon}}{\sqrt{2}} \sqrt{\frac{\sigma}{\omega \epsilon}} = \sqrt{\frac{\omega \sigma \mu}{2}} = \sqrt{\frac{2\pi \times 10^4 \times 4 \times 4\pi \times 10^{-7}}{2}} = 4\pi \times 0.0316 = 0.397$$

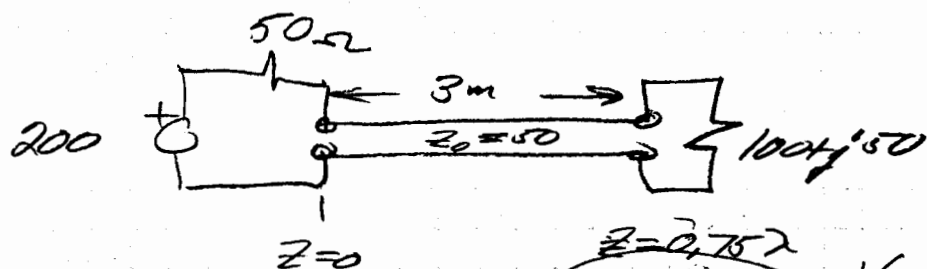
$$\sigma \alpha z = 0.05 \quad ; \quad -\alpha z = \ln 0.05 \quad ; \quad z = -\frac{\ln 0.05}{\alpha} = 7.15 \text{ m}$$

$f = 10^3$
 $\frac{\sigma}{\omega \epsilon} = 72 \times 10^6 \quad \therefore \text{good conductor}$

$$\alpha = \beta = \sqrt{\frac{2\pi \times 10^3 \times 4 \times 4\pi \times 10^{-7}}{2}} = 4\pi \times 10^{-2} = 0.1257$$

$$z = -\frac{\ln 0.05}{0.1257} = 23.8 \text{ m}$$

RF communication in sea water is only good @ very low frequencies ... and even then only over very short distances.



$f = 50 \text{ MHz}$

$\epsilon_r = 2.25$

$v_p = 3 \times 10^8 \frac{1}{\sqrt{2.25}} = 2 \times 10^8 \text{ m/sec} \checkmark \therefore \text{length of line} = \frac{3 \times 10^{-7}}{2 \times 10^8} = 1.5 \times 10^{-1} \text{ m}$

$\lambda = \frac{2 \times 10^8}{0.5 \times 10^8} = 4 \text{ m} \checkmark$

$\Gamma_{\text{load}} = \frac{Z_L - Z_0}{Z_L + Z_0} = \frac{50 + j50}{150 + j50} = 0.4 + j0.2 = 0.4472 \angle 26.57^\circ \checkmark$

$\Gamma_{\text{in}} = \Gamma_{\text{load}} e^{-2\beta l} = (0.4 + j0.2) e^{-j2 \frac{2\pi}{\lambda} \cdot \frac{3\lambda}{4}} = -(0.4 + j0.2) \checkmark$

\therefore approximately 45% voltage reflection (20% power reflection)

$Z_{\text{in}} = 50 \frac{1 + \Gamma_{\text{in}}}{1 - \Gamma_{\text{in}}} = 50 \frac{0.6 - j0.2}{1.4 + j0.2} = 20 - j10 \checkmark$

$\hat{I}_{\text{in}} = \frac{200}{50 + Z_{\text{in}}} = \frac{200}{70 - j10} = 2.828 \angle 8.13^\circ \checkmark$

$P_{\text{in}} = \frac{1}{2} |\hat{I}_{\text{in}}|^2 R_{\text{in}} = \frac{1}{2} (2.828)^2 20 = 79.98 \text{ watts} \checkmark$

$\hat{I} = \hat{I}_{\text{in}} e^{j\beta z} [1 + \Gamma(z)] \therefore \hat{I}_{\text{in}}^+ = \hat{I}_{\text{in}} [1 - \Gamma_{\text{in}}]^{-1}$

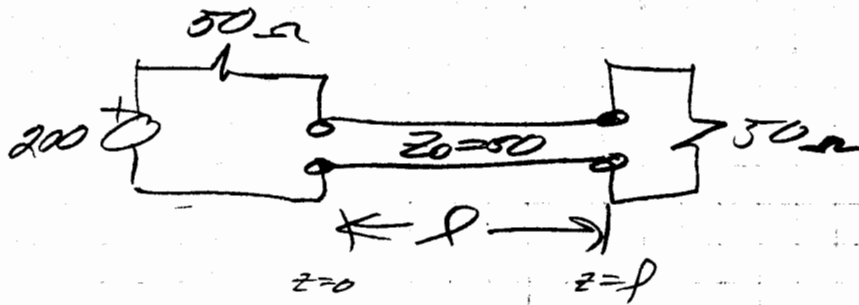
and $I_{\text{load}} = \hat{I}_{\text{in}}^+ e^{-j\beta l} [1 - \Gamma_{\text{load}}] = \frac{\hat{I}_{\text{in}} e^{-j\frac{13\pi}{2}}}{1 - \Gamma_{\text{in}}} [1 + \Gamma_{\text{load}}]$
 $= 2.828 \angle 8.13^\circ \frac{0.6 - j0.2}{1.4 + j0.2}$

or $I_{\text{load}} = 1.2647 \angle 7.156^\circ \checkmark$

so $P_{\text{load}} = \frac{1}{2} (1.2647)^2 100 = 79.97 \text{ watts} \checkmark$

(11)

10-3



$$f = 30 \text{ MHz}$$

$$\rho = 3 \mu$$

$$\epsilon_r = 2.25$$

$$\Gamma_{\text{load}} = 0 \quad \therefore \Gamma(z) = 0 \text{ everywhere!}$$

$$Z(z) = 50 = Z_0 \frac{1 + \Gamma}{1 - \Gamma} \quad \checkmark$$

$$\begin{aligned} \hat{V} &= \hat{V}_m^+ e^{-j\beta z} \\ \hat{I} &= \frac{\hat{V}_m^+}{Z_0} e^{-j\beta z} \end{aligned} \quad \left. \begin{aligned} &= V_m^+ \\ &= \frac{V^+}{Z_0} \end{aligned} \right\} \text{when } z=0, \lambda, 2\lambda, \dots$$

$$\hat{I}_m^+ = \hat{I}_{in} = \frac{200}{100} = 2 \text{ A}; \quad \hat{V}_{in} = 100 = \hat{V}_m^+ \quad \checkmark$$

$$P_{in} = \frac{1}{2} \text{Re} \{ \hat{V}_{in} \hat{I}_m^{*+} \} = \underline{100 \text{ watts}} \quad \checkmark$$

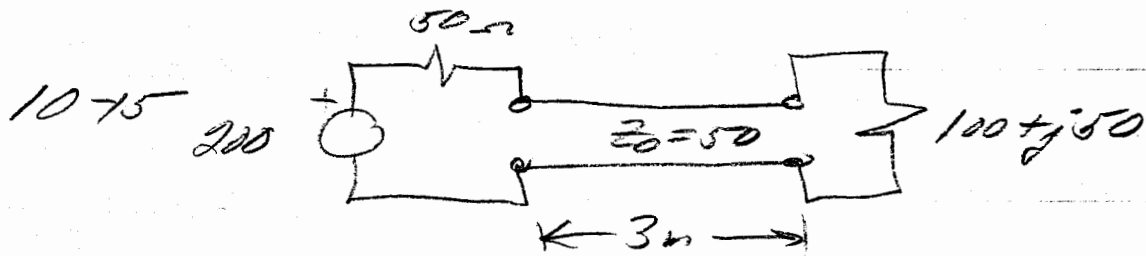
$$\begin{aligned} \hat{V}(z) &= 100 e^{-j \frac{2\pi}{\lambda} z} \\ \hat{I}(z) &= 2 e^{-j \frac{2\pi}{\lambda} z} \end{aligned} \quad \checkmark$$

$$\hat{V}_{\text{load}} = 100 e^{-j \frac{2\pi}{\lambda} \cdot \frac{3}{4} \lambda} = 100j \quad \checkmark$$

$$\hat{I}_{\text{load}} = 2j$$

$$\begin{aligned} P_{\text{load}} &= \frac{1}{2} \text{Re} \{ 100j (-2j) \} = 100 \quad \checkmark \\ &= \frac{1}{2} |\hat{I}|^2 Z_0 = 100 \\ &= \frac{1}{2} \frac{|\hat{V}|^2}{50} = 100 \end{aligned} \quad \checkmark$$

