

EE 321
Fall 2002

Homework #10

Solutions

4.66 See attached MATLAB plot

For $i_B = 10 \mu A$, $i_C = 1 mA$ and $V_{CE} = 4V$

For $i_B = 40 \mu A$, $i_C = 4 mA$ and $V_{CE} = 1V$

Because $V_E = 0V$, $V_C = V_{CE}$, so V_C will swing from $4V$ to $1V$, or $3V$ total.

When $V_{BE} = \frac{1}{2} V_{CC} = 2.5V$, $I_C = 2.5 mA$

$$I_B = I_C / \beta = 25 \mu A$$

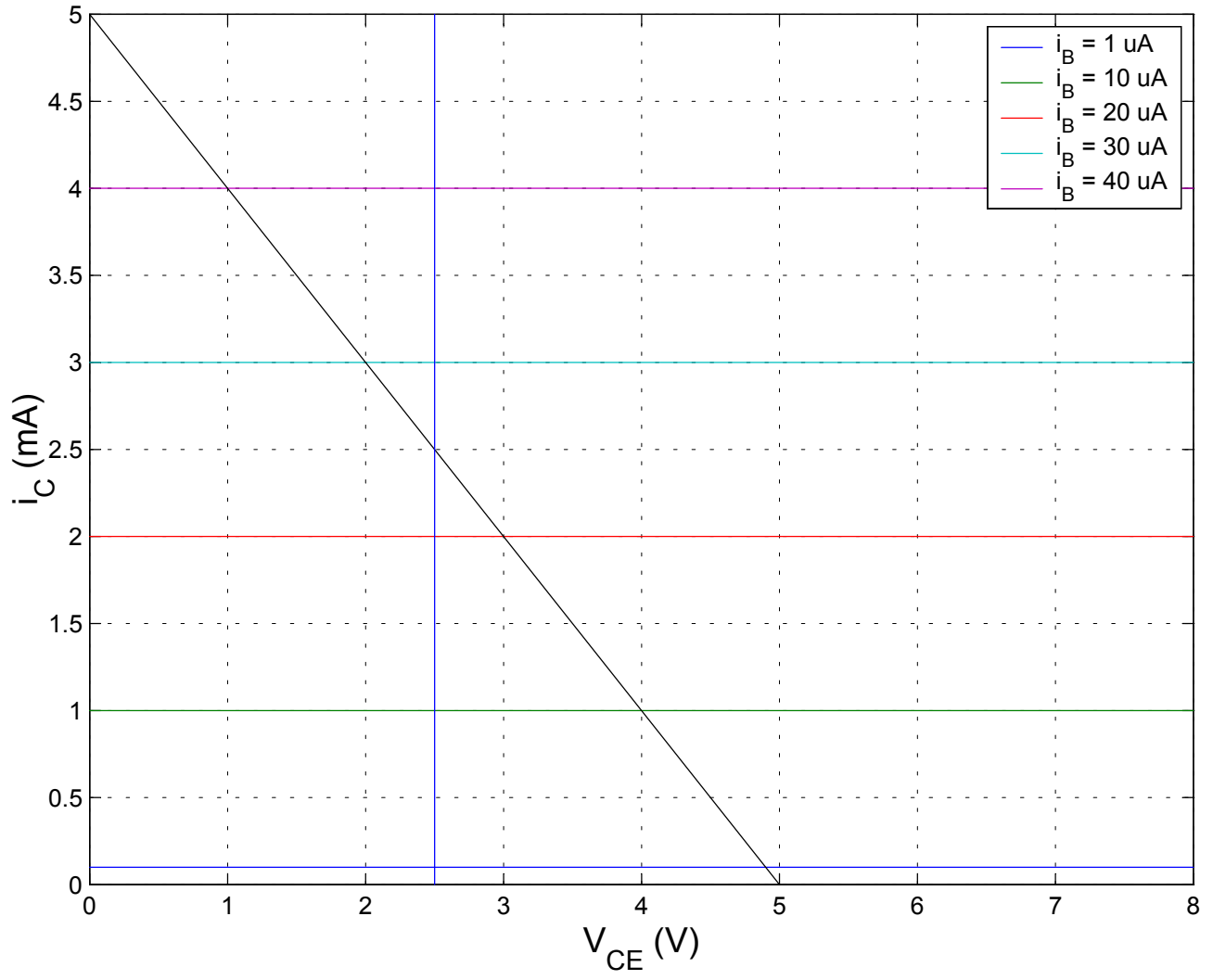
$$V_{BB} = I_B R_B + V_{BE} = (25 \mu A)(100 k\Omega) + 0.7V = 3.2V$$

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% Problem 4.66

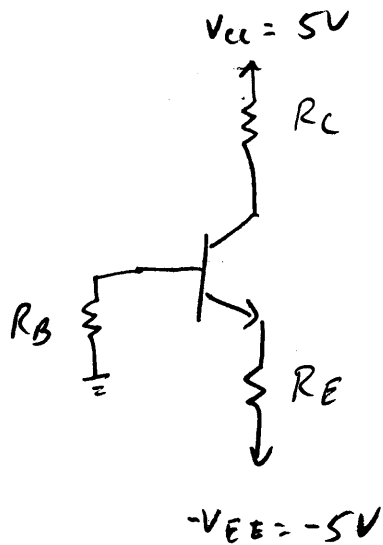
% Find  $i_C$  for  $i_B = 1, 10, 20, 30, 40$ 
%  $i_C = \beta * i_B$  for all  $V_{CE}$ 
beta = 100;
iB=[1 10 20 30 40]*1e-6;
VCE = [0:1:8];
for ii=1:5
    iC(ii,:) = beta*iB(ii)*ones(size(VCE));
end
plot(VCE,iC*1000)
legend('i_B = 1 uA','i_B = 10 uA','i_B = 20 uA','i_B = 30 uA','i_B = 40 uA')
hold on
xlabel('V_{CE} (V)','FontSize',14)
ylabel('i_{C} (mA)','FontSize',14)

% Calculate load line
RC = 1e3;
VL = [0 5];
IL = [5/RC 0];
plot(VL,IL*1000,'k')

% Plot line showing  $V_{CE} = 2.5$  V
plot([2.5 2.5],[0 beta*50e-6]*1000)
grid
```



4.70