⑨



$$\epsilon_r = 2.25 ; f = 50\text{MHz}$$

$$\nu_{\text{phase}} = \frac{3 \times 10^8}{\sqrt{2.25}} = 2 \times 10^8 \quad \therefore \lambda = \frac{2 \times 10^8}{3 \times 10^7} = 4\text{m}$$

$$\text{line length} = \frac{3}{4} \lambda$$

$$\boxed{Z(\ell) = 2 + j1}_{\text{norm}}$$

$$\text{from chart } \boxed{\Gamma(\ell) = 0.45 \angle 26^\circ}$$

$$\lambda \text{ on chart @ input} = 0.213 + 0.25 = 0.463$$

$$\text{from chart } Z_{\text{in}} = 0.41 - j0.2 \quad \text{or} \quad \boxed{Z_{\text{in}} = 205 - j10} \leftarrow$$

$$\boxed{\Gamma(\ell) = 0.45 \angle -2^\circ}$$

IMPEDANCE OR ADMITTANCE COORDINATES

Problem 10-15

Z_0 norm

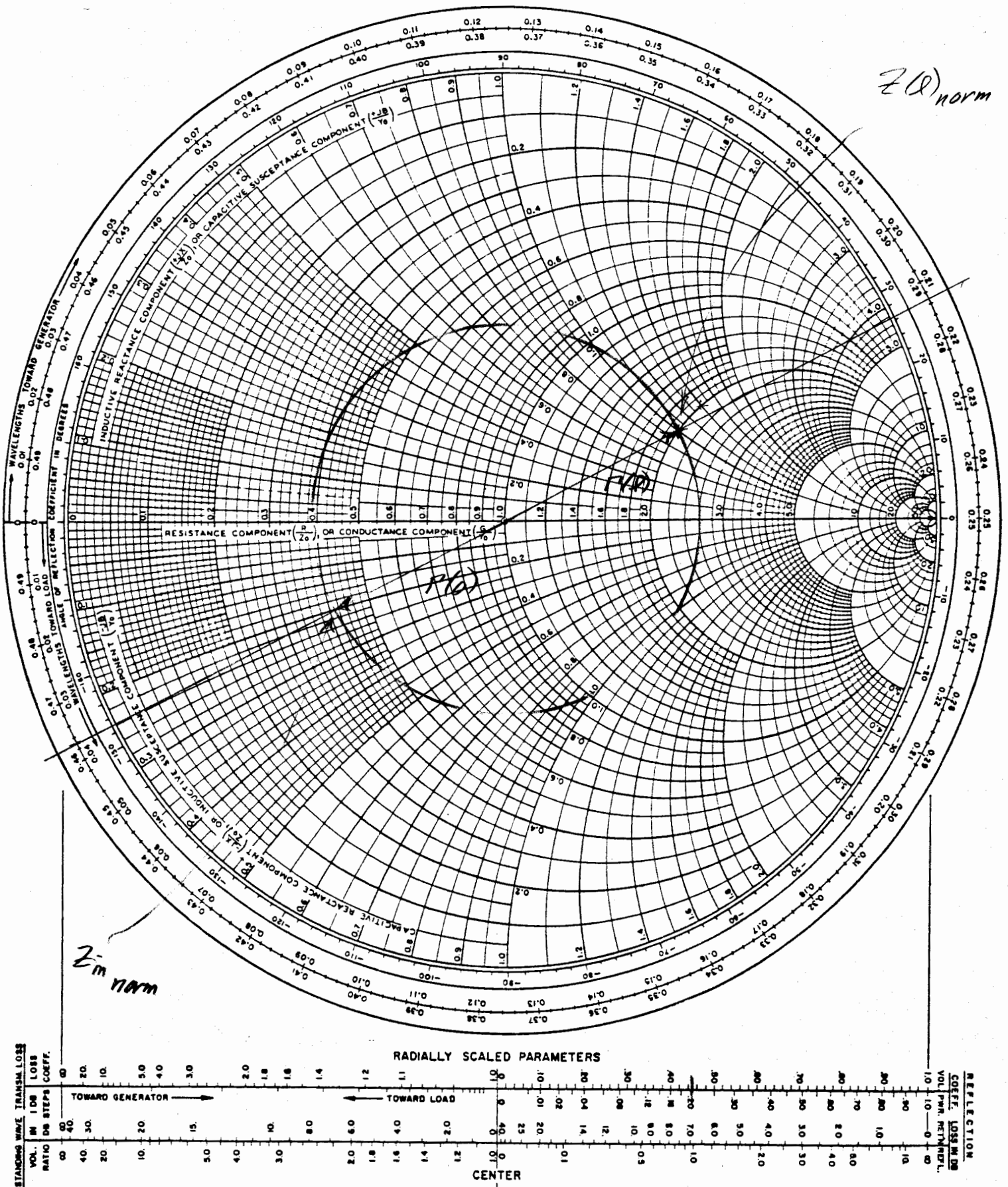
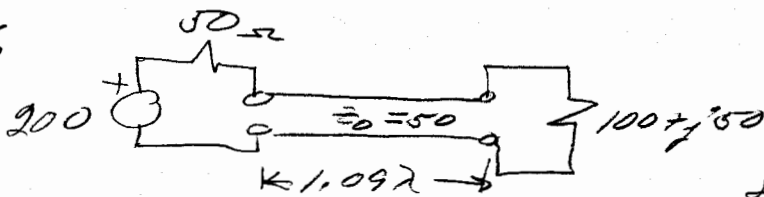


Fig. 9-3. A standard commercially available form of Smith chart graph paper. Copyrighted 1949 by Kay Electric Company, Pine Brook, N. J., and reprinted with their permission.

10.16



$$Z_{L, \text{norm}} = 2 + j1$$

For chart $\lambda = 0.1214 + 0.09 = 0.304\lambda$
rotation

$$\Gamma(\lambda) = 0.455 e^{j26^\circ}$$

$$\Gamma(0) = 0.455 e^{-j239^\circ}$$

$$Z_{in, \text{norm}} = 1.59 - j1.12; \quad Z_{in} = \boxed{79.5 - j56}$$

10.17 same as 10.16 but $\alpha = 0.00197 \text{ Np/m}$; $\ell = 11.5 \text{ m}$

$$e^{-2\alpha\ell} = e^{-2 \times 1.97 \times 10^{-3} \times 11.5} = \boxed{0.956}$$

@ input $|\Gamma| = 0.956 \times 0.455 = 0.435$
rotation not affected

from chart $Z_{in, \text{norm}} = 1.58 - j1.03$; $Z_{in} = \boxed{79 - j51.5}$

10.21 $Z_L = 36 + j20$; $Z_{L, \text{norm}} = 0.72 + j0.4$

$Z_0 = 50 \Omega$

from chart $Y_{L, \text{norm}} = 1.06 - j0.58$

$$\frac{1}{Z_{L, \text{norm}}} = \frac{1}{0.72 + j0.4} = \frac{1}{0.82365 \angle 29.05^\circ} = \boxed{1.06 - j0.59 \text{ QED}}$$

10.23 $Y_{in_2} = G_2 + jB_2$; $Y_{in_3} = G_3 + jB_3$ $\hat{I} = \hat{V} Y$

$$P_{\text{ave}} = \frac{1}{2} \text{Re} \{ \hat{V} \hat{I}^* \} = \frac{1}{2} \text{Re} \{ \hat{V} \hat{V}^* Y^* \} = \frac{1}{2} \text{Re} \{ |\hat{V}|^2 (G - jB) \}$$

so $\frac{P_{\text{ave}_2}}{P_{\text{ave}_3}} = \frac{G_2}{G_3}$ $G_2 = 0.0366$
 $G_3 = 0.012$

$$\frac{1}{2} |\hat{V}|^2 (G_2 + G_3) = 8.5 = \frac{1}{2} |\hat{V}|^2 G_2 \left(1 + \frac{G_3}{G_2} \right) = P_{\text{ave}_2} \left(1 + \frac{G_3}{G_2} \right)$$

$$\therefore P_{\text{ave}_2} = \frac{8.5}{1 + \frac{G_3}{G_2}} = \boxed{6.4 \text{ Watts}}$$

$$P_{\text{ave}_3} = 8.5 - 6.4 = \boxed{2.1 \text{ Watts}}$$

IMPEDANCE OR ADMITTANCE COORDINATES

Problem 10.16

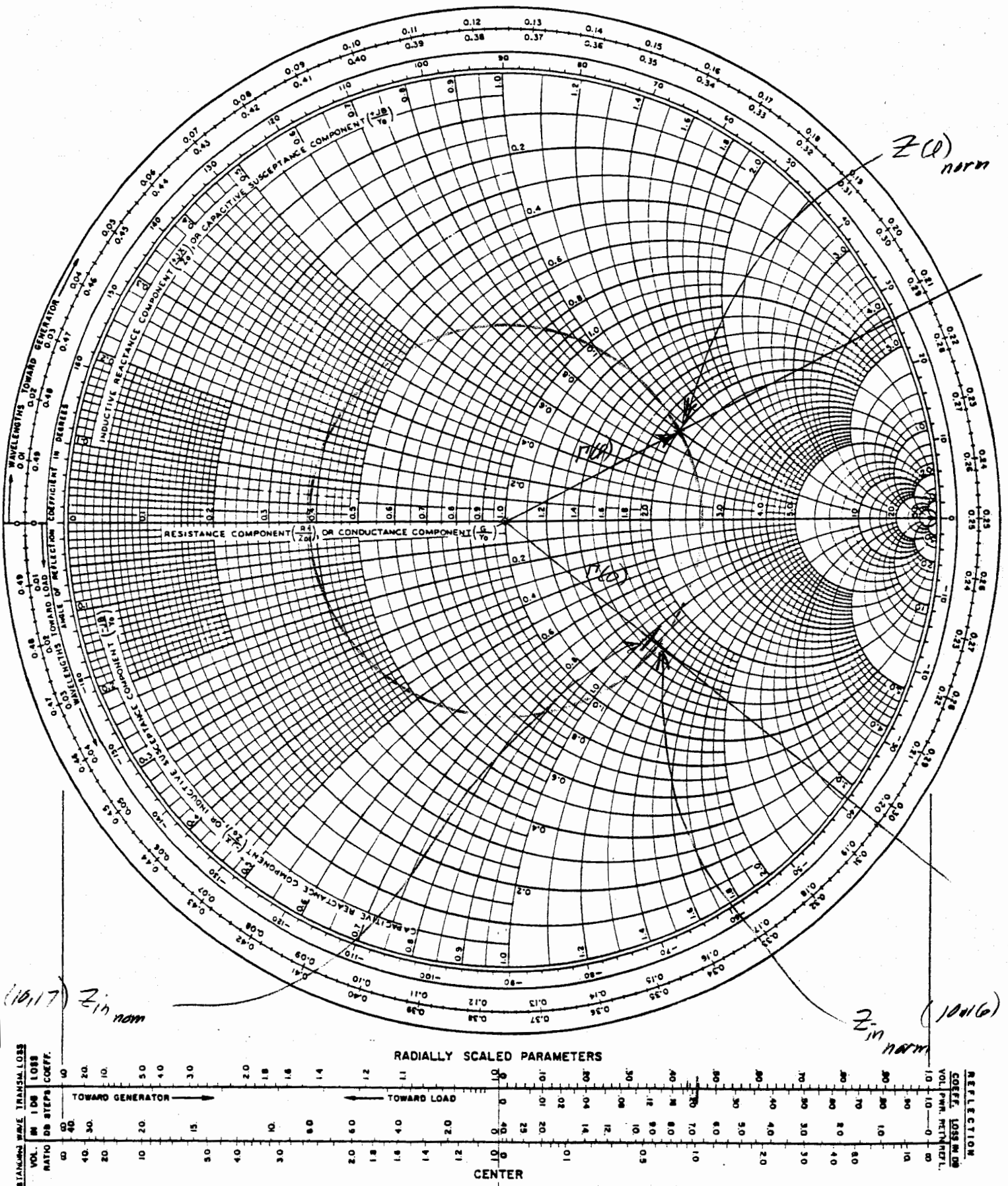


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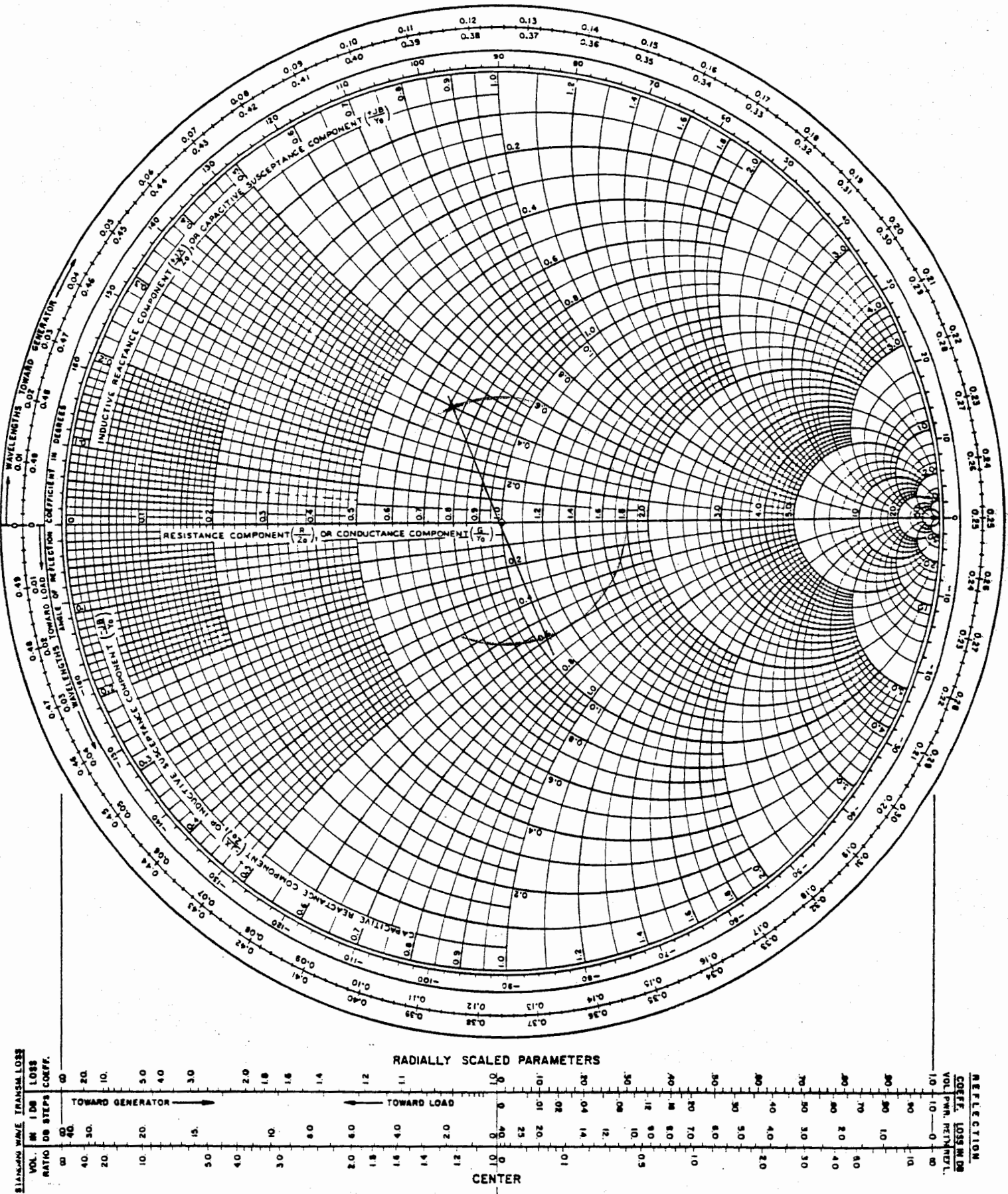
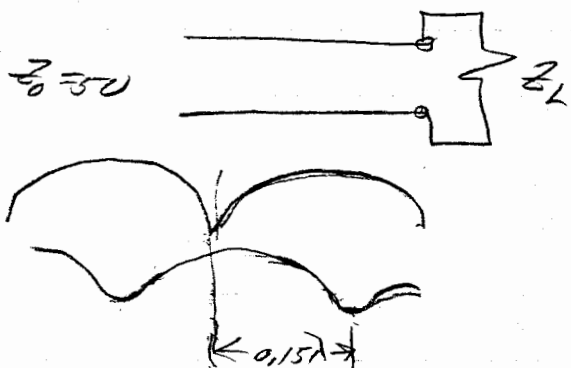