For $\beta = \infty$: $I_B = 0 \Rightarrow V_B = 0 \Rightarrow V_E = -0.7V$

Want V_C 40% between V_E and V_{CC} :

$$V_C = 0.4(V_{CC} - V_E) + V_E = 0.4(5V - (-0.7V)) + (-0.7V) = \underline{1.58V}$$

$$V_C = V_{CC} - I_C R_C \Rightarrow R_C = \frac{V_{CC} - V_C}{I_C} = \frac{5V - 1.58V}{0.1mA} = 34.2k\Omega$$

The nearest 5% resistor is $R_C = 33k\Omega$

$$I_B R_B + V_{BE} + I_E R_E + V_{EE} = 0$$

$$R_E = \frac{-V_{EE} - V_{BE} - I_B R_B}{I_E} \quad \text{For } \beta = \infty, I_B = 0 \text{ and } I_E = I_C$$

$$R_E = \frac{-(-5V) - 0.7V + 0}{0.1mA} = 43k\Omega$$

43k Ω is a standard 5% resistor, so $R_E = 43k\Omega$

For $\beta \neq \infty$:

$$I_B R_B + V_{BE} + (\beta + 1) I_B R_E + V_{EE} = 0$$

$$I_E = \frac{I_B}{\beta + 1} = \frac{-V_{EE} - V_{BE}}{R_E + \frac{R_B}{\beta + 1}} = \frac{4.3V}{43k + \frac{R_B}{\beta + 1}}$$

$$I_E = \frac{V_E - V_{EE}}{R_E} \Rightarrow V_E = V_{EE} + I_E R_E = V_{EE} - \frac{V_{EE} + V_{BE}}{R_E + \frac{R_B}{\beta + 1}}$$

$$V_E = -5 + \frac{4.3V \cdot R_E}{R_E + \frac{R_B}{\beta + 1}}$$

$$V_C = V_{CC} - I_C R_C = V_{CC} - \alpha I_E R_C = 5 - \frac{\alpha \cdot 4.3 \text{ V} \cdot R_C}{R_E + R_B / (\beta + 1)}$$