Fig. 9-3. A standard commercially available form of Smith chart graph paper. Copyrighted 1949 by Kay Electric Company, Pine Brook, N. J., and reprinted with their permission.

10.27

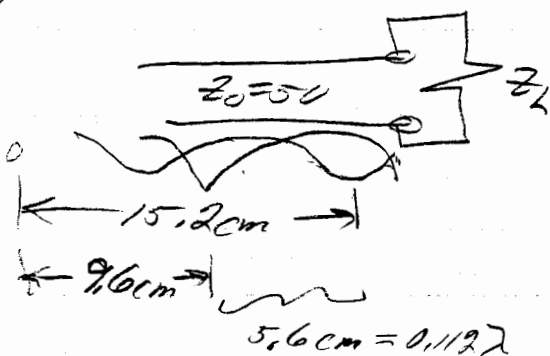


$SWR = 4.0$

from chart $Z_{L, norm} = 0.67 + j1.14$

$\therefore Z_L = 33.5 + j57$

10.28



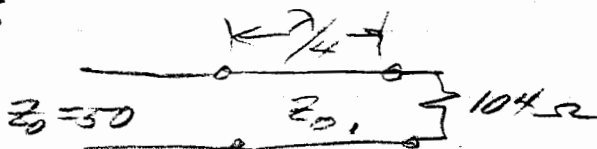
$f = 600 \text{ MHz} ; SWR = 3.5$

$\lambda = \frac{3 \times 10^8}{6 \times 10^8} = 0.5 \text{ m}$

from chart $Z_{L, norm} = 0.475 + j0.73$

or $Z_L = 23.75 + j36.5$

10.36

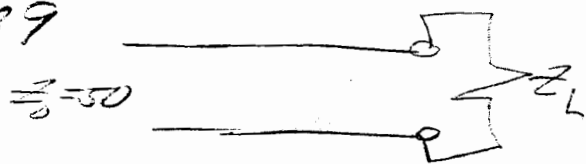


$f = 500 \text{ MHz} ; \epsilon_r = 2.26$

$Z_{01} = \sqrt{50 \times 104} = 72.1 \Omega$

$\lambda = \frac{3 \times 10^8}{\sqrt{2.26} \cdot 5 \times 10^8} = \frac{0.6}{1.5} = 0.4 \text{ m} \therefore \lambda/4 = 0.1 \text{ m}$

10.39



$f = 500 \text{ MHz} ; \lambda = 60 \text{ cm}$

$SWR = 3.5$

(see chart)

place stub $(0.25 - 0.171)\lambda = 0.08\lambda = 4.8 \text{ cm}$ either direction from V_{min}

a) for stub toward the load $Y_{stub} = -j1.3$; stub length = $0.355 - 0.25 = 0.105\lambda$
or stub length = 62.3 cm

SWR from generator to stub = 1
b) SWR from stub to load = 3.5

c) for stub toward the generator $Y_{stub} = +j1.3$; stub length = $(0.145 + 0.35)\lambda = 23.7 \text{ cm}$

IMPEDANCE OR ADMITTANCE COORDINATES

$Z_{Lnorm} = 0.475 + j0.73$

Problem 10.28

Z_{norm}
@ V_{min}
0.1127

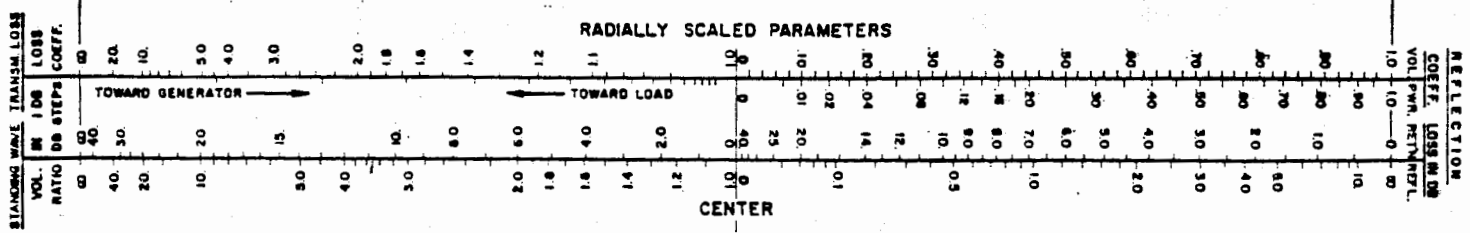
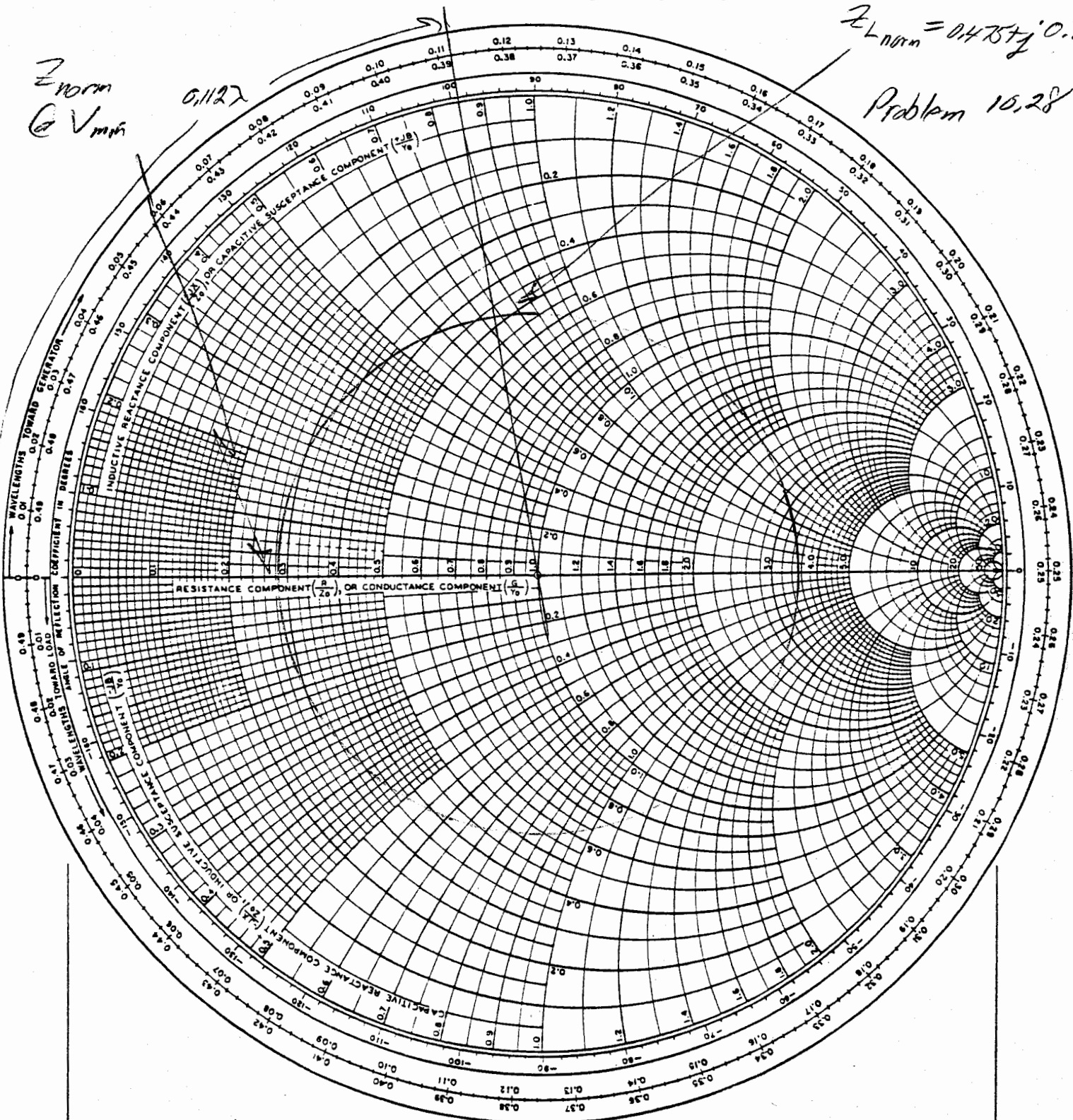


Fig. 9-3. A standard commercially available form of Smith chart graph paper. Copyrighted 1949 by Kay Electric Company, Pine Brook, N. J., and reprinted with their permission.

IMPEDANCE OR ADMITTANCE COORDINATES

$Z_{N \text{ min}} = 0.25$

$Z_{N \text{ load}} = 0.67 + j1.14$

Problem 10.27

0.157

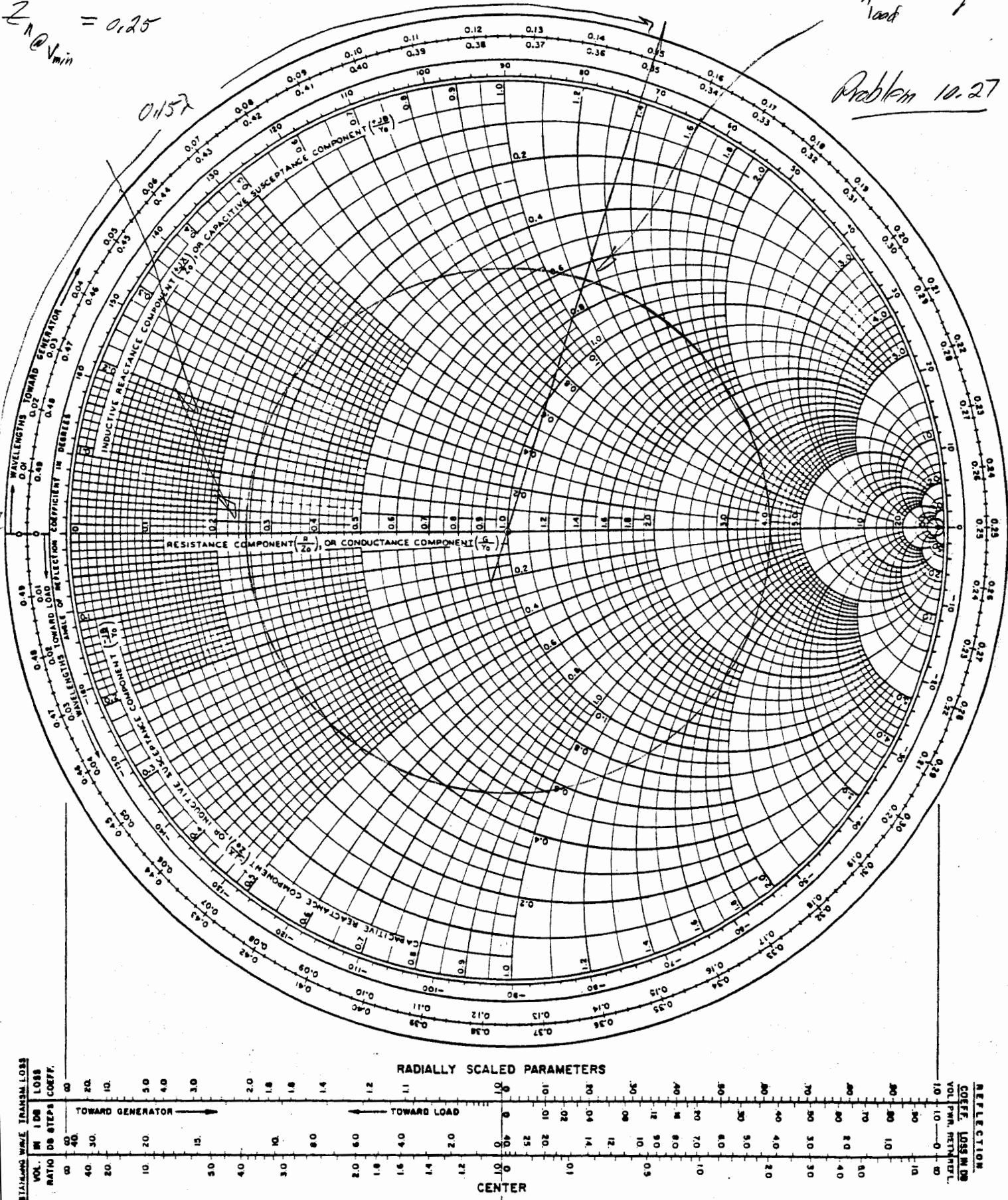


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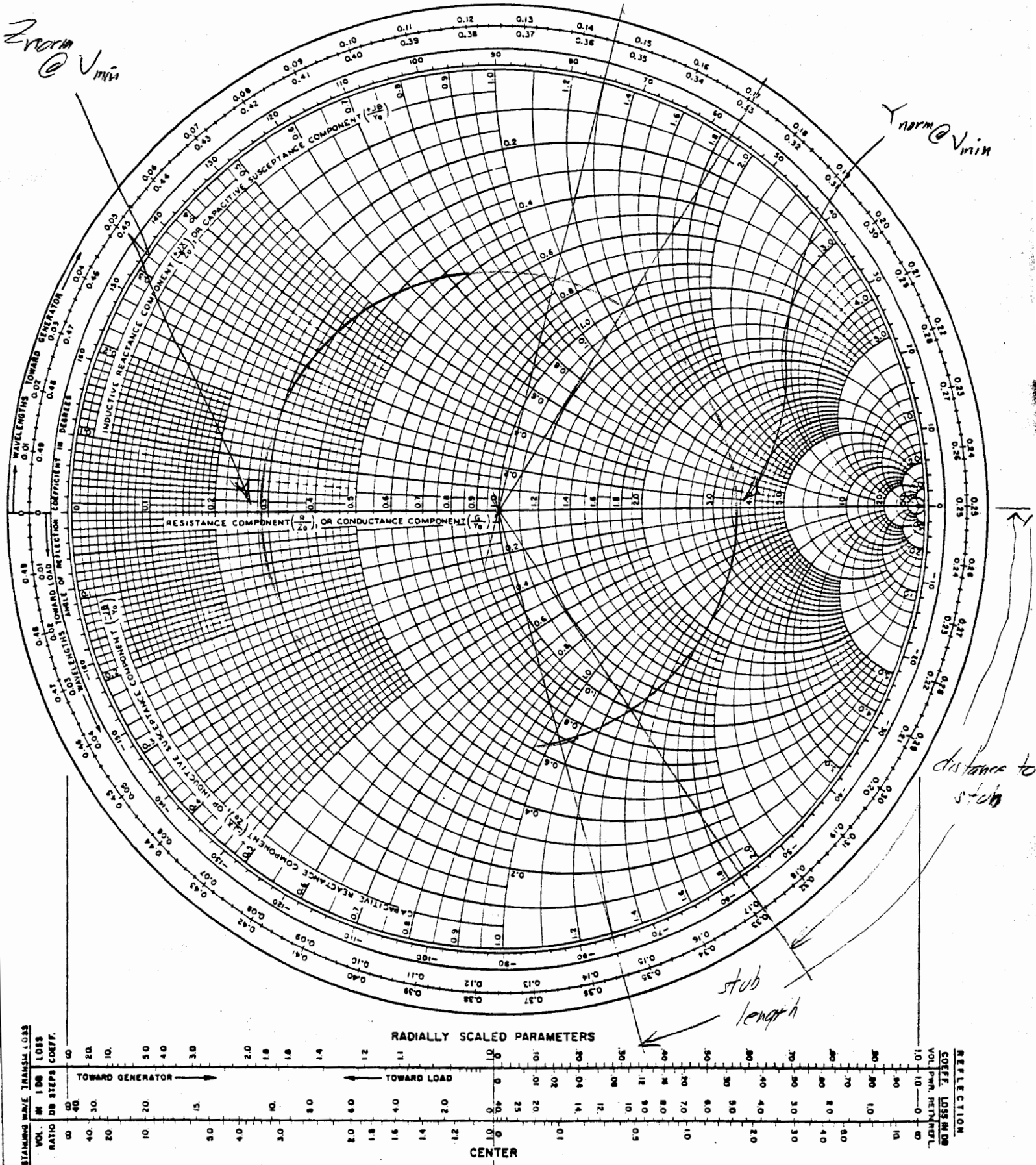
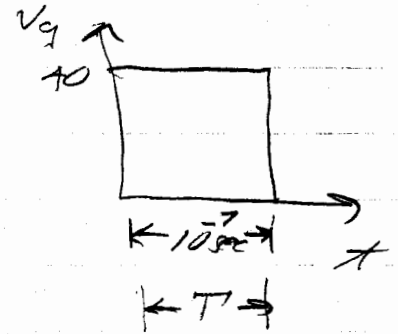
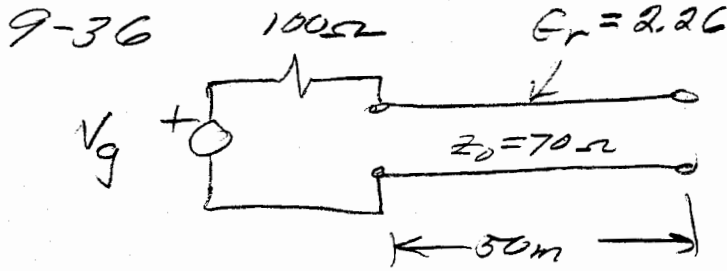


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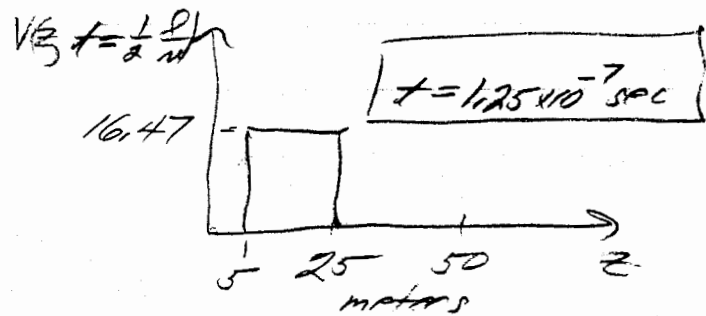
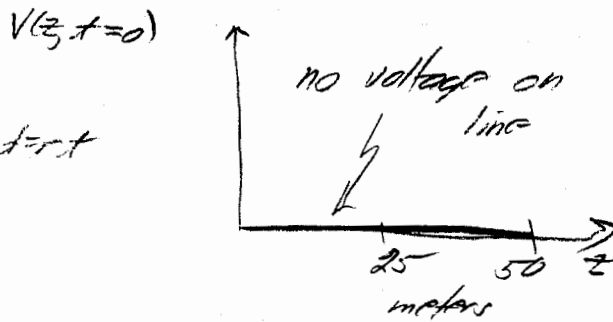
a)
$$v = \frac{3 \times 10^8}{\sqrt{2.26}} = 2 \times 10^8 \text{ m/sec}$$