$$V_{CE} = V_C - V_E = 5 - \frac{\alpha \cdot (4.3 \text{ V}) (R_C)}{R_E + R_B / (\beta + 1)} + 5 - \frac{(4.3 \text{ V}) (R_E)}{R_E + R_B / (\beta + 1)}$$

$$= 10 \text{ V} - \frac{(4.3 \text{ V}) (\alpha R_C + R_E)}{R_E + R_B / (\beta + 1)}$$

Solve for R_B

$$R_B = (\beta + 1) \left[\frac{4.3 \text{ V} (\alpha R_C + R_E)}{10 \text{ V} - V_{CE}} \right]$$

For $\beta = \infty$, $V_C = V_{CC} - I_C R_C = 4.7 \text{ V}$, $V_E = 0.7 \text{ V} \Rightarrow V_{CE} = 2.4 \text{ V}$

For $\beta = 70$, want V_{CE} to increase by no more than 20 %

$$V_{CE} < 1.2 \times 2.4 \text{ V} = 2.88 \text{ V}$$

$$R_B < (\beta + 1) \left[\frac{4.3 \text{ V} (\alpha R_C + R_E)}{10 - 2.736} - R_E \right] = 186 \text{ k}\Omega$$

Any R_B less than 186 k Ω will work

The largest 5% resistor less than 186 k Ω is 180 k Ω

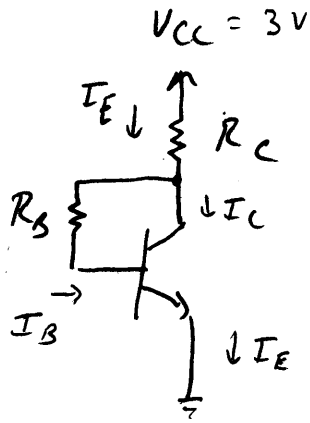
$$\text{Let } \boxed{R_B = 180 \text{ k}\Omega}$$

$$I_E = \frac{4.3 \text{ V}}{43 \text{ k} + R_B / \beta + 1} \Rightarrow I_E = 0.0944 \text{ mA} \quad \boxed{I_C = \alpha I_E = 0.093 \text{ mA}}$$