$$V(z=0, t) = 40 \frac{70}{170} [\mu(t) - \mu(t-7)] = 16.47 [\mu(t) - \mu(t-7)]$$

$$I(z=0, t) = \frac{V(z=0, t)}{70} = \frac{40}{170} [\mu(t) - \mu(t-7)] = 0.235 [\mu(t) - \mu(t-7)]$$

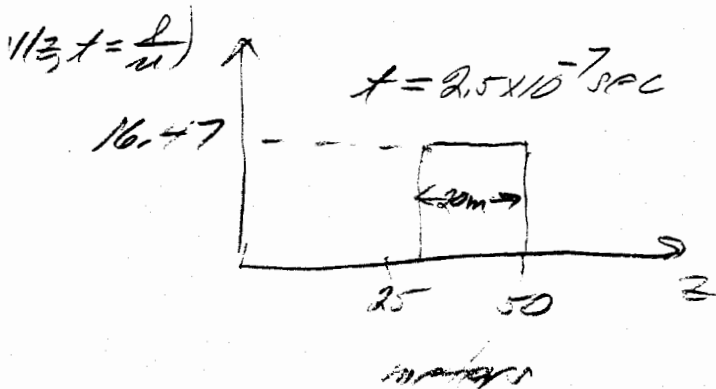
b)
$$V^+(t - \frac{z}{v}) = V_g(t - \frac{z}{v}) \times \frac{70}{170}$$

$$I^+(t - \frac{z}{v}) = \frac{1}{170} V_g(t - \frac{z}{v})$$

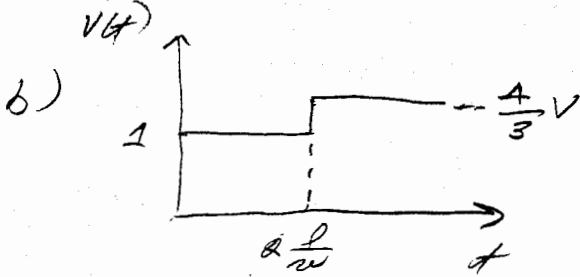
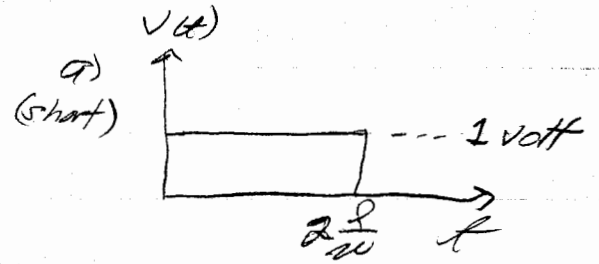
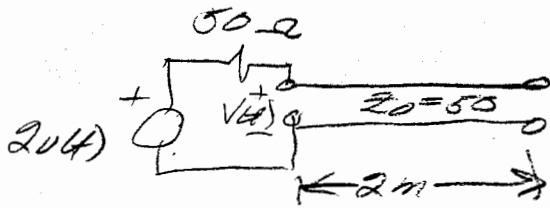


$$\frac{z}{v} = \frac{50}{2 \times 10^8} = 25 \times 10^{-8} = 2.5 \times 10^{-7} \text{ sec}$$

in 10^{-7} seconds wave travels $2 \times 10^8 \times 10^{-7} = \boxed{20 \text{ m}}$