$$V_{CE} = 10 \text{ V} - \frac{4.3 \text{ V} (\alpha R_C + R_E)}{R_E + R_B / \beta + 1} \Rightarrow \boxed{V_{CE} = 2.87 \text{ V}}$$

For $\beta = 70$

4.73



Want $V_{CE} = 1.4V \Rightarrow V_C = 1.4V$

$$I_E = \frac{I_C}{\alpha} = \frac{\beta+1}{\beta} I_C = \frac{101}{100} (0.1 \text{ mA}) = 0.101 \text{ mA}$$

$$V_{CC} - V_C = I_E R_C \Rightarrow R_C = \frac{V_{CC} - V_C}{I_E} = \frac{3V - 1.4V}{0.101 \text{ mA}} = 15.84 \text{ k}\Omega$$

Nearest 5% value is $R_C = 16 \text{ k}\Omega$

$$I_B = I_C / \beta = 0.001 \text{ mA}$$

$$V_C = 1.4V, \quad V_B = 0.7V$$

$$I_B = \frac{V_C - V_B}{R_B} \Rightarrow R_B = \frac{V_C - V_B}{I_B} = \frac{1.4V - 0.7V}{0.001 \text{ mA}} = 700 \text{ k}\Omega$$

The nearest 5% resistor is $R_B = 680 \text{ k}\Omega$

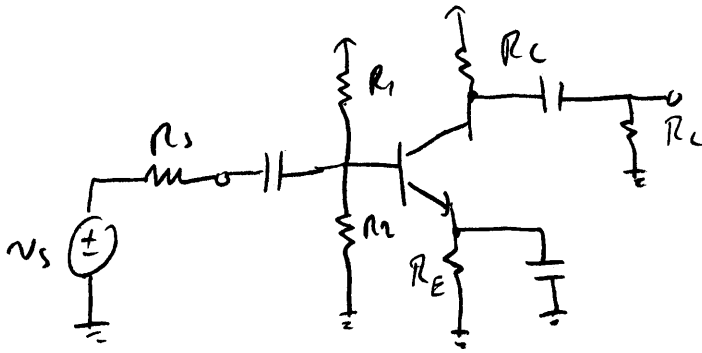
$$V_{CC} = I_E R_C + I_B R_B + V_{BE} = (\beta+1) I_B R_C + I_B R_B + V_{BE}$$

$$I_B = \frac{V_{CC} - V_{BE}}{(\beta+1) R_C + R_B}$$

$$V_C = V_{CC} - I_E R_C = V_{CC} - (\beta+1) I_B R_C$$

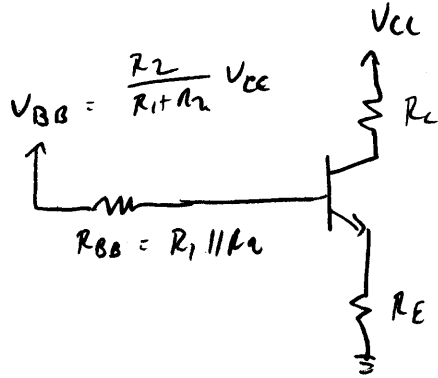
β	I_B	I_C	$V_{CE} = V_C$
50	0.0015 mA	0.077 mA	1.75V
200	0.00059 mA	0.118 mA	1.10V

4.78



$$\beta = 100$$

For DC



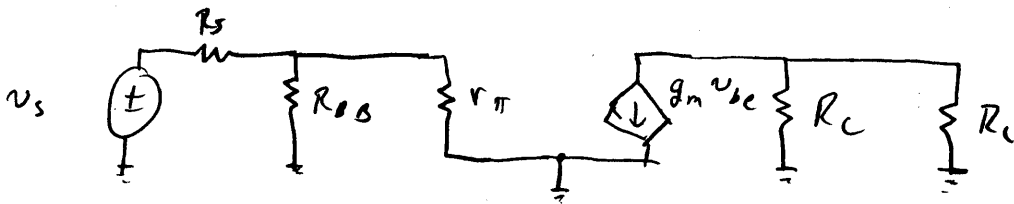
$$V_{BB} = \frac{R_2}{R_1 + R_2} V_{CC} = \frac{15k}{27k + 15k} 9V = 3.21V$$

$$R_{BB} = R_1 \parallel R_2 = 9.64k$$

$$V_{BB} = I_B R_{BB} + V_{BE} + (\beta + 1) I_B R_E$$

$$I_B = \frac{V_{BB} - V_{BE}}{R_{BB} + (\beta + 1) R_E} = \frac{9V - 0.7V}{9.64k + (101)(1.2k)} = 0.0634mA$$

$$I_E = (\beta + 1) I_B = 6.41mA$$

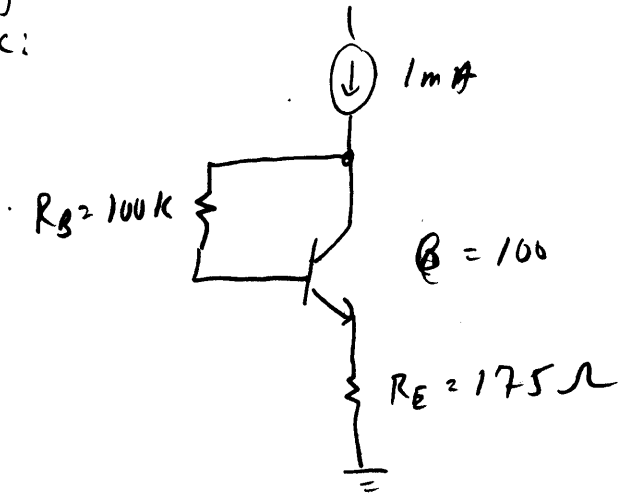


$$g_m = \frac{I_C}{V_T} = \frac{\beta I_B}{V_T} = 25V mA/V$$

$$r_{\pi} = \frac{V_T}{I_B} = 394 \Omega$$

4.85

(a)
DC:



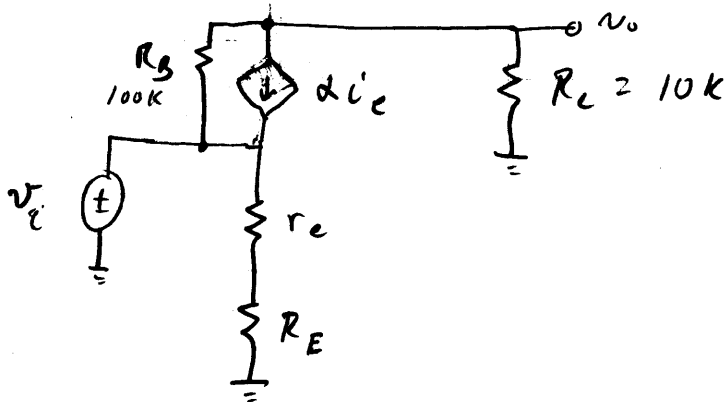
$$I_E = 1 \text{ mA} \Rightarrow I_C = \alpha I_E = \frac{\beta}{\beta + 1} I_E = \boxed{0.99 \text{ mA} = I_C}$$

$$V_C = I_B R_B + V_{BE} + I_E R_E = \frac{I_E R_B}{\beta + 1} + V_{BE} + I_E R_E$$

$$\boxed{V_C = 1.865 \text{ V}}$$

$$r_e = \frac{V_T}{I_E} = 25 \Omega$$

(b) Small signal



$$i_e = \frac{v_i}{R_E + r_e}$$

$$\frac{v_i}{R_E + r_e}$$

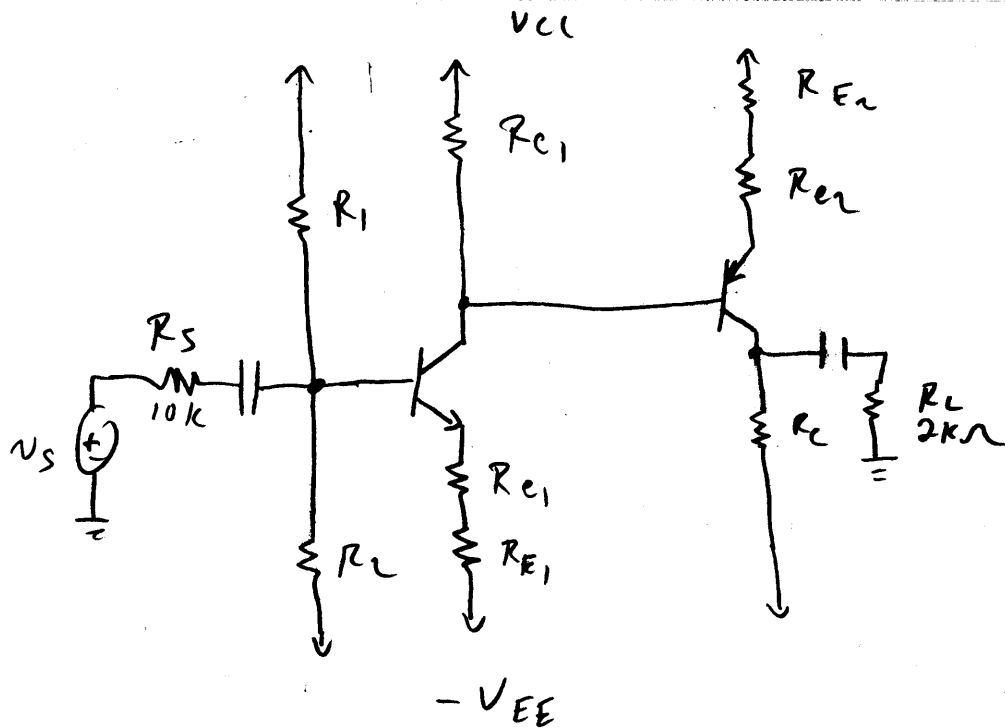
KCL at v_o :

$$\frac{v_o - v_i}{R_B} + \alpha i_e + \frac{v_o}{R_L} = 0$$

Solve for v_o :

$$\frac{v_o}{v_i} = (R_B \parallel R_L) \left(\frac{1}{R_B} - \frac{\alpha}{R_E + r_e} \right) = -44.9 \text{ V/V}$$

6.