9-38

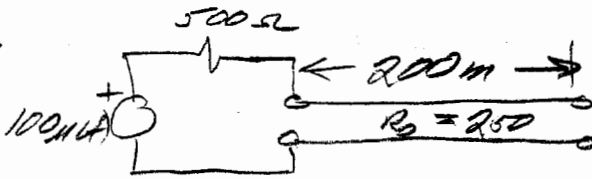


$$R_L = 100$$

$$\Gamma(t) = \frac{100 - 50}{100 + 50} = \frac{1}{3}$$

$$\frac{L}{u} = \frac{2}{3 \times 10^8} = \frac{2}{3} \times 10^{-8} \text{ sec}$$

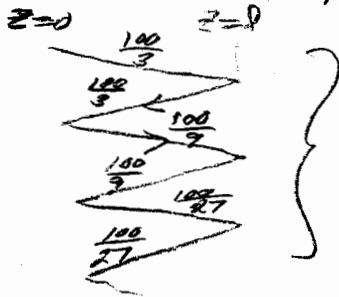
9-39



$$V^+(t, z=0) = 100 \frac{250}{750}$$

$$V^+(t, z=l) = \frac{100}{3}$$

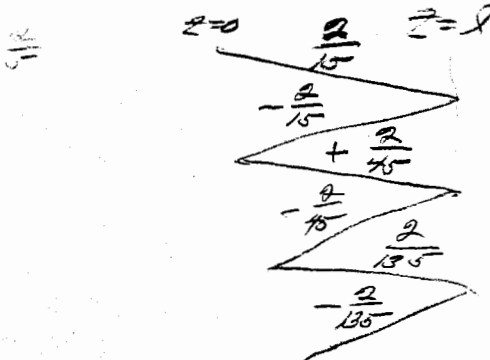
a) $\Gamma(l) = \frac{1}{3}$ $\Gamma(0) = 1$

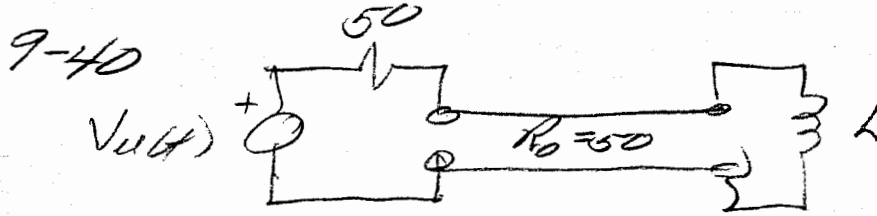


b) $V(z, t) = 100$ as $t \rightarrow \infty$

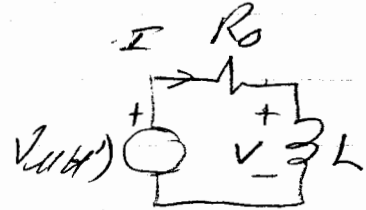
$$V(z, t) = V^+(t - \frac{z}{u}) + V^-(t + \frac{z}{u})$$

c) $I(z, t) = \frac{1}{R_0} \{ V^+(t - \frac{z}{u}) - V^-(t + \frac{z}{u}) \}$





@ load $v(t') = \frac{V}{2} u(t')$



for $t' > 0$ $v = IR_0 + L \frac{dI}{dt}$

$I_{\text{homogeneous}} = A e^{st}$; $0 = R_0 + Ls \Rightarrow s = -\frac{R_0}{L}$; $I_h = A e^{-\frac{R_0}{L} t'}$

$I_{\text{particular}} = K$ so $v = R_0 K$ or $K = \frac{v}{R_0}$

this gives $I = I_h + I_p = \frac{v}{R_0} + A e^{-\frac{R_0}{L} t'}$

assuming no initial energy storage (i.e. $I(t'=0) = 0$)

we have $I = \frac{v}{R_0} (1 - e^{-\frac{R_0}{L} t'}) = \frac{v+(t-\frac{l}{u})}{R_0} - \frac{v-(t+\frac{l}{u})}{R_0}$

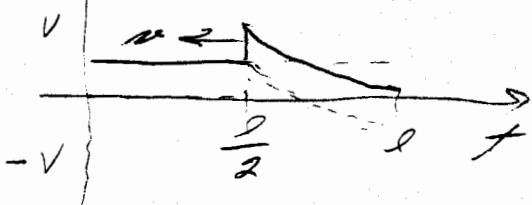
giving: $v-(t+\frac{l}{u}) = v+(t-\frac{l}{u}) - R_0 I (z=l, t)$

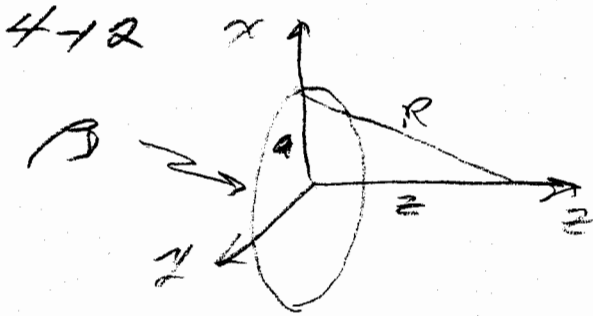
or $v-(t+\frac{l}{u}) = \frac{v}{2} u(t-\frac{l}{u}) - v(1 - e^{-\frac{R_0}{L}(t-\frac{l}{u})}) u(t-\frac{l}{u})$

$v-(t, z=l)$ $v-(t+\frac{l}{u}) = -\frac{v}{2} u(t-\frac{l}{u}) + v e^{-\frac{R_0}{L}(t-\frac{l}{u})} u(t-\frac{l}{u})$



$v(t = \frac{3}{2} \frac{l}{u}, z)$





$$a) \vec{E} = \int_{\phi=0}^{2\pi} \frac{\rho_0 a d\phi}{4\pi\epsilon R} = \frac{\rho_0 a}{2\epsilon \sqrt{a^2+z^2}}$$

$$\vec{E} = -\nabla\Phi = -\frac{\partial\Phi}{\partial z} = \frac{\rho_0 a 2z}{2\epsilon (a^2+z^2)^{3/2}}$$

$$b) \Phi = -\int_{\rho=\infty}^z \frac{\rho_0 a z}{2\epsilon (a^2+z^2)^{3/2}} dz = -\int_{\infty}^u \frac{\rho_0 a du}{4\epsilon u^{3/2}} = \frac{\rho_0 a}{2\epsilon u^{1/2}}$$

$u = a^2 + z^2$
 $du = 2z dz$

or $\Phi = \frac{\rho_0 a}{2\epsilon \sqrt{a^2+z^2}}$

$$4-15) a) \vec{E} = \frac{Q}{2\pi\epsilon l} \frac{1}{\rho} ; \Phi(\rho) = -\int_b^{\rho} \frac{Q}{2\pi\epsilon l} \frac{1}{\rho} d\rho = \frac{Q}{2\pi\epsilon l} \ln \frac{b}{\rho}$$