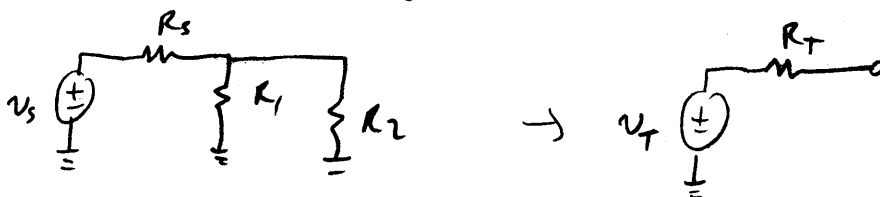


In the small signal analysis Stage 1 sees R_{c1} in parallel with R_{i2} (the input resistance of Stage 2), so

$$A_{v_1} = \frac{-\beta(R_{c1} \parallel R_{i2})}{R_{s_1} + (\beta+1)(r_{e_1} + R_{E1})} \quad (\text{eq. 4.75})$$

where $R_{i2} = (\beta+1)(r_{e_2} + R_{E2})$ (eq 4.70)

The input to stage 1 can be redrawn:



$$\text{where } V_T = \frac{R_1 \parallel R_2}{R_s + R_1 \parallel R_2} v_s \quad \text{and} \quad R_T = R_s \parallel R_1 \parallel R_2$$

The output voltage of Stage 1 is

$$v_{o_1} = A_{v_1} v_T = A_{v_1} \frac{R_1 \parallel R_2}{R_s + R_1 \parallel R_2} v_s$$

$$\text{and } R_{s_1} = R_T$$

We will make $R_{BB} = R_1 \parallel R_2 \gg R_S$ so

$$R_T = R_S \parallel R_{BB} \approx R_S, \quad \text{and } v_T = \frac{R_1 \parallel R_2}{R_1 \parallel R_2 + R_S} v_S$$

Then $v_{o1} = A_{v1} v_S$ and $R_{S2} = R_S$

Stage 2 sees R_L is parallel with R_{C2} , so

$$A_{v2} = \frac{-\beta(R_{C2} \parallel R_L)}{R_{S2} + (\beta+1)(r_{e2} + R_{C2})}$$

R_{S2} is the output resistance from stage 1

$$R_{S2} = R_{o1} = R_{C1} \quad (\text{eg on Page 488 of text})$$

The input voltage to Stage 2 is the output voltage from Stage 1, so

$$v_o = A_{v2} v_{i2} = A_{v2} v_{o1} = A_{v2} A_{v1} v_S$$

$$\frac{v_o}{v_S} = \frac{-\beta(R_{C1} \parallel [(\beta+1)(r_{e2} + R_{C2})])}{R_S + (\beta+1)(r_{e1} + R_{C1})} \cdot \frac{\beta(R_{C2} \parallel R_L)}{R_{C1} + (\beta+1)(r_{e2} + R_{C2})}$$

To make gain independent of β , want R_{C1} and R_{C2} fairly large, but this reduces the gain.

Also, want R_{C2} fairly large so $R_{C2} \parallel R_L$ is large. However, if R_{C2} is too large, the emitter current of stage 2 will not be able to supply the 2mA needed by the load.

$$\text{Let } R_{C2} = 2.2 \text{ k}\Omega, R_{E2} = 1 \text{ k}\Omega, I_{E2} = 7 \text{ mA}$$

$$\text{Then } V_{C2} = I_{C2} R_{C2} - 15 \text{ V} \approx I_{E2} R_{C2} - 15 \text{ V} = 0.4 \text{ V}$$

$$V_{E2} = 15 \text{ V} - I_{E2} R_{E2} = 8 \text{ V}$$

This gives plenty of voltage swing for v_o (need $\pm 4 \text{ V}$)

$$V_{E2} = 8 \text{ V} \Rightarrow V_{C1} = V_{E2} - V_{BE2} = 7.3 \text{ V}$$

Let $I_{E1} = 1 \text{ mA}$ (don't need much current in stage 1, because it just drives the base current for stage 2)

$$R_{C1} = \frac{15 \text{ V} - V_{C1}}{I_{C1}} \approx \frac{15 \text{ V} - V_{C1}}{I_{E1}} = 7.7 \text{ k}\Omega \rightarrow 7.5 \text{ k}\Omega \quad (\text{nearest } 5\%)$$

$$\text{Let } V_{B1} = -5 \text{ V} \quad \left(\frac{1}{3} \text{ of way between } V_{EE} \text{ and } V_{CC} \right)$$

We can do this with $R_2 = 50 \text{ k}\Omega \rightarrow 51 \text{ k}\Omega, R_1 = 100 \text{ k}\Omega$

$$\text{Then } V_{E1} = V_{B1} - V_{BE1} = -5.7 \text{ V}$$

$$R_{E1} = \frac{V_{E1} - (-15 \text{ V})}{I_{E1}} = \frac{-5.7 \text{ V} + 15 \text{ V}}{1 \text{ mA}} = 9.3 \text{ k}\Omega \rightarrow 9.1 \text{ k}\Omega$$

$$\text{Note that } r_{e1} = \frac{V_T}{I_{E1}} = 25 \Omega$$

$$r_{e2} = \frac{V_T}{I_{E2}} = 3.6 \Omega$$

To find gains, assume $\beta = 150$

Want $A_{v2} = 10$:

$$A_{v2} = \frac{\beta (R_{c2} \parallel R_L)}{R_{c1} + (\beta + 1)(r_{e2} + R_{E2})}$$

$$R_{E2} = \frac{\left[\frac{\beta (R_{c2} \parallel R_L)}{A_{v2}} - R_{c1} \right]}{\beta + 1} - r_{e2} = 52 \Omega \rightarrow 51 \Omega$$

$$A_{v1} = \frac{\beta (R_{c1} \parallel R_{i2})}{R_S + (\beta + 1)(r_{e1} + R_{E1})}$$

$$R_{i2} = (\beta + 1)(r_{e2} + R_{E2}) = 8.2 \text{ k}$$

$$R_{E1} = \frac{\left[\frac{\beta (R_{c1} \parallel R_{i2})}{A_{v1}} - R_S \right]}{\beta + 1} - r_{e1} = 105 \Omega \rightarrow 100 \Omega$$

$$R_1 = 100 \text{ k} \quad R_2 = 51 \text{ k}$$

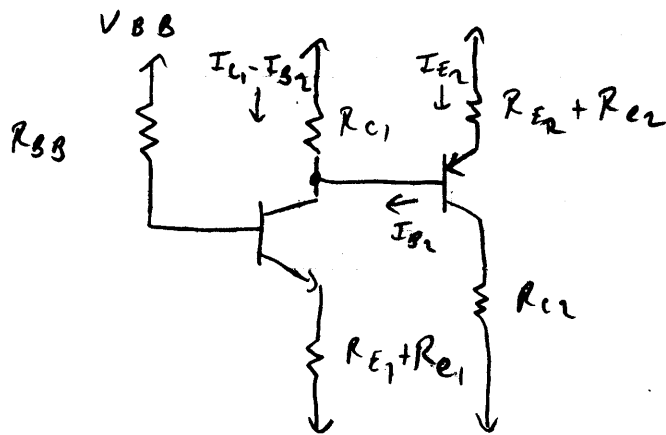
$$R_{C1} = 7.5 \text{ k} \quad R_{C2} = 2.2 \text{ k}$$

$$R_{E1} = 9.1 \text{ k} \quad R_{E2} = 1 \text{ k}$$

$$R_{e1} = 100 \Omega \quad R_{e2} = 51 \Omega$$

Solve for $\beta = 100$. Find actual bias voltages, currents, r_{e1} , r_{e2} , gain.