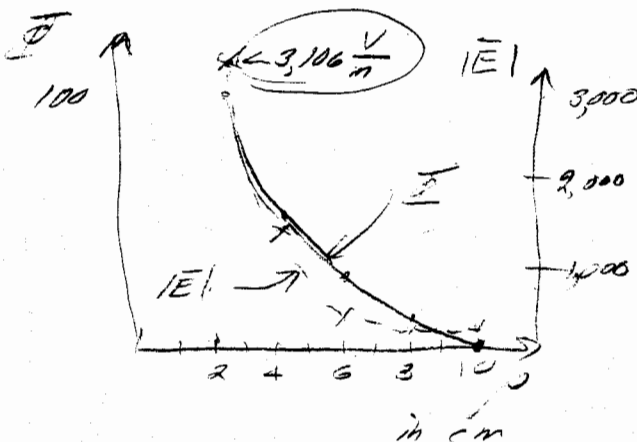
from book $C = \frac{Q}{V} = \frac{2\pi\epsilon l}{\ln \frac{b}{a}} = \frac{Q}{V} \implies \Phi(\rho) = V \frac{\ln \frac{b}{\rho}}{\ln \frac{b}{a}}$

$$\vec{E} = -\nabla\Phi = -\frac{\partial\Phi}{\partial\rho} = + \frac{V}{\ln \frac{b}{a}} \cdot \frac{b}{\rho} \cdot \frac{1}{b} \cdot \frac{1}{\rho} = \frac{V}{\ln \frac{b}{a}} \cdot \frac{1}{\rho}$$

c) $V=100, a=2cm, b=10cm, \epsilon_r=2$

$$C/m = \frac{2\pi\epsilon}{\ln \frac{b}{a}} = \frac{2\pi \times 10^{-9} \times 2}{\ln 5} = 0.06 \times 10^{-9} = 60 \frac{pF}{m}$$

$$\Phi = 100 \frac{\ln \frac{b}{\rho}}{\ln 5} = 62.13 \frac{1}{\rho}$$



$$|E| = \frac{100}{\ln \frac{b}{a}} \cdot \frac{1}{\rho} = 62.13 \left(\frac{1}{\rho} \right)$$

$$\frac{\Phi}{100} \ln 5 = \ln \frac{b}{\rho} \text{ or } \frac{b}{\rho} = e^{0.0161 \Phi}$$

$$\text{or } \rho = \frac{2.1}{e^{0.0161 \Phi}}$$

\bar{I}	ρ
0	0.1
25	0.0669
50	0.0447
75	0.0299
100	0.02

$$\text{@ } \rho = 0.06 \text{ m}$$

$$\bar{I} = 31.74 \text{ Volts} \leftarrow$$

4-16

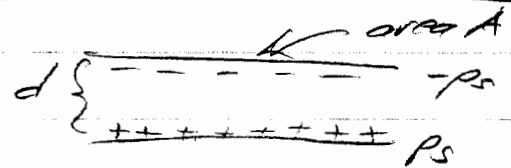
$$\text{for coax. } C/m = \frac{2\pi\epsilon}{\ln \frac{b}{a}} = 96.8 \times 10^{-12}$$

$$\ln \frac{b}{a} = \frac{2\pi \times 10^{-9} \times 0.26}{96.8 \times 10^{-12}} = 1.297 \quad ; \quad \frac{b}{a} = 3.658$$

$$\text{so } b = 0.713 \text{ in or } 1.81 \text{ cm} \leftarrow$$

4-21

$$U_e = \frac{1}{2} \int_V \bar{D} \cdot \bar{E} \, dv$$



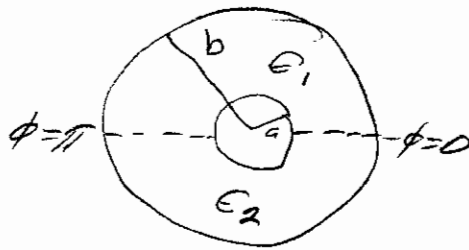
$$\bar{D} = \rho_s$$

$$\therefore U_e = \frac{1}{2} dA \rho_s^2 \frac{1}{\epsilon} = \frac{dA \rho_s^2}{2\epsilon}$$

$$\text{b) } U_e = \frac{1}{2} C V^2 \quad ; \quad V = Ed = \frac{\rho_s d}{\epsilon}$$

$$\therefore C = \frac{2U_e}{V^2} = \frac{\frac{dA \rho_s^2}{\epsilon}}{\frac{\rho_s^2 d^2}{\epsilon^2}} = \frac{AE}{d} \leftarrow$$

4.28



$$\Phi(a) = V \quad ; \quad \Phi(b) = 0$$

a) for example 4-12

$$\Phi(\rho) = V \frac{\ln \frac{b}{\rho}}{\ln \frac{b}{a}}$$

$$\vec{E} = -\nabla \Phi = \hat{\rho} \frac{1}{\rho} \cdot \frac{V}{\ln \frac{b}{a}}$$

These relations are valid. They give the correct potentials at $\rho = a$ and $\rho = b$ and tangential \vec{E} is continuous at $\phi = 0$ and $\phi = \pi$.

$$\left. \begin{array}{l} \text{a) in Region 1} \quad \vec{D}_1 = \epsilon_1 \frac{1}{\rho} \cdot \frac{V}{\ln \frac{b}{a}} \hat{\rho} \\ \text{in Region 2} \quad \vec{D}_2 = \epsilon_2 \frac{1}{\rho} \cdot \frac{V}{\ln \frac{b}{a}} \hat{\rho} \end{array} \right\} \leftarrow$$

$$\text{b) } q \text{ in length } l = \frac{\pi a l V}{\ln \frac{b}{a}} \{ \epsilon_1 + \epsilon_2 \} ; \quad C = \frac{\pi l}{\ln \frac{b}{a}} (\epsilon_1 + \epsilon_2) \leftarrow$$

$$C_{\text{top}} = \frac{\pi l \epsilon_1}{\ln \frac{b}{a}} ; \quad C_{\text{bottom}} = \frac{\pi l \epsilon_2}{\ln \frac{b}{a}} \leftarrow$$

$$\text{if } \epsilon = \frac{\epsilon_1 + \epsilon_2}{2} \quad C = \frac{2\pi l}{\ln \frac{b}{a}} \left\{ \frac{\epsilon_1 + \epsilon_2}{2} \right\} \quad \text{Q.E.D.} \leftarrow$$

$$\text{for } \epsilon_1 = 1 ; \quad \epsilon_2 = 2.26 ; \quad a = 2 \text{ mm} , \quad b = 7 \text{ mm}$$

$$C/l = \frac{\pi 10^{-9}}{\ln \left(\frac{7}{2} \right)} (1 + 2.26) = 0.0723 \times 10^{-9} = 72.3 \text{ pF/m} \leftarrow$$

$$4.29 \quad U_0 = \frac{1}{2} \iiint \vec{D} \cdot \vec{E} \, d\vec{a} = \frac{1}{2} \int_{\phi=0}^{\pi} \int_{\rho=0}^b \int_{z=0}^l \epsilon_1 \frac{V^2 \rho \, d\rho \, dz \, d\phi}{\rho^2 (\ln \frac{b}{a})^2} \\ + \frac{1}{2} \int_{\phi=\pi}^{2\pi} \int_{\rho=a}^b \int_{z=0}^l \epsilon_2 \frac{V^2 \rho \, d\rho \, dz \, d\phi}{\rho^2 (\ln \frac{b}{a})^2}$$

$$\text{or } U_0 = \frac{\pi l}{2} \frac{V^2 \ln \frac{b}{a}}{(\ln \frac{b}{a})^2} (\epsilon_1 + \epsilon_2) = \frac{1}{2} C V^2 \triangleleft$$

$$\therefore C = \frac{\pi l}{\ln \frac{b}{a}} (\epsilon_1 + \epsilon_2) \triangleleft$$

$$4.61 \quad 30 \rightarrow 500 \text{ pF in } 0 \text{ to } 260^\circ \quad V = 5000 \text{ V}$$

$$T = \frac{\partial U_0}{\partial \theta} = \frac{\Delta U_0}{\Delta \theta}$$

$$U_0 = \frac{1}{2} C V^2 \quad \therefore \Delta U_0 = \frac{V^2}{2} (30 - 500) = - V^2 \frac{470}{2}$$

$$T = - \frac{25 \times 10^6 \times 470 \times 10^{-12}}{2 \times 260 \times \pi / 180} = 1294 \times 10^{-6} = 1.294 \times 10^{-3} \text{ N-m}$$