Look at DC only for bias:



$$V_{BB} = \frac{3V}{R_1 + R_2} \times R_2 - 15V = -5V$$

$$R_{BB} = R_1 \parallel R_2 = 34k\Omega$$

KVL from V_{BB} through R_{BB} , V_{BE1} , R_{E2} to V_{EE}

$$0 = I_{B1} R_{BB} + 0.7V + (\beta + 1) I_{B1} (R_{E1} + R_{e1})$$

$$I_{B1} = \frac{70V - 0.7V}{R_{BB} + (\beta + 1)(R_{E1} + R_{e1})} = 0.0097 \text{ mA}$$

$$I_{E1} = (\beta + 1) I_{B1} = 0.98 \text{ mA}$$

$$V_{E1} = I_{E1} (R_{E1} + R_{e1}) - 15V = -6.0V$$

$$I_{C1} = \beta I_{B1} = 0.97 \text{ mA}$$

KVL from V_{CC} through R_{E2} , V_{BE2} , R_{C1} to V_{CC}

$$0V = (\beta + 1) I_{B2} R_{E2} + 0.7V - (I_{C1} - I_{B2}) R_{C1}$$

$$I_{B2} = \frac{I_{C1} R_{C1} - 0.7V}{R_{C1} + (\beta + 1)(R_{E2} + R_{e2})} = 0.058 \text{ mA}$$

$$I_{E2} = (\beta + 1) I_{B2} = 5.8 \text{ mA}$$

$$I_{C2} = \beta I_{B2} = 5.8 \text{ mA}$$

$$V_{E2} = V_{CC} - I_{E2} (R_{E2} + R_{e2}) = 0V - 8.9V$$

$$V_{C2} = I_{C2} R_{C2} - 15V = -2.8V$$

$$r_{e1} = \frac{V_T}{I_{E1}} = 26 \Omega$$

$$r_{e2} = \frac{V_T}{I_{E2}} = 4.3 \Omega$$

$$R_{i2} = (\beta + 1)(r_{e2} + R_{E2}) = 5.6 \text{ k}\Omega \quad (11.k)$$

$$\frac{v_o}{v_i} = \frac{\beta (R_{C1} \parallel R_{i2})}{R_s + (\beta + 1)(r_{e1} + R_{E1})} \cdot \frac{\beta (R_{C2} \parallel R_L)}{R_{C1} + (\beta + 1)(r_{e2} + R_{E2})} = 113 \text{ V/V}$$

Do the same for $\beta = 200$

	$\beta = 100$	$\beta = 200$
I_{B1}	0.0097 mA	0.0049 mA
I_{E1}	0.98 mA	0.99 mA
I_{C1}	0.97 mA	0.99 mA
V_{E1}	-6.0 V	-5.9 V
V_{C1}	8.2 V	7.8 V
I_{B2}	0.058 mA	0.031 mA
I_{E2}	5.8 mA	6.2 mA
I_{C2}	5.8 mA	6.1 mA
V_{E2}	8.9 V	8.5 V
V_{C2}	-2.2 V	-1.5 V
r_{e1}	26 Ω	25 Ω
r_{e2}	4.3 Ω	4.0 Ω
$\frac{v_o}{v_i}$	113	287

Will work, but gain is fairly dependent on β .
 Could improve this by isolating the stages with emitter followers